

U.S.Department of Transportation Federal Highway Administration



I-80 Reconstruction SR 0080 Section 17M Preliminary Noise Analysis

Agreement E02656 MPMS 76357

> July 2016 Prepared by



Pennsylvania Department of Transportation Interstate 80 Reconstruction SR 0080 Section 17M

Preliminary NOISE ANALYSIS

Submitted to:

Pennsylvania Department of Transportation District 5 1002 Hamilton Street Allentown, PA 18101

Submitted by:



July 2016

Table of Contents

I.	Executive Summary	1
II.	Introduction	2
III.	Alternatives Considered	3
IV.	Noise Monitoring Methodology and Results	4
V.	Noise Modeling Methodology and Existing Conditions	6
VI.	Evaluation of Design Year Noise Levels & Noise Impact Assessment 1	1
VII.	Undeveloped Lands 1	8
VIII.	Noise Abatement Evaluation and Mitigation1	9
IX.	Construction Noise	5
X.	Public Involvement	5
XI.	Conclusion	6

FIGURES

Figure 1 – Project Location Map

Figure 2-1 to 4-5 – Project Specific Mapping

TABLES

 Table 1 – FHWA/PennDOT Noise Abatement Criteria

 Table 2 – Sound Level Summary

Table 3 – Undeveloped Lands Noise Level Summary

 Table 4-1 – Alternative 2A Noise Mitigation Evaluation

Table 4-2 – Alternative 2B Noise Mitigation Evaluation

 Table 4-3 – Alternative 2D Noise Mitigation Evaluation

 Table 5-1 – Alternative 2A Noise Abatement Feasibility/Reasonableness Evaluation

 Table 5-2 – Alternative 2B Noise Abatement Feasibility/Reasonableness Evaluation

 Table 5-3 – Alternative 2D Noise Abatement Feasibility/Reasonableness Evaluation

Table 6- Noise Impact Summary

APPENDICES

- Appendix A Noise Meter and Acoustical Calibrator Calibration Certificates
- **Appendix B** Noise Monitoring Data Forms

Appendix C – Noise Monitoring Data (2013)

Appendix D – Traffic Data Summary

Appendix E – TNM Noise Modeling Input and Output Files

Appendix F – Feasibility and Reasonableness Worksheets

Appendix G – References

Appendix H – List of Preparers and Reviewers

I. Executive Summary

As a means to promote safe and efficient traffic flow within the I-80 corridor from west of Exit 303 in Stroud Township to west of Exit 308 in East Stroudsburg Borough in Monroe County, FHWA and PennDOT are proposing the Interstate 80 Reconstruction Project. The project involves the addition of travel lanes to mainline Interstate 80, as well as interchange improvements at Route 209 (Exit 304), West Main Street (Business Route 209/Exit 305), Route 611 (Exit 303), Park Avenue (Route 611/Exit 307), and Broad Street (Route 191/Exit 307). Exit 306 (Dreher Avenue) will be eliminated as part of this project. These improvements are being proposed to provide greater operational efficiency for existing and Design Year traffic volumes. Information from this report will be incorporated into the NEPA document for the project, currently scoped as an Environmental Assessment.

This report documents the existing and Design Year noise levels associated with the three potential alternatives for I-80 Reconstruction Project in Monroe County, Pennsylvania. Noise monitoring of Category B and Category E noise receptor sites was performed at 30 locations to gain a thorough understanding of the existing noise environment. In addition, the noise analysis included noise projections for undeveloped lands (Category G) and can be referenced in Section VII of this report. These sites were also modeled and an additional 124 noise modeling "only" receptor sites were added to better quantify the effect of the improvements to noise-sensitive land uses within the project area. For reporting purposes, the project was divided into areas of common noise environment, referred to as Noise Study Areas (NSAs). Noise modeling was completed for existing (2013), Design Year (2045) No-Build conditions and Design Year (2045) Build conditions. Existing (2013) worst-case noise levels exceed FHWA/PennDOT Noise Abatement Criteria (NAC) at 52 receptor sites representing 112 residences, four commercial properties and one cemetery.

Design Year (2045) No-Build noise levels increase by approximately one dB(A)throughout the project area and exceed the NAC at 66 receptor sites representing 147 residences, four commercial properties and one cemetery. Design Year (2045) Build condition noise levels for Alternative 2A are projected to increase, as a result of widening and reconstruction of I-80 and the associated ramps. Noise levels are projected to exceed the NAC at 89 receptor sites representing 190 residences, four commercial properties and one cemetery. Of these, two receptors representing two residences would be acquired under the Alternative 2A condition. Design Year (2045) Build condition noise levels for Alternative 2B are projected to increase, as a result of widening and reconstruction of I-80 and the associated ramps. Noise levels are projected to exceed the NAC at 75 receptor sites representing 129 residences, four commercial properties and one cemetery. Of these, 10 receptors representing 30 residences would be acquired under the Alternative 2B condition. Design Year (2045) Build condition noise levels for Alternative 2D is projected to increase, as a result of widening and reconstruction of I-80 and the associated ramps. Noise levels are projected to exceed the NAC at 69 receptor sites representing 103 residences, four commercial properties and one cemetery. Specific to

this alternative, five receptors representing 21 residences would be acquired under the Alternative 2D condition.

The following discussions detail the noise analysis methodology and results for each NSA, under all three alternatives, and presents noise mitigation options where warranted. Based on the noise modeling results, it has been determined that, within these limits of work, noise abatement is feasible (i.e., capable of reducing Design Year noise levels by at least 5 dBA) and reasonable (cost-effective) for six Noise Study Areas under the Alternative 2A option, five areas under the Alternative 2B option, and five areas under the Alternative 2D option. The details of the proposed mitigation measures are contained within this report.

II. Introduction

Impacts associated with noise are often a prime concern when evaluating roadway improvement projects. Roadway construction at a new location or improvements to the existing transportation network may cause negative impacts to the noise-sensitive environment located adjacent to the project area. For this reason, the Federal Highway Administration (FHWA) and Pennsylvania Department of Transportation (PennDOT) have established a noise analysis methodology and noise level criteria to assess the potential noise impacts associated with construction and use of transportation related projects. In accordance with 23 CFR 772.5, the project is defined as a Type I project and the results of the noise analysis are included in the following sections of the report.

The purpose of this study is to develop a comprehensive overview of traffic noise within the identified study area for the I-80 Reconstruction Project in Monroe County, Pennsylvania. This analysis was initiated to enable a preliminary investigation of project alternatives and potential noise impacts for the proposed improvement project. PennDOT has proposed the corridor improvements to enhance overall mobility and improve safety conditions within Stroud Township and the Boroughs of East Stroudsburg, and Stroudsburg. The boundary of the study area begins approximately one half mile west of the I-80 Exit 303 and terminates at Broadhead Creek, approximately one quarter mile east of the Route 191 off ramp. The project area can be seen in *Figure 1*.

This report details the steps involved in the Preliminary noise analysis for the I-80 Reconstruction Project including noise monitoring and modeling methodologies, results, impact evaluation, mitigation alternatives and preliminary abatement recommendations. Information from this report will be incorporated into the NEPA document for the project, currently scoped as an Environmental Assessment.

The methodologies applied to this noise analysis are in accordance with the Pennsylvania Department of Transportation's (PennDOT) "*Project Level Highway Traffic Noise Handbook*" Publication No. 24, November 2015. PennDOT guidelines are based on the updated U.S. Department of Transportation Federal Highway Administration, Federal Aid Policy Guide 23 CFR 772, U.S. Government Printing Office.

III. Alternatives Considered

Five preliminary build alternatives were assessed in the Phase I Alternatives Analysis Report. Three alternatives have been carried forward for Phase II analysis: Alternatives 2A, 2B, and 2D. A detailed discussion of each of the alternatives considered for the analysis can be referenced below.

Alternative 2A

After completion of Phase I, A combination of Phase I Alternatives H and I were selected and renamed Alternative 2A for Phase II. I-80 Mainline will generally follow the existing alignment, while Interchange improvements will occur at SR 611 Interchange (Exit 303), US 209/Business, and 209/Dreher Avenue Interchanges (Exits 304, 305, and 306).

Mainline I-80 will generally follow the existing alignment and the proposed typical section consists of 3-12 foot lanes each way with a 26-foot median (including 12-foot inside shoulders) and flanking 12-foot outside shoulders. Interchanges improvements will occur at the SR 611 Interchange (Exit 303), US 209/Business, and 209/Dreher Avenue Interchanges (Exits 304, 305, 306, and 307).

Alternative 2B

After completion of Phase I, Alternatives 1F and 1G were combined into Alternative 2B due to similarities in provided movements. Interchange improvements will occur at the SR 611 Interchange (Exit 303), US 209/Business, 209/Dreher Avenue Interchanges (Exits 304, 305, and 306), and SR 191 Interchange (Exit 307).

Due to the proximity of Exit 305 to Exit 304, the two interchanges function as one. In comparison to Phase I, the movements at Exit 305 have had horizontal and vertical changes. The connection of the ramps to West Main St has changed slightly to reduce overall impacts and improve the geometry of West Main St. Improvements to West Main St will start at Bridge St and end just east of Exit 305. Exit 306 was removed to simplify and reduce the number of exits within the corridor.

At the SR 191 Interchange (Exit 307), the EB on and off ramps to I-80 have been relocated to tie into the PA-611 Bridge. The new locations of these ramps reduce overall impacts as well as pull the EB and WB movement's closer together.

Alternative 2D

In comparison to Phase I, Alternative 2D is similar to Alternative 1B. Interchange improvements will occur at the SR 611 Interchange (Exit 303), US 209/Business, 209/Dreher Avenue Interchanges (Exits 304, 305, and 306), and SR 191 Interchange (Exit 307).

Pennsylvania Department of Transportation Interstate 80 Reconstruction Preliminary Noise Analysis Monroe County, PA The SR 611 Interchange (Exit 303) diamond configuration was moved west to tie into the main intersection with the shopping center on PA-611. Improvements on PA-611 will extend east and tie into the existing section.

At the US 209/Business 209/Dreher Avenue Interchanges (Exits 304, 305, and 306), significant horizontal and vertical changes have occurred for ramps and the mainline. With Exit 303 pushed to the west, there is now adequate spacing to place the I-80 WB exit ramp to PA-611 at Exit 303 rather than begin it at Exit 304. Similarly, the improvements on West Main St are the same as Alternative 2B, which will begin at Bridge St and end east of Exit 305. Exit 305 is identical to Alternative 2B. Exit 306 was removed to simplify and reduce the number of exits within the corridor.

At the SR 191 Interchange (Exit 307), the EB on and off ramps to I-80 have been relocated to tie into the PA-611 Bridge. The new locations of these ramps reduce overall impacts as well as pull the EB and WB movement's closer together.

It should be noted that the above alternatives considered in this analysis are based on the preliminary engineering plans that were on display during the December 2014 open-house meetings. Since December 2014, several minor modifications to the alignments have occurred and are not included in this study. Most of the modifications are to Alternative 2D; however, minor modification to the roadway profile for CD road, between Main Street and Dreher Avenue, have also been implemented.

IV. Noise Monitoring Methodology and Results

The preliminary noise analysis was initiated by studying the project area and thoroughly identifying all noise-sensitive land uses within the project corridor. Noise-sensitive land uses included in this analysis consist of FHWA/PennDOT defined activity Category B and Category C land uses. However, Category E and Category G land uses are also present within the project study area. According to FHWA/PennDOT procedures, Category B and Category C receptor sites are particularly sensitive to potential noise impacts associated with transportation improvement projects. *Table 1* contains the definitions of each Land Use Activity Category.

The selection of noise-sensitive land uses and noise monitoring locations was guided by the existing alignment of I-80 and the proposed widening design, including interchange reconfiguration. In order to determine existing noise levels within the project area, noise monitoring was conducted at 30 representative noise-sensitive receptor sites. *Figure 2-1 through Figure 4-5* shows the project area and the locations of the 30 noise monitoring sites. Short-term monitoring sites are designated with an "R" in the site identification (e.g., 1-R1) number, versus an "M" for "modeling-*only*" sites (e.g., M1A).

Noise monitoring was performed at each of the selected noise-sensitive receptors using Rion NL-42 Sound level meters. Readings were taken on the A-weighted scale and reported in decibels (dBA). The noise monitoring equipment meets all requirements of the American National Standard Specifications for Sound Level Meters, ANSI S1.4-1983 (R1991), Type 2, and meets all requirements as defined by FHWA. Noise Monitoring was conducted in accordance with the methodologies contained in FHWA-PD-96-046, *Measurement of Highway-Related Noise*, (FHWA, May 1996). Copies of the noise meter calibration certificates are included within the Appendices of the report.

Noise monitoring was conducted at each location in order to thoroughly represent existing, worst-case noise levels at the noise-sensitive locations throughout the project corridor. 24-hour noise monitoring was not completed for the project since this is not a typical commuter route with a defined noise peak. In general, noise levels remain consistent throughout the day. However, congestion does periodically occur and therefore attempts were made to avoid these times and to have the noise monitoring represent worst-case, free flow conditions along the corridor.

Short-term noise monitoring was performed during free-flow conditions for the purposes of noise model validation and not to predict noise impacts. As such, in some cases, the short-term noise monitoring may actually occur during a typical "off-peak" period of the day. Noise monitoring was conducted at each site for a 10-minute duration. Although noise monitoring durations can varying from project to project, a 10-minute duration was considered appropriate for this project since traffic was flowing freely throughout the monitoring session.

Noise monitoring was conducted between the 16th and the 23rd of July, 2013. During the monitoring sessions, noise level data was recorded at 10-second intervals for the 10minute duration of each test. Data collected by the sound analyzers includes time, average noise level (Lav), maximum noise level (Lmax), and instantaneous peak noise level (Lpk) for each 10-second interval. Additional data collected at each monitoring location included atmospheric conditions, wind speed, background noise sources, and unusual or non-traffic-related noise events. Traffic data (vehicle volume and speed) were also recorded on all roadways which were visible from the monitoring site and significantly contributed to the overall noise level. For noise monitoring and modeling purposes, PennDOT and FHWA guidelines and the FHWA TNM Traffic Noise Model suggest traffic data should be grouped into one of five categories: Cars, Medium Trucks, Heavy Trucks, Busses, and Motorcycles. For this project, traffic was only grouped into one of three categories: cars, medium trucks, and heavy trucks. Supplied traffic data did not include projections for busses and motorcycles and were not included in the analysis. The data collected is only used for model validation purposes and is not used to represent existing worst-case conditions.

The peak-hour noise monitoring results are summarized in *Table 2*. Column 1 provides the descriptor of the noise receptor sites. Column 2 describes the type and number of land uses represented by each receptor site. Column 3 provides the existing, monitored noise level at each of the monitoring locations. As shown in Column 3, existing monitored noise levels throughout the corridor range from 47 to 73 dBA. The main

traffic thoroughfare and dominant noise source in the area is I-80. As expected, land uses in closest proximity to I-80 experience the highest noise levels within the project area.

V. Noise Modeling Methodology and Existing Conditions

Computer modeling is the accepted technique for predicting existing and Design Year noise levels associated with traffic-induced noise. Currently, the FHWA Traffic Noise Model (TNM) 2.5 computer-modeling program is the FHWA-approved highway noise prediction model. The TNM has been established as a reliable tool for representing noise generated by highway traffic. The information applied to the modeling effort includes the following: highway design files (existing, as-built, and proposed design), traffic data, 3-D cut/fill lines, and surveying of terrain. Base mapping and field views were used to identify Activity Category noise-sensitive land uses within the corridor.

The modeling process begins with computer model validation, as per PennDOT requirements. This is accomplished by comparing the monitored noise levels with noise levels generated by the computer model, using the traffic volumes and speeds that were experienced during the monitoring effort. This comparison ensures that reported changes in noise levels between existing and Design Year conditions are due to changes in traffic conditions and not to discrepancies between monitoring and modeling techniques. A difference of 3-dBA or less between the monitored and modeled level is considered acceptable, since this is the limit of change detectable by the typical human ear. *Table 2* provides a summary of the model validation for the I-80 existing conditions. Column 4 is the modeled noise level produced by the traffic volumes and speeds witnessed in the field during the noise monitoring phase. Column 5 represents the difference between the monitored level (Column 3) and the level produced by the model (Column 4).

Because all analyzed receptors show a 3-dBA or less difference between the monitored and modeled noise levels, the model is considered an accurate representation of actual existing conditions throughout the project area. Following calibration of the existing conditions model, additional modeling sites were added to thoroughly predict existing noise levels throughout the project corridor.

Following noise model validation, additional noise modeling was performed for existing conditions using traffic data supplied by traffic engineers. This modeling step was performed to evaluate existing, "worst-case" conditions associated with existing worst-case traffic volumes and composition. Column 6 of *Table 2* provides a summary of worst-case existing noise levels, based on supplied worst-case existing traffic volumes. PM peak traffic volumes were used in the analysis as a worst-case approach. The following discussion is an explanation of the existing noise environment within each evaluated NSA.

NSA A1

Noise Study Area A1 (NSA A1) is located south of I-80 in the western portion of the project area, just west of NSA A. NSA A1 is composed of one monitoring site (R1-A1)

Pennsylvania Department of Transportation Interstate 80 Reconstruction Preliminary Noise Analysis Monroe County, PA and one modeling site along White Stone Corner Road which combined represents three residences. The locations of these receptor sites can be seen in *Figure 2-1*. The existing, monitored noise level within NSA A1 was found to be 63 dBA. As shown in *Table 2*, existing (2013), worst-case noise levels are 64 dBA. As expected, I-80 is the dominant noise source in this area.

NSA A

Noise Study Area A (NSA A) is located south of I-80, in the western portion of the project area, extending from the end of Tanite Road to Palmer Avenue. NSA A contains three monitoring sites (R1 - R3) and four modeling sites, which combined represents approximately 23 residences. The locations of these receptor sites can be seen in *Figure 2-1 and 2-2*. NSA A consists mainly of residential frontage along I-80. Existing, monitored noise levels within NSA A range from 60 to 65 dBA. As shown in Column 6 of *Table 2*, existing (2013), worst-case noise levels are predicted to range from 59 to 68 dBA. As expected, noise levels are highest at receivers in closest proximity to I-80.

NSA B

Noise Study Area B (NSA B) is located just east of NSA A and to the south of I-80. NSA B is composed of residences along Bridge Street and Fairground Circle, in addition to the residences located along Miller Street that are in closest proximity to I-80. NSA B contains three monitoring sites (R4-R6) and six modeling sites, which combined represents approximately 54 residences. The locations of these receptor sites can be seen in *Figure 2-2*. The majority of sensitive receivers within NSA B have I-80 as the dominant noise source. Existing monitored noise levels within NSA B range from 56 to 65 dBA. As shown in Column 6 of *Table 2*, existing (2013), worst-case noise levels are predicted to range from 60 to 70 dBA.

NSA C

Noise Study Area C (NSA C) is located just east of NSA B and south of I-80 and is composed of the residences north of W. Main Street (Business Route 209) along Myrtle Street, Maple Street, Hazel Street, Pearl Street and Pokona Avenue. NSA C also includes the residences south of W. Main Street along Hemlock Road and Honeysuckle Lane. NSA C contains four monitoring sites (R7 - R10) and 19 modeling sites, which represent approximately 57 residences. The locations of these receptor sites can be seen in *Figure 2-2*. Existing, monitored noise levels within NSA C range from 59 to 69 dBA. As shown in Column 6 of *Table 2*, existing (2013), worst-case noise levels are predicted to range from 60 to 70 dBA, with I-80 and W. Main Street being the dominant noise sources in the area.

NSA C2

Noise Study Area C2 (NSA C2) is located east of Route 209 adjacent to Arlington Avenue to the north and King David Road to the east. This area is comprised of single

family homes. NSA C2 contains one monitoring site (R1-C2) and three modeling sites, which combined represent approximately 11 residences. The locations of these receptor sites can be seen in *Figure 2-3*. As shown, most residences within NSA C2 front Route 209 and thus, the dominant noise source for these residences is Route 209. The existing, monitored noise level within NSA C2 is 62 dBA. As shown in Column 6 of *Table 2*, existing (2013), worst-case noise levels are predicted to range from 57 to 66 dBA.

NSA D

Noise Study Area D (NSA D) is located south of I-80 extending from Dreher Avenue to the end of Anna Court. NSA D contains four monitoring sites (R11 – R14) and nine modeling sites which combined represent approximately 22 residencies and one cemetery. The locations of these receptor sites can be seen in *Figure 2-3 and 2-4*. Existing, monitored noise levels within NSA D range from 57 to 71 dBA. As shown in Column 6 of *Table 2*, existing (2013), worst-case noise levels are predicted to range from 55 to 74 dBA. As expected, noise levels are highest at receivers in closest proximity to I-80.

NSA D2

Noise Study Area D2 (NSA D2) is located south of NSA D along Dreher Avenue at the Kautz Street intersection. NSA D2 contains two monitoring sites (R1-D1 and R2-D2) and two modeling sites, which combined represent approximately eight residences. The locations of these receptor sites can be seen in *Figure 2-3*. Existing, monitored noise levels within NSA D2 range from 47 to 48 dBA. As shown in Column 6 of *Table 2*, existing (2013), worst-case noise levels are predicted to range from 56 to 59 dBA.

NSA E

Noise Study Area E (NSA E) is located south of I-80 extending east from Dreher Avenue to Village Drive. NSA E contains four modeling sites, which represent approximately 11 residences. The locations of these receptor sites can be seen in *Figure 2-3 and 2-4*. As shown in Column 6 of *Table 2*, existing (2013), worst-case noise levels are predicted to range from 58 to 60 dBA. Noise levels for NSA E are affected by the traffic on the I-80 ramps and Dreher Avenue.

NSA F

Noise Study Area F (NSA F) is located south of I-80 in the eastern portion of the project area, bordered by Bryant Street on the west and Park Avenue (Route 611) on the east. NSA F contains three monitoring sites (R15 – R17) and seven modeling sites, which combined represent approximately 31 residences. The locations of these receptor sites can be seen in *Figure 2-4* NSA F consists of residential homes along I-80 and the ramps for Exit 307. Existing, monitored noise levels within NSA F range from 58 to 73 dBA. As shown in Column 6 of *Table 2*, existing (2013), worst-case noise levels are predicted

Pennsylvania Department of Transportation Interstate 80 Reconstruction Preliminary Noise Analysis Monroe County, PA to range from 55 to 73 dBA. As expected, noise levels are highest at receivers in closest proximity to I-80.

NSA G

Noise Study Area G (NSA G) is located south of I-80 in the eastern portion of the project area, bordered by Park Avenue (Route 611) to the west, Lenox Street to the South, and Broad Street to the east. NSA G contains one monitoring site (R18) and three modeling sites, which combined represent approximately 10 residences. The locations of these receptor sites can be seen in *Figure 2-5*. The existing, monitored noise level within NSA G is 71 dBA. As shown in Column 6 of *Table 2*, existing (2013), worst-case noise levels are predicted to range from 52 to 75 dBA. As expected, noise levels are highest at receivers in closest proximity to I-80.

NSA H

Noise Study Area H (NSA H) is located south of I-80 in the eastern most portion of the project area, bordered by Broad Street to the west and Storm Street to the east, composed of residences located along Colbert Street. NSA H contains three monitoring sites (R19 – R21) and ten modeling sites, which combined represent approximately 33 residences. The locations of these receptor sites can be seen in *Figure 2-5*. Existing, monitored noise levels within NSA H range from 51 to 69 dBA. As shown in Column 6 of *Table 2*, existing (2013), worst-case noise levels are predicted to range from 52 to 70 dBA. As expected, noise levels are highest at receivers in closest proximity to I-80.

NSA I

Noise Study Area I (NSA I) is located north of I-80 in the eastern most portion of the project area just east of Broad Street. NSA I contains one modeling site, which currently represents a medical office building. The locations of the receptor site can be seen in *Figure 2-5*. At the initial time of the field survey, homes were present in this NSA. However, based on recent aerial inspections it appears that these homes have been razed and replaced with the medical office building. No areas of common outdoor use are present at this location. Therefore, there are no longer any noise sensitive receptors in NSA I, thus eliminating it from further investigation.

NSA J

Noise Study Area J (NSA J) is located north of I-80 just west of NSA I. It contains residential units along Ann Street from S. 7th Street to Broad Street. NSA J contains one monitoring site (R22) and two modeling sites, which combined represent approximately 10 residences. The locations of these receptor sites can be seen in *Figure 2-5*. The existing, monitored noise level within NSA J is 59 dBA. As shown in Column 6 of *Table 2*, existing (2013), worst-case noise levels are predicted to range from 65 to 66 dBA. As expected, noise levels are highest at receivers in closest proximity to I-80.

NSA J consists mainly of residential land uses along I-80; however, the Ann Street Park is also located in this NSA. This park was not initially monitored during the preliminary phase of the project. A preliminary assumption of 100 people at one half hour use per day has been determined for the use factor of this park. Based on the "Trail" adjustments located in Table 2, Appendix E, of PennDOT Pub 24, the applicable criteria associated with this particular Category C land use resulted in an Equivalent Residential Units (ERU's) value of 0.013 for one grid point based on the size of the property. As such, the Ann Street Park in NSA J would represent a total of less than one ERU. Regardless of noise impacts, the Ann Street Park only provides 0.013 ERUs (or equivalent to 1.3% of one residence) toward noise barrier reasonableness. Furthermore, when qualitatively evaluating a noise barrier along Broad Street, a minimum barrier would require approximately 200 feet in length at a minimum height of 10 feet and would yield 2,000 total square feet. Considering this minimum barrier scenario, the barrier would far exceed the maximum square foot per benefited receptor valued of 2000. A complete analysis for the area will be undertaken during the Final Design Phase using final design elements.

NSA J-1

NSA J-1 consists of the Rotary Creek Park. This park was not initially monitored during the preliminary phase of the project. A preliminary assumption of 15 people at one half hour use per day has been determined for the use factor of this park. This assumption assumes that the park is primarily used for fishing. Based on the "Trail" adjustments located in Table 2, Appendix E, of PennDOT Pub 24, the applicable criteria associated with this particular Category C land use resulted in an ERU value of .01 for seven grid points. The Rotary Creek Park in NSA J-1 would represent a total of less than one ERU. As such, any length of wall in the area would exceed the reasonableness criteria of 2,000 square feet per benefit. A complete analysis for the area will be undertaken during the Final Design Phase using final design elements. Noise mitigation for NSA J-1 may be warranted and feasible, but would not reasonable at this time, based on the above ERU calculation. A complete analysis for the area will be undertaken during the Final Design Phase using final design elements.

NSA K

Noise Study Area K (NSA K) is located north of I-80 and represents the Stroudsburg Cemetery (a Category C land use). NSA K contains 36 modeling sites, determined by the grid method noted in Appendix E of PennDOT Pub 24. Each modeling site represents approximately .0037 Equivalent Residential Units (ERUs) determined by the applicable criteria associated with this Category C land use under the "Cemetery 2" criteria. The locations of these receptor sites can be seen in *Figure 2-4*. As shown in Column 6 of *Table 2*, existing (2013), worst-case noise levels are predicted to range from 59 to 70 dBA, with I-80 being the dominant noise source in the area.

NSA L

Noise Study Area L (NSA L) is located north of I-80, bordered by NSA K to the east and Dreher Avenue to the west. NSA L contains three modeling sites, which combined represent approximately five residences. The locations of these receptor sites can be seen in *Figure 2-4*. As shown in *Table 2*, existing (2013), worst-case noise levels are predicted to range from 61 to 63 dBA. As expected, noise levels are highest at receivers in closest proximity to I-80.

NSA M

Noise Study Area M (NSA M) is located north of I-80, bordered by Dreher Avenue to the east, W Main Street to the north, and Beers Street to the west. NSA M contains four monitoring sites (R23 – R26) and 12 modeling sites, which combined represent approximately 51 residences. The locations of these receptor sites can be seen in *Figure 2-4*. Existing, monitored noise levels within NSA M range from 64 to 65 dBA. As shown in Column 6 of *Table 2*, existing (2013), worst-case noise levels are predicted to range from 65 to 75 dBA. As expected, noise levels are highest at receivers in closest proximity to I-80.

NSA N

Noise Study Area N (NSA N) is located north of I-80 and south Rt. 611 in the western portion of the project area. NSA N contains one modeling site, which represents approximately four (Category E) commercial land uses. The locations of these receptor sites can be seen in *Figure 2-2*. As shown in Column 6 of *Table 2*, the existing (2013), worst-case noise level is predicted to be 75 dBA. Traffic along I-80 and N. 9th Street are the dominant noise sources.

There are no "official" outdoor use areas within NSA N; however, it is still unclear if any apartments are present within the commercial properties. Final determination and reanalysis will be made in the final design phase of the project.

NSA O

Noise Study Area O (NSA O) is located north of I-80 in the western most portion of the project area. NSA O contains one modeling site, which represents one residence. The locations of this receptor site can be seen in *Figure 2-1*. As shown in Column 6 of *Table 2*, the existing (2013), worst-case noise level is predicted to be 71 dBA.

VI. Evaluation of Design Year Noise Levels & Noise Impact Assessment

Following the development of the existing conditions model and the prediction of Existing (2013) noise levels, the assessment continued with the projection of Design Year (2045) noise levels. This task was accomplished by accounting for the proposed

improvements and applying Design Year (2045) traffic volumes and composition to the validated computer model. The proposed improvements should be considered conceptual and preliminary in nature. The proposed improvements are shown on *Figure 2-1 through Figure 4-5*. Design Year (2045) Build noise levels were predicted with the conceptual improvements in place and in use.

Design Year (2045) noise levels were also modeled for the No-Build alternative for comparative purposes to Build conditions. The No-Build alternative was modeled with the assumption that the roadway improvements proposed, as part of the PennDOT project, would not be in place in the Design Year (2045) of the project, but the existing roadways would carry Design Year traffic volumes, speeds and composition. The noise levels associated with the No-Build modeling analysis are summarized in Column 8 of *Table 2*. No-Build noise levels are projected to approach or exceed the FHWA/PennDOT NAC at 66 sensitive receptor sites, representing 151 Category B, Category C, and Category E land uses.

The next step in the noise analysis is to project Design Year (2045) noise levels for Alternatives 2A, 2B, and 2D and to determine if receptors would approach or exceed the NAC. If the criteria are approached or exceeded at any receptor, noise abatement would be considered and evaluated in an attempt to reduce Design Year noise levels. The noise levels associated with the Build condition modeling analysis are summarized in Columns 9 through 11 of *Table 2*. As shown, Design Year (2045) Build condition noise levels are projected to approach or exceed the NAC within 15 of the 18 NSAs for Alternative 2A, 11 of the 18 NSAs for Alternative 2B and 12 of the 18 NSAs for Alternative 2D.

The information applied to the Design Year modeling effort includes the following: proposed preliminary design roadway improvements, and traffic data derived from modeling efforts for Design Year (2045) Build conditions. Base mapping and field views were used to further identify noise-sensitive land uses and terrain that shields noise levels considerably within the project corridor. The Design Year (2045) Build conditions model was created by adding the proposed roadway improvements to the existing computer model and accounting for proposed roadway changes in vertical and horizontal alignment.

Design Year (2045) traffic volumes, vehicle composition, and speeds were assigned to all existing and proposed roadways. All traffic data used in the noise analyses were derived from traffic engineering studies for the project.

The following discussions present a summary of the Design Year (2045) noise levels throughout the project corridor. NSA boundaries can be referenced on **Figures 2-1 through 2-5** (Alternative 2A), **Figures 3-1 through 3-5** (Alternatives 2B), and **Figures 4-1 through 4-5** (Alternative 2D).

Since the initial development of the preliminary engineering, changes have been made to Alternative 2D that is not shown on the noise project mapping. Improvements to the auxiliary lane between Exit 306 and Exit 307 (eastbound) were since incorporated.

Although these changes have not been modeled under the Preliminary Design Noise Analysis, it is assumed there will be minimal impacts to the predicted noise levels in NSA's E, F, K, and L. However, a more detailed evaluation will be performed once an Alternative is selected and final engineering is complete.

NSA A1

NSA A1 Design Year (2045) Build noise levels for Alternative 2A are predicted to range from 65 to 67 dBA. One receptor site representing one residence shows predicted impacts as a result of the Alternative 2A scenario. Design Year (2045) Build noise levels for Alternative 2B is predicted to be 67 dBA for both receptors. Two receptor sites representing three residences show predicted impacts as a result of the Alternative 2B scenario. Design Year (2045) Build noise levels for Alternative 2D are predicted to range from 65 to 66 dBA. One receptor site representing one residence shows a predicted impact as a result of the Alternative 2D scenario. Noise levels are highest at those sites in closest proximity to I-80; the dominant noise source in the area. Since Design Year noise levels exceed the NAC for all alternatives, noise mitigation for NSA A1 is warranted and will be discussed in the following sections of this report.

NSA A

NSA A Design Year (2045) Build noise levels for Alternative 2A are predicted to range from 63 to 69 dBA. Four receptor sites representing 14 residence show predicted impacts as a result of the Alternative 2A scenario. Design Year (2045) Build noise levels for Alternative 2B are predicted to range from 61 to 68 dBA. One receptor site representing three residences show predicted impacts as a result of the Alternative 2B scenario. Design Year (2045) Build noise levels for Alternative 2D are predicted to range from 61 to 67 dBA. One receptor site representing two residences show a predicted impact as a result of the Alternative 2D scenario. Noise levels are highest at those sites in closest proximity to I-80; the dominant noise source in the area. Since Design Year noise levels exceed the NAC for all alternatives, noise mitigation for NSA A is warranted and will be discussed in the following sections of this report.

NSA B

NSA B Design Year (2045) Build noise levels for Alternative 2A are predicted to range from 62 to 70 dBA. Six receptor sites representing 40 residences show predicted impacts as a result of the Alternative 2A scenario. Design Year (2045) Build noise levels for Alternative 2B are predicted to range from 56 to 58 dBA, resulting in no noise impacts. Three receptor sites representing 20 residences are assumed to be acquired under the Alternative 2B condition. Design Year (2045) Build noise levels for Alternative 2D are predicted to range from 62 to 64 dBA, resulting in no noise impacts. Two receptor sites representing 18 residences are assumed to be acquired under the Alternative 2D condition. Noise levels are highest at those sites in closest proximity to I-80; the dominant noise source in the area. The properties assumed to be acquired were not included in the mitigation evaluation. Since Design Year noise levels exceed the NAC

for Alternative 2A, noise mitigation for NSA B is warranted and will be discussed in the following sections of this report.

NSA C

NSA C Design Year (2045) Build noise levels for Alternative 2A are predicted to range from 64 to 74 dBA. Eighteen receptor sites representing 42 residences show predicted impacts as a result of the Alternative 2A scenario. In addition, one receptor representing one residence is assumed to be acquired under Alternative 2A. Design Year (2045) Build noise levels for Alternative 2B are predicted to range from 63 to 70 dBA. Thirteen receptor sites representing 33 show predicted impacts as a result of the Alternative 2B scenario. In addition, three receptors representing three residences are assumed to be acquired under Alternative 2B. Design Year (2045) Build noise levels for Alternative 2B. Design Year (2045) Build noise levels for Alternative 2B. Design Year (2045) Build noise levels for Alternative 2B are predicted to range from 63 to 68 dBA. Six receptor sites representing 14 residences show predicted impacts as a result of the Alternative 2D scenario. In addition, two receptors representing two residences are assumed to be acquired under the Alternative 2D scenario. Noise levels are highest at those sites in closest proximity to I-80; the dominant noise source in the area. Since Design Year noise levels exceed the NAC for all alternatives, noise mitigation for NSA C is warranted and will be discussed in the following sections of this report.

NSA C2

NSA C2 Design Year (2045) Build noise levels for Alternative 2A are predicted to range from 61 to 71 dBA, however, Alternative 2A improvements end at West Main Street to the north. At this time, noise mitigation is not warranted for this area under Alternative 2A, since this NSA is located beyond the Alternative 2A project limits. Design Year (2045) Build noise levels for Alternative 2B are predicted to range from 58 to 60 dBA, resulting in no noise impacts. Design Year (2045) Build noise levels for Alternative 2D are predicted to range from 58 to 66 dBA. One receptor site representing two residences show predicted impacts as a result of Alternative 2D scenario. Noise levels are highest at those sites in closest proximity to SR 209; the dominant noise source in the area. Since Design Year noise levels exceed the NAC for Alternatives 2D, noise mitigation for NSA C2 is warranted under the 2D Alternative only and will be discussed in the following sections of this report.

NSA D

NSA D Design Year (2045) Build noise levels for Alternative 2A are predicted to range from 61 to 76 dBA. Three receptor sites representing four residences show predicted impacts as a result of the Alternative 2A scenario. In addition, one receptor representing one residence is assumed to be acquired under Alternative 2A. Design Year (2045) Build noise levels for Alternative 2B are predicted to range from 57 to 67 dBA. Five receptor sites representing nine residences show predicted impacts as a result of the Alternative 2B are predicted impacts as a result of the Alternative 2B scenario. In addition, one receptor representing one residence is assumed to be acquired under Alternative 2B. Design Year (2045) Build noise levels for Alternative 2B. Design Year (2045) Build noise levels for Alternative 2D.

are predicted to range from 60 to 68 dBA. Eight receptor sites representing 11 residences and a cemetery show predicted impacts as a result of the Alternative 2D scenario. In addition, one receptor representing one residence is assumed to be acquired under Alternative 2D. Noise levels are highest at those sites in closest proximity to I-80; the dominant noise source in the area. Since Design Year noise levels exceed the NAC for all alternatives, noise mitigation for NSA D is warranted and will be discussed in the following sections of this report.

The existing Hollinshead Cemetery lies adjacent to the residence represented by MD9 in NSA D. The cemetery contains approximately 15 grave sites and is located on a 90ft by 60ft piece of land. Regardless of a potential noise impact, due to the size of the property, the result of the ERU calculation would have minimal effect on the overall reasonableness for a potential noise barrier. As referenced under the Alternatives discussion of the report, this area has had several design modifications since the development of this report that will be reanalyzed during Final Design noise activities.

NSA D2

NSA D2 Design Year (2045) Build noise levels for Alternative 2A are predicted to range from 60 to 63 dBA. Alternative 2A is the only design to have proposed engineering near the area of NSA D2. It is assumed, for this analysis, that future noise levels within this NSA would not be affected by the Alternative 2B or Alternative 2D alignments. Therefore, the future no-build noise levels are assumed for these scenarios. Since Design Year noise levels do not exceed the NAC, noise mitigation for NSA D2 is not warranted and will not be discussed further.

NSA E

NSA E Design Year (2045) Build noise levels for Alternative 2A are predicted to range from 60 to 63 dBA. Design Year (2045) Build noise levels for Alternative 2B are predicted to range from 62 to 64 dBA. Design Year (2045) Build noise levels for Alternative 2D are predicted to range from 61 to 63 dBA. Since Design Year noise levels do not exceed the NAC, noise mitigation for NSA E is not warranted and will not be discussed further.

NSA F

NSA F Design Year (2045) Build noise levels for Alternative 2A are predicted to range from 58 to 75 dBA. Five receptor sites representing 17 residences show predicted impacts as a result of the Alternative 2A scenario. Design Year (2045) Build noise levels for Alternative 2B are predicted to range from 56 to 75 dBA. Four receptor sites representing 12 residences show predicted impacts as a result of the Alternative 2B scenario. Design Year (2045) Build noise levels for Alternative 2D are predicted to range from 57 to 75 dBA. Three receptor sites representing 10 residences show predicted impacts as a result of the Alternative 2D are predicted to range from 57 to 75 dBA. Three receptor sites representing 10 residences show predicted impacts as a result of the Alternative 2D scenario. Since Design Year (2045) noise levels

exceed the NAC for all alternatives, noise mitigation for NSA F is warranted and will be discussed in the following sections of this report.

NSA G

NSA G Design Year (2045) Build noise levels for Alternative 2A are predicted to range from 55 to 77 dBA. One receptor site representing two residences show predicted impacts as a result of the Alternative 2A scenario. Design Year (2045) Build noise levels for Alternative 2B are predicted to range from 54 to 55 dBA. Two receptor sites (R18 and MG3) representing four residences are assumed to be acquired under Alternative 2B. Design Year (2045) Build noise levels for Alternative 2D are predicted to range from 54 to 56 dBA. Two receptor sites (R18 and MG3) representing four residences are assumed to be acquired under Alternative 2B. Design Year (2045) Build noise levels for Alternative 2D are predicted to range from 54 to 56 dBA. Two receptor sites (R18 and MG3) representing four residences are assumed to be acquired under Alternative 2D. Since Design Year noise levels exceed the NAC for Alternatives 2A, noise mitigation for NSA G is warranted under Alternative 2A only and will be discussed in the following sections of this report.

NSA H

NSA H Design Year (2045) Build noise levels for Alternative 2A are predicted to range from 54 to 76 dBA. Three receptor sites representing four residences show predicted impacts as a result of the Alternative 2A scenario. Design Year (2045) Build noise levels for Alternative 2B are predicted to range from 52 to 75 dBA. Six receptor sites representing 10 residences show predicted impacts as a result of the Alternative 2B scenario. In addition, one receptor site (R19) representing two residences are assumed to be acquired under Alternative 2B. Design Year (2045) Build noise levels for Alternative 2D is predicted to range from 47 to 73 dBA. In addition, one receptor site (R19) representing two residences are assumed to be acquired under Alternative 2D. Six receptor sites representing 10 residences show predicted impacts as a result of the Alternative 2D. Six receptor sites representing 10 residences show predicted impacts as a result of the Alternative 2D. Six receptor sites representing 10 residences show predicted impacts as a result of the Alternative 2D. Six receptor sites representing 10 residences show predicted impacts as a result of the Alternative 2D scenario. Since Design Year noise levels exceed the NAC for all alternatives, noise mitigation for NSA H is warranted and will be discussed in the following sections of this report. The properties assumed to be acquired will not be included in the mitigation evaluation.

NSA J

NSA J Design Year (2045) Build noise levels for Alternative 2A are predicted to range from 63 to 67 dBA. Two receptor sites representing seven residences show predicted impacts as a result of the Alternative 2A scenario. Design Year (2045) Build noise levels for Alternative 2B are predicted to range from 64 to 67 dBA. Two receptor sites representing seven residences show predicted impacts as a result of the Alternative 2B scenario. Design Year (2045) Build noise levels for Alternative 2D is predicted to range from 63 to 67 dBA. One receptor site representing three residences show predicted impacts as a result of the Alternative 2D is predicted to range from 63 to 67 dBA. One receptor site representing three residences show predicted impacts as a result of the Alternative 2D scenario. The Ann Street Park is also apart of NSA J; however, the calculated ERU value for the park is insignificant and will not count toward the reasonableness criteria. Since Design Year noise levels exceed the NAC for

all alternatives, noise mitigation for NSA J is warranted and will be discussed in the following sections of this report.

NSA J-1

Rotary Creek Park is currently closed to the public. At this time, it has been determined by the project team that this area will yield very limited public activity and it would prove extremely difficult to determine a proper ERU value. Once appropriate activity use information can be obtained for the park, a full analysis will be completed under the selected Alternative in the Final Design Phase of the project.

NSA K

NSA K Design Year (2045) Build noise levels for Alternative 2A are predicted to range from 65 to 73 dBA. Twenty-five receptor sites show predicted impacts as a result of the Alternative 2A scenario. Design Year (2045) Build noise levels for Alternative 2B are predicted to range from 64 to 71 dBA. Twenty-four receptor sites show predicted impacts as a result of the Alternative 2B scenario. Design Year (2045) Build noise levels for Alternative 2B are predicted to range from 64 to 71 dBA. Twenty-four receptor sites show predicted impacts as a result of the Alternative 2B scenario. Design Year (2045) Build noise levels for Alternative 3D are predicted to range from 64 to 72 dBA. Twenty-six receptor sites show predicted impacts as a result of the Alternative 2D scenario.

Since Design Year noise levels exceed the NAC for all alternatives, noise mitigation for NSA K is warranted and will be discussed in the following sections of this report.

NSA L

NSA L Design Year (2045) Build noise levels for Alternative 2A are predicted to range from 64 to 67 dBA. One receptor site representing two residences show predicted impacts as a result of the Alternative 2A scenario. Design Year (2045) Build noise levels for Alternative 2B are predicted to range from 63 to 65 dBA. Design Year (2045) Build noise levels for Alternative 2D are predicted to range from 63 to 65 dBA. Since Design Year noise levels exceed the NAC for Alternative 2A, noise mitigation for NSA L is warranted under Alternative 2A only and will be discussed in the following sections of this report.

NSA M

NSA M Design Year (2045) Build noise levels for Alternative 2A are predicted to range from 66 to 75 dBA. Sixteen receptor sites representing 51 residences show predicted impacts as a result of the Alternative 2A scenario. Design Year (2045) Build noise levels for Alternative 2B are predicted to range from 66 to 74 dBA. Sixteen receptor sites representing 51 residences show predicted impacts as a result of the Alternative 2B scenario. Design Year (2045) Build noise levels for Alternative 2B scenario. Design Year (2045) Build noise levels for Alternative 2D are predicted to range from 67 to 76 dBA. Sixteen receptor sites representing 51 residences show predicted impacts as a result of the Alternative 2D are predicted to range from 67 to 76 dBA. Sixteen receptor sites representing 51 residences show predicted impacts as a result of the Alternative 2D are predicted to range from 67 to 76 dBA. Sixteen receptor sites representing 51 residences show predicted impacts as a result of the Alternative 2D are predicted to range from 67 to 76 dBA.

levels exceed the NAC for all alternatives noise mitigation for NSA M is warranted and will be discussed in the following sections of this report.

NSA N

NSA N Design Year (2045) Build noise levels for Alternative 2A are predicted to be 75 dBA. One receptor sites representing four commercial properties show predicted impacts as a result of the Alternative 2A scenario. Design Year (2045) Build noise levels for Alternative 2B is predicted to be 77 dBA. One receptor sites representing four commercial properties show predicted impacts as a result of the Alternative 2B scenario. Design Year (2045) Build noise levels for Alternative 2D is predicted to be 77 dBA. One receptor sites representing four commercial properties show predicted impacts as a result of the Alternative 2B scenario. Design Year (2045) Build noise levels for Alternative 2D is predicted to be 77 dBA. One receptor sites representing four commercial properties show predicted impacts as a result of the Alternative 2D scenario. Since Design Year noise levels exceed the NAC for all alternatives noise mitigation for NSA N is warranted and will be discussed in the following sections of this report.

NSA O

NSA O Design Year (2045) Build noise levels for Alternative 2A is predicted to be 74 dBA. One receptor site representing one residence show predicted impacts as a result of the Alternative 2A scenario. Design Year (2045) Build noise levels for Alternative 2B is predicted to be 68 dBA. One receptor site representing one residence show predicted impacts as a result of the Alternative 2B scenario. Design Year (2045) Build noise levels for Alternative 2D is predicted to be 66 dBA. One receptor site representing one residence show predicted impacts as a result of the Alternative 2D scenario. Design Year (2045) Build noise levels for Alternative 2D is predicted to be 66 dBA. One receptor site representing one residence show predicted impacts as a result of the Alternative 2D scenario. Since Design Year noise levels exceed the NAC for all alternatives noise mitigation for NSA O is warranted and will be discussed in the following sections of this report.

VII. Undeveloped Lands

As indicated in PennDOT guidance, if undeveloped land is not permitted for development, a noise analysis is still required to predict future noise levels for use by local planning officials. As shown in *Figures 2-1* through 4-5, there are areas along the project corridor that are comprised of undeveloped wooded areas. As such, modeling receptors were offset every 100 feet up to 550 feet from the edge of shoulder of the new I-80 eastbound alignment to predict the depth of noise impact (66 dBA) from the proposed improvement. As shown in *Table 3*, using site modeling techniques, noise impacts are predicted approximately 500 feet from the proposed eastbound alignment. Local planning officials should exercise caution if any planned developments extend within 500 feet of the proposed improvements since it would be within the impact threshold. During Final Design, coordination should be performed to determine if the status of the undeveloped lands in the project corridor has changed. Only lands where development is permitted by the date of public knowledge (i.e. the NEPA clearance date) will be eligible for abatement consideration.

VIII. Noise Abatement Evaluation and Mitigation

Design Year (2045) noise levels are projected to approach or exceed the FHWA/PennDOT Noise NAC in locations throughout the project corridor. Therefore, in accordance with FHWA/PennDOT procedures, noise abatement considerations are warranted, as discussed above for *Phase 1* of PennDOT's three-phased approach, for the impacted properties within the project corridor.

Where it is determined in *Phase 1* of the noise analysis that consideration of noise abatement is warranted, *Phase 2* and *Phase 3* (feasibility and reasonableness) are then considered. *Phase 2* and *Phase 3* of PennDOT's three-phased approach to considering noise abatement and determining the feasibility and reasonableness of noise barriers are discussed below in detail.

Phase 2: Feasibility Criteria for Noise Barriers

• At least a 5 dBA highway traffic noise reduction at impacted receptors. Per 23 CFR 772 FHWA requires the highway agency to determine the number of impacted receptors required to achieve at least 5 dBA of reduction. PennDOT requires that fifty percent (50%) or more of the impacted receptors experience 5 dBA or more of insertion loss to be feasible; and

• The determination that it is possible to design and construct the noise abatement measure. The factors related to the design and construction include: safety, barrier height, topography, drainage, utilities, and maintenance of the abatement measure, maintenance access to adjacent properties, and general access to adjacent properties (i.e. arterial widening projects).

FHWA and PennDOT guidelines recommend a variety of abatement measures which should be considered in response to transportation-related noise impacts. While noise barriers and/or earth berms are generally the most effective form of noise abatement, additional abatement measures exist which have the potential to provide considerable noise reductions, under certain circumstances. A brief depiction of PennDOT-approved noise abatement options is provided below:

• Construction of noise barriers, including acquisition of property rights, either within or outside the highway right-of-way. Landscaping is not a viable noise abatement measure.

• Traffic management measures including, but not limited to, traffic control devices and signing for prohibition of certain vehicle types, time-use restrictions for certain vehicle types, modified speed limits, and exclusive lane designations.

• Alteration of horizontal and vertical alignments.

• Acquisition of real property or interests therein (predominantly unimproved property) to serve as a buffer zone to preempt development which would be adversely impacted by traffic noise. This measure may be included in Type I projects only.

• Noise insulation of Activity Category D land use facilities listed in *Table 1*. Post-installation maintenance and operational costs for noise insulation are not eligible for Federal-aid funding.

Due to the nature of the proposed improvements, traffic control measures were not considered an appropriate solution. Property acquisition to provide noise abatement via a <u>buffer zone was not necessary</u> or supported by the analysis. Therefore, noise barriers and/or earth berms were considered the only form of abatement having the potential to reduce Design Year (2045) noise levels for this project.

Noise walls and earth berms are often incorporated into the highway design in response to identified noise impacts. The use of earth berms is not always an option, due to the excessive space they require adjacent to the roadway corridor. At a standard slope of 2:1, every one foot of berm height would require approximately four feet of horizontal width at the base. This requirement becomes more complex on roadway improvement projects, where residential properties often abut the proposed roadway corridor. In these situations, implementation of earth berms can require considerable property acquisition to accommodate noise abatement. Due to limited right-of-way throughout the proposed roadway corridor and the potential impact to (and acquisition of) adjacent residential properties and local roadways that would be required to provide berms, earth berms were not considered a viable abatement option for this project. Therefore, noise barriers were evaluated in an attempt to reduce Design Year (2045) Build noise levels below criteria.

Phase 3: Reasonableness Criteria for Noise Barriers

A determination of noise barrier reasonableness will include the consideration of the parameters listed below. The parameters used during the NEPA process are also used during the Final Design Phase when making a determination of noise barrier reasonableness. When performing a reasonableness analysis for the NEPA document, some parameters (e.g., desires of the impacted community) would not yet be quantifiable. All of the reasonableness factors must collectively be achieved in order for a noise abatement measure to be deemed reasonable.

• Noise Reduction Design Goals

The design goal is a reasonableness factor indicating a specific reduction in noise levels that PennDOT uses to identify that a noise abatement measure effectively reduces noise. The design goal establishes a criterion, selected by PennDOT that noise abatement must achieve. The design goal is not the same as acoustic feasibility, which is the minimum level of effectiveness of a noise abatement measure. Acoustic feasibility indicates that the noise abatement measure can, at a minimum, achieve a discernible reduction in noise levels.

• Cost-effectiveness

PennDOT's noise barrier cost effectiveness value is based upon a Maximum Square Footage of Abatement per Benefited Receptor (MaxSF/BR) value of 2,000 sq. ft. This MaxSF/BR criterion shall be applied as part of the noise barrier reasonableness determination. It replaces the previously used "Cost per Benefited Receptor" criteria under the previous noise policy.

• Viewpoints of the benefited receptors

PennDOT shall solicit the viewpoints of all benefited receptors and obtain enough responses to document a decision as to whether or not there is a desire for the proposed noise abatement measure. Fifty percent (50%) or more of the respondents shall be required to favor the noise abatement measure in determining reasonableness.

The effectiveness of a noise barrier is measured by examining the barrier's capability to reduce Design Year (2045) Build noise levels. Noise reduction is measured by comparing Design Year pre-and post-barrier noise levels. This difference between unabated and abated noise levels is known as "insertion loss" (IL). It is important to optimize the noise barrier design to achieve the most effective noise barrier in terms of both noise reduction (insertion losses) and cost. Although at least a 5 dBA reduction is required to meet the feasibility criteria, the following tiered noise barrier abatement goals should be used to govern barrier design and optimization.

- It is required that exterior noise levels be reduced by at least 7 dB(A) for at least one benefitted receptor.
- While conforming to the MaxSF/BR criteria, it is desirable to obtain the 7 dB(A) minimum exterior insertion loss for additional impacted receptor sites if justified by a "point of diminishing returns' evaluation.
- While conforming to the MaxSF/BR criteria, it is desirable to provide additional exterior insertion loss above the 7 dB(A) minimum if justified by a "point of diminishing returns' evaluation.
- If possible, it is desirable to reduce future exterior noise levels to the low- 60decibel range (60-63) for Category B and C receptors and the upper-60 dB(A) range (65-68) for Category E receptors.
- If possible, it is desirable to reduce future exterior noise levels back to existing exterior noise levels.

The following discussion presents potential abatement options for NSAs A1, A, B, C, C2, D, F, G, H, J, K, L, M, N and O within the I-80 Reconstruction Project. Where a noise

barrier was evaluated, the effectiveness was measured in terms of achievable IL (reference *Table 4-1 through Table 4-3*).

The following is a preliminary discussion of the evaluated noise barrier system for each of the impacted NSAs under the associated alternative scenario. Noise abatement was evaluated where noise impacts are predicted to occur. The noise evaluation is preliminary and a more detailed analysis will be completed during the Final Design phase of the project using final engineering information. Final noise mitigation recommendations and commitments are not made until the Final Design phase of the project is complete.

The following is a discussion of the Design Year (2045) Build evaluated noise mitigation options for each NSA for which noise mitigation is warranted. As stated earlier, due to space requirements for earth berms, noise barriers were found to be the only feasible form of noise mitigation for the I-80 project area.

NSA A1 – Alternative 2A

A single post-and-panel noise barrier was modeled for NSA A1, under the Alternative 2A scenario. Moving from west to east the barrier was modeled along the eastbound edge-of-shoulder of I-80. *Figure 2-1* displays the location and limits of the preliminary noise barrier.

The preliminary noise barrier was evaluated at heights ranging from 8 to 20 feet. As shown in *Table 4-1*, the preliminary noise barrier evaluated for this area satisfies the feasibility criteria for the impacted receptor at a height of 14 feet. However, noise reduction of at least 7 dBA at one impacted receptor site is not achieved until the barrier height reaches 20 feet. *Table 5-1* shows the preliminary barrier has an average height of 20 feet and length of 1,344 feet, which yields a total area of 26,880 ft². The preliminary barrier system for NSA A1 benefits three residences and has a MaxSF per benefited residence. Therefore, this barrier is considered to be feasible but not reasonable at this time. However, this area will be re-evaluated during the Final Design phase of the project.

NSA A1 – Alternative 2B

A single post-and-panel noise barrier was modeled for NSA A1 under the Alternative 2B scenario. Moving from west to east the barrier was modeled along the eastbound edge-of-shoulder of I-80. *Figure 3-1* displays the location and limits of the preliminary noise barrier.

The preliminary noise barrier evaluated at heights ranging from 8 to 20 feet. As shown in *Table 4-2*, the preliminary noise barrier system evaluated for this area satisfies the feasibility criteria for the impacted receptors at a height of eight feet. However, noise reduction of at least 7 dBA at one impacted receptor site is not achieved until the barrier height reaches 10 feet. *Table 5-2* shows the preliminary barrier has an average height of 10 feet and length of 1,383 feet, which yields a total area of 13,830 ft². The preliminary

barrier system for NSA A1 benefits three residences and has a MaxSF per benefited residence of 4,610, which exceeds the PennDOT limit of 2,000 Max/SF per benefited residence. Therefore, this barrier is considered to be feasible but not reasonable at this time. However, this area will be re-evaluated during the Final Design phase of the project.

NSA A1 – Alternative 2D

A single post-and-panel noise barrier was modeled for NSA A1 under the Alternative 2D scenario. Moving from west to east the barrier was modeled along the eastbound edge-of-shoulder of I-80. *Figure 4-1* displays the location and limits of the preliminary noise barrier.

The preliminary noise barrier evaluated at heights ranging from 8 to 20 feet. As shown in *Table 4-3*, the preliminary noise barrier system evaluated for this area satisfies the feasibility criteria for the impacted receptors at a height of 10 feet. However, noise reduction of at least 7 dBA at one impacted receptor site is not achieved until the barrier height reaches 12 feet. *Table 5-3* shows the preliminary barrier has an average height of 12 feet and length of 1,502 feet, which yields a total area of 18,024 ft². The preliminary barrier system for NSA A1 benefits three residences and has a MaxSF per benefited residence of 6,008, which exceeds the PennDOT limit of 2,000 Max/SF per benefited residence. Therefore, this barrier is considered to be feasible but not reasonable at this time. However, this area will be re-evaluated during the Final Design phase of the project.

NSA A – Alternative 2A

A two barrier post-and-panel noise barrier system was modeled for NSA A under the Alternative 2A scenario. Moving from west to east the barrier was modeled along the eastbound edge-of-shoulder of I-80. *Figure 2-1 and 2-2* displays the location and limits of the preliminary noise barrier.

The preliminary noise barrier was evaluated at heights ranging from 8 to 20 feet. As shown in *Table 4-1*, the preliminary noise barrier system evaluated for this area satisfies the feasibility criteria for the majority of impacted receptors at a height of 10 feet; however, additional barrier optimization would greatly reduce noise levels to below the NAC at many additional receptors within the area. Noise reduction of at least 7 dBA at one impacted receptor site is not achieved until the barrier height reaches 12 feet. *Table 5-1* shows the preliminary barrier has an average height of 12 feet and a combined length of 3,000 feet, which yields a total area of 36,000 ft². The preliminary barrier system for NSA A benefits 18 residences and has a MaxSF per benefited residence of 2,000, which is at the PennDOT limit of 2,000 Max/SF per benefited residence. Under this barrier scenario, 100% of the three impacted receptor sites obtain at least a 7 dBA reduction. Considering these factors, noise abatement for NSA A. Alternative 2A is warranted, feasible, and reasonable at this time. This area will be re-evaluated during the Final Design phase of the project.

NSA A – Alternative 2B

A single post-and-panel noise barrier system was modeled for NSA A under the Alternative 2B scenario. Moving from west to east the barrier was modeled along the eastbound edge-of-shoulder of I-80. *Figure 3-1 and 3-2* displays the location and limits of the preliminary noise barrier.

The preliminary noise barrier system was evaluated at heights ranging from 8 to 20 feet. As shown in *Table 4-2*, the preliminary noise barrier system evaluated for this area satisfies the feasibility criteria for the impacted receptors at a height of 12 feet. However, noise reduction of at least 7 dBA at one impacted receptor site is not achieved until the barrier height reaches 20 feet. *Table 5-2* shows the preliminary barrier system has an average height of 20 feet and length of 2,952 feet, which yields a total area of 59,040 ft². The preliminary barrier system for NSA A benefits three residences and has a MaxSF per benefited residence of 19,680, which exceeds the PennDOT limit of 2,000 Max/SF per benefited residence. Therefore, this barrier is considered to be feasible but not reasonable at this time. However, this area will be re-evaluated during the Final Design phase of the project.

NSA A – Alternative 2D

A single post-and-panel noise barrier system was modeled for NSA A under the Alternative 2D scenario. Moving from west to east the barrier was modeled along the eastbound edge-of-shoulder of I-80. *Figure 4-2* displays the location and limits of the preliminary noise barrier.

The preliminary noise barrier system was evaluated at heights ranging from 8 to 20 feet. As shown in *Table 4-3*, the preliminary noise barrier system evaluated for this area satisfies the feasibility criteria for the impacted receptors at a height of eight feet. However, noise reduction of at least 7 dBA at one impacted receptor site is not achieved until the barrier height reaches 10 feet. *Table 5-3* shows the preliminary barrier system has an average height of 10 feet and length of 959 feet, which yields a total area of 9,590 ft². The preliminary barrier system for NSA A benefits two residences and has a MaxSF per benefited residence of 4,795, which exceeds the PennDOT limit of 2,000 Max/SF per benefited residence. Therefore, this barrier is considered to be feasible but not reasonable at this time. However, this area will be re-evaluated during the Final Design phase of the project.

NSA B – Alternative 2A

A post-and-panel noise barrier was modeled for NSA B under the Alternative 2A scenario. Moving from west to east the barrier was modeled along the eastbound edge-of-shoulder of I-80. *Figure 2-2* displays the location and limits of the preliminary noise barrier.

The preliminary noise barrier was evaluated at heights ranging from 8 to 20 feet. As shown in *Table 4-1*, the preliminary noise barrier evaluated for this area satisfies the feasibility criteria for the majority of impacted receptors at a height of eight feet; however, additional barrier optimization would greatly reduce noise levels to below the NAC at many additional receptors within the area. *Table 5-1* shows the preliminary barrier has an average height of 12 feet and length of 1,761 feet, which yields a total area of 21,132 ft². The preliminary barrier system for NSA B benefits 50 residences and has a MaxSF per benefited residence of 423, which is well within the PennDOT limit of 2,000 Max/SF per benefited residence. Under this barrier scenario, 100% of the seven impacted receptor sites obtain at least 5 dBA decrease, while 86% receive at least a 7 dBA reduction. Considering these factors, noise abatement for NSA B, Alternative 2A is warranted, feasible, and reasonable at this time. This area will be re-evaluated during the Final Design phase of the project.

NSA C – Alternative 2A

A post-and-panel noise barrier was modeled for NSA C under the Alternative 2A scenario. Moving from west to east the barrier was modeled along the eastbound edgeof-shoulder of I-80 from west of NSA C to its termini along the I-80 off-ramp to Hemlock Road. *Figure 2-2* displays the location and limits of the preliminary noise barrier.

The preliminary noise barrier was evaluated at heights ranging from 8 to 20 feet. As shown in *Table 4-1*, the preliminary noise barrier system evaluated for this area satisfies the feasibility criteria for the majority of impacted receptors at a height of 10 feet; however, additional barrier optimization would greatly reduce noise levels to below the NAC at many additional receptors within the area. *Table 5-1* shows the preliminary barrier has an average height of 14 feet and length of 2,575 feet, which yields a total area of 36,050 ft². The preliminary barrier system for NSA C benefits 46 residences and has a MaxSF per benefited residence of 784, which is well within the PennDOT limit of 2,000 Max/SF per benefited residence. Under this barrier scenario, 83% of the 18 impacted receptor sites obtain at least 5 dBA decrease, while 33% receive at least a 7 dBA reduction. Considering these factors, noise abatement for NSA C, Alternative 2A is warranted, feasible, and reasonable at this time. This area will be re-evaluated during the Final Design phase of the project.

NSAs C and D – Alternative 2B

A single continuous post-and-panel noise barrier system was modeled for NSAs C and D under the Alternative 2B scenario. Moving from west to east the barrier was modeled along the eastbound edge-of-shoulder of I-80 from west of NSA C to its termini just east of Dreher Avenue, encompassing both NSA C and NSA D. *Figure 3-2 and 3-4* displays the location and limits of the preliminary noise barrier.

The preliminary noise barrier was evaluated at heights ranging from 8 to 20 feet. As shown in *Table 4-2*, the preliminary noise barrier system evaluated for this area satisfies

the feasibility criteria for the majority of impacted receptors at a height of 14 feet. *Table 5-2* shows the preliminary barrier has an average height of 14 feet and length of 4,172 feet, which yields a total area of 58,408 ft². The preliminary barrier system for NSAs C and D benefits 43 residences and has a MaxSF per benefited residence of 1,358 which is well within the PennDOT limit of 2,000 Max/SF per benefited residence. Under this barrier scenario, 56% of the 18 impacted receptor sites obtain at least 5 dBA decrease, while 22% receive at least a 7 dBA reduction. Considering these factors, noise abatement for NSA C and NSA D, Alternative 2B is warranted, feasible, and reasonable at this time. This area will be re-evaluated during the Final Design phase of the project.

NSAs C and D – Alternative 2D

A single post-and-panel noise barrier was modeled for NSA C2 under the Alternative 2A scenario. Moving from west to east the barrier was modeled along the eastbound edgeof-shoulder of I-80 from west of NSA C to its termini just east of Dreher Avenue, encompassing both NSA C and NSA D. *Figure 4-2 and 4-4* displays the location and limits of the preliminary noise barrier.

The preliminary noise barrier was evaluated at heights ranging from 8 to 20 feet. As shown in *Table 4-3*, the preliminary noise barrier system evaluated for this area satisfies the feasibility criteria for the majority of impacted receptors at a height of 12 feet; however, additional barrier optimization would greatly reduce noise levels to below the NAC at many additional receptors within the area. Noise reduction of at least 7 dBA at one impacted receptor site is not achieved until the barrier height reaches 14 feet. *Table 5-3* shows the preliminary barrier has an average height of 16 feet and length of 4,205 feet, which yields a total area of 67,280 ft². The preliminary barrier system for NSAs C and D benefits 54 residences and has a MaxSF per benefited residence of 1,246 which is well within the PennDOT limit of 2,000 Max/SF per benefited residence. Under this barrier scenario, 77% of the 13 impacted receptor sites obtain at least 5 dBA decrease, while 31% receive at least a 7 dBA reduction. Considering these factors, noise abatement for NSA C and NSA D, Alternative 2D is warranted, feasible, and reasonable at this time. This area will be re-evaluated during the Final Design phase of the project.

NSA C2 – Alternative 2D

A single continuous post-and-panel noise barrier was modeled for NSA C2 under the Alternative 2D scenario. Moving from south to north the barrier was modeled along the northbound edge-of-shoulder of Route 209 just south of NSA C2 to its termini at the start of the Route 209 off-ramp to Main Street. *Figure 4-3* displays the location and limits of the preliminary noise barrier.

The preliminary noise barrier was evaluated at heights ranging from 8 to 20 feet. As shown in *Table 4-3*, the preliminary noise barrier system evaluated for this area satisfies the feasibility criteria for the majority of impacted receptors at a height of eight feet. *Table 5-3* shows the preliminary barrier has an average height of eight feet and length of 655 feet, which yields a total area of 5,240 ft². The preliminary barrier for NSA C2

benefits five residences and has a MaxSF per benefited residence of 1,048, which is well within the PennDOT limit of 2,000 Max/SF per benefited residence. Under this barrier scenario, the impacted receptor obtains at least a 7 dBA reduction. Considering these factors, noise abatement for NSA C2, Alternative 2D is warranted, feasible, and reasonable at this time. This area will be re-evaluated during the Final Design phase of the project.

NSA D – Alternative 2A

A single continuous post-and-panel noise barrier was modeled for NSA D under the Alternative 2A scenario. Moving from west to east the barrier was modeled along the PennDOT right-of-way and transitions to the I-80 eastbound edge-of-shoulder. *Figure 2-3 and 2-4* displays the location and limits of the preliminary noise barrier.

The preliminary noise barrier was evaluated at heights ranging from 8 to 20 feet. As shown in *Table 4-1*, the preliminary noise barrier system evaluated for this area satisfies the feasibility criteria for the majority of impacted receptors at a height of 10 feet. *Table 5-1* shows the preliminary barrier has an average height of 10 feet and length of 1,780 feet, which yields a total area of 17,800 ft². The preliminary barrier for NSA C2 benefits two residences and has a MaxSF per benefited residence of 8,900, which exceeds the PennDOT limit of 2,000 Max/SF per benefited residence. Considering these factors, noise abatement for NSA D, Alternative 2A is warranted, and feasible, but not reasonable. This area will be re-evaluated during the Final Design phase of the project.

NSA F – Alternative 2A

A single continuous post-and-panel noise barrier system was modeled for NSA F under the Alternative 2A scenario. Moving from west to east the barrier was modeled along the top of the cut line between NSA F and the I-80 off-ramp to Route 611. This mitigation location will be determined when final engineering is available. *Figure 2-4* displays the location and limits of the preliminary noise barrier.

The preliminary noise barrier was evaluated at heights ranging from 8 to 20 feet. As shown in *Table 4-1*, the preliminary noise barrier system evaluated for this area satisfies the feasibility criteria for the impacted receptors at a height of eight feet; however, additional barrier optimization would greatly reduce noise levels to below the NAC at many additional receptors within the area. Noise reduction of at least 7 dBA at one impacted receptor site is not achieved until the barrier height reaches 10 feet. *Table 5-1* shows the preliminary barrier has an average height of 10 feet and length of 1,366 feet, which yields a total area of 13,660 ft². The preliminary barrier for NSA F benefits 12 residences and has a MaxSF per benefited residence of 1,138, which is well within the PennDOT limit of 2,000 Max/SF per benefited residence. Under this barrier scenario, 80% of the five impacted receptor sites obtain at least 5 dBA decrease, while 40% receive at least a 7 dBA reduction. Considering these factors, noise abatement for NSA F, Alternative 2A is warranted, feasible, and reasonable at this time. This area will be re-evaluated during the Final Design phase of the project.

NSA F – Alternative 2B

A single continuous post-and-panel noise barrier was modeled for NSA F under the Alternative 2B scenario. Moving from west to east the barrier was modeled along the top of the cut line between NSA F and the I-80 off-ramp to Route 611. This mitigation location will be determined when final engineering is available. *Figure 3-4* displays the location and limits of the preliminary noise barrier.

The preliminary noise barrier was evaluated at heights ranging from 8 to 20 feet. As shown in *Table 4-2*, the preliminary noise barrier evaluated for this area satisfies the feasibility criteria for the impacted receptors at a height of eight feet. *Table 5-2* shows the preliminary barrier has an average height of eight feet and length of 975 feet, which yields a total area of 7,800 ft². The preliminary barrier system for NSA F benefits 12 residences and has a MaxSF per benefited residence of 650, which is well within the PennDOT limit of 2,000 Max/SF per benefited residence. Under this barrier scenario, 100% of the five impacted receptor sites obtain at least 5 dBA decrease, while 20% receive a 7 dBA reduction. Considering these factors, noise abatement for NSA D, Alternative 2B is warranted, feasible, and reasonable at this time. This area will be re-evaluated during the Final Design phase of the project.

NSA F – Alternative 2D

A single continuous post-and-panel noise barrier was modeled for NSA F under the Alternative 2D scenario. Moving from west to east the barrier was modeled along the top of the cut line between NSA F and the I-80 off-ramp to Route 611. This mitigation location will be determined when final engineering is available. *Figure 4-4* displays the location and limits of the preliminary noise barrier.

The preliminary noise barrier was evaluated at heights ranging from 8 to 20 feet. As shown in *Table 4-3*, the preliminary noise barrier evaluated for this area satisfies the feasibility criteria for the impacted receptors at a height of eight feet. *Table 5-3* shows the preliminary barrier has an average height of eight feet and length of 1,019 feet, which yields a total area of $8,152 \text{ ft}^2$. The preliminary barrier system for NSA F benefits 12 residences and has a MaxSF per benefited residence of 679, which is well within the PennDOT limit of 2,000 Max/SF per benefited residence. Under this barrier scenario, 100% of the three impacted receptor sites obtain at least 5 dBA decrease, while 33% receive at least a 7 dBA reduction. Considering these factors, noise abatement for NSA D, Alternative 2D is warranted, feasible, and reasonable at this time. This area will be re-evaluated during the Final Design phase of the project.

NSA G – Alternative 2A

A post-and-panel noise barrier was modeled for NSA G under the Alternative 2A scenario. Moving from west to east the barrier was modeled along the top of the cut line between NSA G and the I-80 eastbound lanes. *Figure 2-5* displays the location and limits of the preliminary noise barrier.

The preliminary noise barrier was evaluated at heights ranging from 8 to 20 feet. As shown in *Table 4-1*, the preliminary noise barrier evaluated for this area satisfies the feasibility criteria for the impacted receptors at a height of 12 feet. Noise reduction of at least 7 dBA at one impacted receptor site is not achieved until the barrier height reaches 18 feet. *Table 5-1* shows the preliminary barrier has an average height of 18 feet and length of 640 feet, which yields a total area of 11,520 ft². The preliminary barrier for NSA G benefits two residences and has a MaxSF per benefited residence of 5,760, which exceeds the PennDOT limit of 2,000 Max/SF per benefited residence. Considering these factors, noise abatement for NSA G, Alternative 2A is warranted and feasible, but not reasonable at this time. This area will be re-evaluated during the Final Design phase of the project.

NSA H – Alternative 2A

A two barrier post-and-panel noise barrier system was modeled for NSA H under the Alternative 2A scenario. Moving from west to east the first barrier was modeled along the top of the cut line between NSA H and the I-80 eastbound lanes. The second barrier was modeled along the I-80 eastbound edge-of-shoulder. *Figure 2-5* displays the location and limits of the preliminary noise barrier.

The preliminary noise barrier was evaluated at heights ranging from 8 to 20 feet. As shown in *Table 4-1*, the preliminary noise barrier system evaluated is not able to satisfy the feasibility criteria, even at a height of 20 feet. Therefore, the barrier for NSA H Alternative 2A is considered to be not feasible at this time. However, this area will be re-evaluated during the Final Design phase of the project.

NSA H – Alternative 2B

A single continuous post-and-panel noise barrier was modeled for NSA H under the Alternative 2B scenario. Moving from west to east the barrier was modeled along the top of the cut line and transitions to the I-80 edge-of-shoulder. *Figure 3-5* displays the location and limits of the preliminary noise barrier.

The preliminary noise barrier was evaluated at heights ranging from 8 to 20 feet. As shown in *Table 4-2*, the preliminary noise barrier system evaluated for this area satisfies the feasibility criteria for the impacted receptors at a height of eight feet. *Table 5-2* shows the preliminary barrier has an average height of 12 feet and length of 1,614 feet, which yields a total area of 19,368 ft². The preliminary barrier for NSA H benefits 15 residences and has a MaxSF per benefited residence of 1,291, which is well within the PennDOT limit of 2,000 Max/SF per benefited residence. Under this barrier scenario, 83% of the six impacted receptor sites obtain at least 5 dBA decrease, while 50% receive at least a 7 dBA reduction. Considering these factors, noise abatement for NSA H, Alternative 2B is warranted, feasible, and reasonable at this time. This area will be re-evaluated during the Final Design phase of the project.

NSA H – Alternative 2D

A single continuous post-and-panel noise barrier was modeled for NSA H under the Alternative 2B scenario. Moving from west to east the barrier was modeled along the top of the cut line and transitions to the I-80 edge-of-shoulder. *Figure 4-5* displays the location and limits of the preliminary noise barrier.

The preliminary noise barrier was evaluated at heights ranging from 8 to 20 feet. As shown in *Table 4-3*, the preliminary noise barrier system evaluated for this area satisfies the feasibility criteria for the impacted receptors at a height of eight feet. *Table 5-3* shows the preliminary barrier has an average height of 12 feet and length of 1,614 feet, which yields a total area of 19,368 ft². The preliminary barrier for NSA H benefits 11 residences and has a MaxSF per benefited residence of 1,761, which is well within the PennDOT limit of 2,000 Max/SF per benefited residence. Under this barrier scenario, 83% of the six impacted receptor sites obtain at least 5 dBA decrease, while 50% receive at least a 7 dBA reduction. Considering these factors, noise abatement for NSA H, Alternative 2D is warranted, feasible, and reasonable at this time. This area will be re-evaluated during the Final Design phase of the project.

NSA J- Alternative 2A

A single continuous post-and-panel noise barrier was modeled for NSA J under the Alternative 2A scenario. Moving from east to west the barrier was modeled along the I-80 on-ramp from Route 191, between Route 191 and Route 611. *Figure 2-5* displays the location and limits of the preliminary noise barrier system.

The preliminary noise barrier was evaluated at heights ranging from 8 to 20 feet. As shown in *Table 4-1*, the preliminary noise barrier system evaluated for this area is not able to satisfy the feasibility criteria for the impacted receptors at a height of 20 feet. Therefore, this barrier is considered to be not feasible at this time. However, this area will be re-evaluated during the Final Design phase of the project.

NSA J – Alternative 2B

A single continuous post-and-panel noise barrier was modeled for NSA J under the Alternative 2D scenario. Moving from east to west the barrier was modeled along the I-80 on-ramp from Route 191, between Route 191 and Route 611. *Figure 3-5* displays the location and limits of the preliminary noise barrier system.

The preliminary noise barrier was evaluated at heights ranging from 8 to 20 feet. As shown in *Table 4-2*, the preliminary noise barrier system evaluated for this area satisfies the feasibility criteria for the impacted receptors at a height of 10 feet. However, noise reduction of at least 7 dBA at one impacted receptor site is not achieved until the barrier height reaches 16 feet. *Table 5-2* shows the preliminary barrier has an average height of 16 feet and length of 853 feet, which yields a total area of 13,648 ft². The preliminary barrier for NSA J benefits six residences and has a MaxSF per benefited residence of 2,275, which is not within the PennDOT limit of 2,000 Max/SF per benefited residence.

Considering these factors, noise abatement for NSA J, Alternative 2B is warranted, feasible, but not reasonable at this time. This area will be re-evaluated during the Final Design phase of the project.

Although the Ann Street Park was not initially modeled during the preliminary phase of the project it is assumed, based on its orientation to I-80 and the impacts to the Ann Street residences, that the park is also impacted. Once an Alternative is selected and engineering is finalized during the Final Design Phase, the Ann Street Park will be fully analyzed and included in the reasonableness calculations. At this time, the NSA J barrier under Alternative 2B is still feasible, but not reasonable, regardless of the parks inclusion.

NSA J – Alternative 2D

A single continuous post-and-panel noise barrier was modeled for NSA J under the Alternative 2D scenario. Moving from east to west the barrier was modeled along the I-80 on-ramp from Route 191, between Route 191 and Route 611. *Figure 4-5* displays the location and limits of the preliminary noise barrier system.

The preliminary noise barrier was evaluated at heights ranging from 8 to 20 feet. As shown in *Table 4-3*, the preliminary noise barrier system evaluated for this area satisfies the feasibility criteria for the impacted receptors at a height of 10 feet. However, noise reduction of at least 7 dBA at one impacted receptor site is not achieved until the barrier height reaches 20 feet. *Table 5-3* shows the preliminary barrier has an average height of 20 feet and length of 853 feet, which yields a total area of 17,060 ft². The preliminary barrier for NSA J benefits six residences and has a MaxSF per benefited residence of 2,843, which is not within the PennDOT limit of 2,000 Max/SF per benefited residence. Considering these factors, noise abatement for NSA J, Alternative 2D is warranted, feasible, but not reasonable at this time. This area will be re-evaluated during the Final Design phase of the project.

Although the Ann Street Park was not initially modeled during the preliminary phase of the project it is assumed, based on its orientation to I-80 and the impacts to the Ann Street residences, that the park is also impacted. Once an Alternative is selected and engineering is finalized during the Final Design Phase, the Ann Street Park will be fully analyzed and included in the reasonableness calculations. At this time, the NSA J barrier under Alternative 2D is still feasible, but not reasonable, regardless of the parks inclusion.

NSA K – Alternatives 2A, 2B and 2D

As discussed in previous sections of this report, the methodology set forth in PennDOT guidance (Appendix E, Table E2) for assessing impacts at Category C sites, each noise receptor in NSA K represents 0.0037 Equivalent Residential Units (ERU). This calculation was based on the Cemetery (Case 2) from Appendix E, Table E2. There are 36 receptors in NSA K, which total 0.1332 ERU(or equivalent to 13% of one residence) toward noise barrier reasonableness. Furthermore, when qualitatively evaluating a noise

barrier along the westbound shoulder of I-80, a minimum barrier would require approximately 1,000 feet in length at a minimum height of 10 feet and would yield 10,000 total square feet. Considering this minimum barrier scenario, the barrier would far exceed the maximum square foot per benefited receptor valued of 2000. Therefore, even if all the receptors are benefited, the barrier would not be reasonable, regardless of the mitigation design under either alternative. Further analysis of NSA K will not be undertaken at this time.

NSA L and M – Alternative 2A

A continuous post-and-panel noise barrier system was modeled for NSAs L and M under the Alternative 2A scenario. The barrier was modeled along the westbound shoulder of I-80 and transitions to the shoulder of the I-80 off-ramp to West Main Street. *Figure 2-4* displays the location and limits of the preliminary noise barrier.

The preliminary noise barrier was evaluated at heights ranging from 8 to 20 feet. As shown in *Table 4-1*, the preliminary noise barrier evaluated for this area satisfies the feasibility criteria for the impacted receptors at a height of 14 feet. *Table 5-1* shows the preliminary barrier has an average height of 14 feet and length of 2,060 feet, which yields a total area of 28,840 ft². The preliminary barrier for NSA L and M benefits 45 residences and has a MaxSF per benefited residence of 641, which is well within the PennDOT limit of 2,000 Max/SF per benefited residence. Under this barrier scenario, 82% of the 17 impacted receptor sites obtain at least 5 dBA decrease, while 53% receive at least a 7 dBA reduction. Considering these factors, noise abatement for NSAs L and M, Alternative 2A is warranted, feasible, and reasonable at this time. This area will be re-evaluated during the Final Design phase of the project.

NSA L and M – Alternative 2B

A two barrier overlapped post-and-panel noise barrier system was modeled for NSAs L and M under the Alternative 2B scenario. Moving from east to west the first barrier was modeled along the westbound edge of shoulder of I-80 and then edge-of-shoulder of the I-80 off-ramp to West Main Street. The second barrier is modeled between the I-80 westbound travel lanes and the I-80 off ramp to West Main Street. *Figure 3-2 and 3-4* displays the location and limits of the preliminary noise barrier system.

The preliminary noise barrier system was evaluated at heights ranging from 8 to 20 feet. As shown in *Table 4-2*, the preliminary noise barrier system evaluated for this area satisfies the feasibility criteria for the impacted receptors at a height of 14 feet. *Table 5-2* shows the preliminary barrier has an average height of 14 feet and length of 2,454 feet, which yields a total area of 34,356 ft². The preliminary barrier system for NSA L and M benefits 45 residences and has a MaxSF per benefited residence of 763, which is well within the PennDOT limit of 2,000 Max/SF per benefited residence. Under this barrier scenario, 81% of the 16 impacted receptor sites obtain at least 5 dBA decrease, while 38% receive at least a 7 dBA reduction. Considering these factors, noise abatement for

NSAs L and M, Alternative 2B is warranted, feasible, and reasonable at this time. This area will be re-evaluated during the Final Design phase of the project.

NSAs L and M - Alternative 2D

A two barrier overlapped post-and-panel noise barrier system was modeled for NSAs L and M under the Alternative 2D scenario. Moving from east to west the first barrier was modeled along the westbound edge of shoulder of I-80 and then edge-of-shoulder of the I-80 off-ramp to West Main Street. The second barrier is modeled between the I-80 westbound travel lanes and the I-80 off ramp to West Main Street. *Figure 4-2 and 4-4* displays the location and limits of the preliminary noise barrier system.

The preliminary noise barrier system was evaluated at heights ranging from 8 to 20 feet. As shown in *Table 4-3*, the preliminary noise barrier system evaluated for this area satisfies the feasibility criteria for the impacted receptors at a height of 10 feet. *Table 5-3* shows the preliminary barrier has an average height of 10 feet and length of 2,756 feet, which yields a total area of 27,560 ft². The preliminary barrier system for NSAs L and M benefits 25 residences and has a MaxSF per benefited residence of 1,102, which is well within the PennDOT limit of 2,000 Max/SF per benefited residence. Under this barrier scenario, 50% of the 16 impacted receptor sites obtain at least 5 dBA decrease, while 25% receive at least a 7 dBA reduction. Considering these factors, noise abatement for NSAs L and M, Alternative 2D is warranted, feasible, and reasonable at this time. This area will be re-evaluated during the Final Design phase of the project.

NSA N – Alternative 2A

A single continuous post-and-panel noise barrier was modeled for NSA N, Alternative 2A. Moving from east to west the noise barrier was modeled along the edge-of-shoulder of the I-80 off-ramp to Route 611. *Figure 2-2* displays the location and limits of the preliminary noise barrier system.

The preliminary noise barrier was evaluated at heights ranging from 8 to 20 feet. As shown in *Table 4-1*, the preliminary noise barrier system evaluated for this area satisfies the feasibility criteria for the impacted receptor at a height of eight feet. *Table 5-1* shows the preliminary barrier has an average height of eight feet and length of 1,065 feet, which yields a total area of 8,520 ft². The preliminary barrier system for NSA N benefits 4 commercial land uses and has a MaxSF per benefited land use of 2,130, which exceeds the PennDOT limit of 2,000 Max/SF per benefited residence. Therefore this barrier is considered feasible but not reasonable. However, this area will be re-evaluated during the Final Design phase of the project.

NSA N – Alternative 2B

A single continuous post-and-panel noise barrier was modeled for NSA N, Alternative 2B. Moving from east to west the noise barrier was modeled along the edge-of-shoulder

of the I-80 off-ramp to Route 611. *Figure 3-2* displays the location and limits of the preliminary noise barrier system.

The preliminary noise barrier was evaluated at heights ranging from 8 to 20 feet. As shown in *Table 4-2*, the preliminary noise barrier system evaluated for this area satisfies the feasibility criteria for the impacted receptor at a height of eight feet. *Table 5-2* shows the preliminary barrier has an average height of eight feet and length of 902 feet, which yields a total area of 7,216 ft². The preliminary barrier system for NSA N benefits 4 commercial land uses and has a MaxSF per benefited land use of 1,804, which is well within the PennDOT limit of 2,000 Max/SF per benefited residence. Under this barrier scenario, the impacted receptor obtains a reduction of 10 dBA satisfying the feasibility criteria and the design goal of receiving at 7 dBA reduction. Considering these factors, noise abatement for NSA N, Alternative 2B is warranted, feasible, and reasonable at this time. This area will be re-evaluated during the Final Design phase of the project.

NSA N – Alternative 2D

A single continuous post-and-panel noise barrier was modeled for NSA N under the Alternative 2D scenario. Moving from east to west the noise barrier was modeled along the edge-of-shoulder of the I-80 westbound lanes. *Figure 4-2* displays the location and limits of the preliminary noise barrier system.

The preliminary noise barrier system was evaluated at heights ranging from 8 to 20 feet. As shown in *Table 4-3*, the preliminary noise barrier system evaluated for this area satisfies the feasibility criteria for the impacted receptors at a height of 10 feet. However, noise reduction of at least 7 dBA at one impacted receptor site is not achieved until the barrier height reaches 12 feet. *Table 5-3* shows the preliminary barrier has an average height of 12 feet and length of 1,065 feet, which yields a total area of 12,780 ft². The preliminary barrier system for NSA N benefits 4 commercial land uses and has a MaxSF per benefited land use of 3,195, which exceeds the PennDOT limit of 2,000 Max/SF per benefited residence. Therefore this barrier is considered feasible but not reasonable. However, this area will be re-evaluated during the Final Design phase of the project.

NSA O – Alternative 2A

A single continuous post-and-panel noise barrier was modeled for NSA O under the Alternative 2A scenario. Moving from east to west the barrier was modeled along the westbound edge-of-shoulder of I-80. *Figure 2-1* displays the location and limits of the preliminary noise barrier system.

The preliminary noise barrier was evaluated at heights ranging from 8 to 20 feet. As shown in *Table 4-1*, the preliminary noise barrier system evaluated for this area satisfies the feasibility criteria for the impacted receptor at a height of 16 feet. However, noise reduction of at least 7 dBA at one impacted receptor site is not achieved until the barrier height reaches 20 feet. *Table 5-1* shows the preliminary barrier has an average height of 20 feet and length of 1,000 feet, which yields a total area of 20,000 ft². The preliminary

barrier system for NSA N benefits one residence and has a MaxSF per benefited residence of 20,000, which exceeds the PennDOT limit of 2,000 Max/SF per benefited residence. Therefore this barrier is considered feasible but not reasonable. However, this area will be re-evaluated during the Final Design phase of the project.

NSA O – Alternative 2B

A single continuous post-and-panel noise barrier was modeled for NSA O, Alternative 2B. Moving from east to west the barrier was modeled along the westbound edge-of-shoulder of I-80. *Figure 3-1* displays the location and limits of the preliminary noise barrier system.

The preliminary noise barrier was evaluated at heights ranging from 8 to 20 feet. As shown in *Table 4-2*, the preliminary noise barrier system evaluated was not able to meet the feasibility criteria even at a height of 20 feet. Therefore this barrier is considered to be neither feasible nor reasonable. However, this area will be re-evaluated during the Final Design phase of the project.

NSA O – Alternative 2D

A single continuous post-and-panel noise barrier was modeled for NSA O, Alternative 2B. Moving from east to west the barrier was modeled along the westbound edge-of-shoulder of I-80. *Figure 4-1* displays the location and limits of the preliminary noise barrier system.

The preliminary noise barrier was evaluated at heights ranging from 8 to 20 feet. As shown in *Table 4-3*, the preliminary noise barrier evaluated for this area is not able to satisfy the feasibility criteria for the impacted receptors at a height of 20 feet. Therefore, this barrier is considered to be not feasible at this time. However, this area will be re-evaluated during the Final Design phase of the project.

In summary, 11 of the 18 NSAs within the project corridor warrant noise mitigation, are feasible for construction of noise barriers, and are reasonable (cost effective) at this time. A summary of the noise impacts, under each alternative, can be referenced in *Table 6*.

IX. Construction Noise

PennDOT is also concerned with noise generated during the construction phase of the project. The use of heavy machinery and construction techniques may cause temporary impacts to noise-sensitive land uses in close proximity to construction work zones.

Based on review of the project area, no significant, long-term construction-related noise impacts are anticipated. Existing noise levels are relatively high along Interstate 80, with significant noise influences from heavy trucks and high traffic volumes; therefore temporary construction noise will be minimal in comparison. Any construction-related

noise impacts that do occur are anticipated to be temporary in nature and would cease at the completion of the project.

To help minimize construction-related noise impacts, the contractor shall use equipment adapted to operate within reasonable noise levels, and will conduct construction work in a responsible manner, to limit annoyance to the occupants of nearby properties.

X. Public Involvement

Public involvement is an integral step to address proposed noise abatement with affected residents, and those who have concerns about increased noise levels as a result of the proposed improvements. The purpose of the public involvement process is to present the noise analysis results to the public, and to receive input on desirable mitigation measures. It is important to establish if the majority of a noise-impacted community is truly in favor of the proposed noise mitigation measures. As part of the reasonableness evaluation, the desires for noise mitigation must be verified. If the majority of a noise-impacted community does not want a noise barrier, PennDOT will not force a barrier on the community. Public meetings are generally used as the appropriate forum to establish the desires of the community and complete the reasonableness evaluation in the form of a noise barrier survey.

In conjunction with the Preliminary Alternatives Analysis phase of the I-80 Section 17M Project, public Open House Plans Displays were held on February 20, 2014 and February 23, 2014 at the Stroudsburg Area High School. A second set of public Open House Plans displays were held on December 4th, 2014 and December 7th, 2014 in the same venue. At both sets of meetings, PennDOT explained that noise studies were being undertaken and that, based on the nature of the roadway and surrounding area, noise barriers might be warranted along some portions of I-80. PennDOT also said that any proposed noise barriers would be shown at future public meetings, but that final determinations on noise walls would not occur until Final Design.

In comments forms submitted at both sets of meetings, between 4 and 5 % of respondents identified noise as one of the most important factors for the project team to consider. One attendee specifically raised a concern about potential negative construction and roadway noise impacts along Bridge Street.

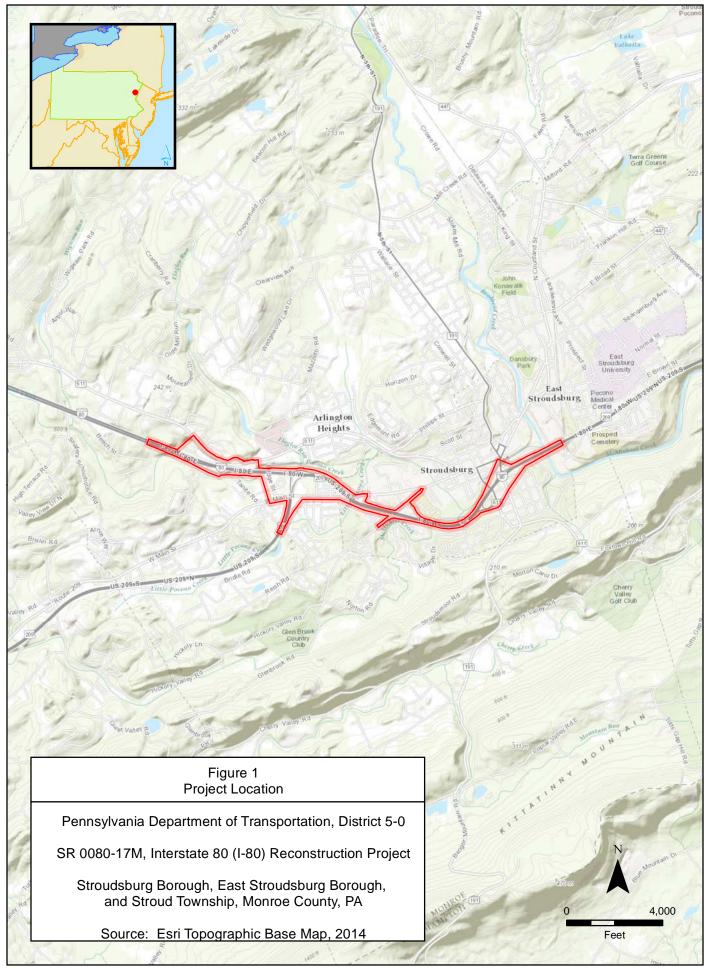
No other public meetings are planned during the Preliminary Design phase. A hearing will be held for the Environmental Assessment if warranted. PennDOT will conduct public involvement activities regarding any proposed noise abatement during the Final Design phase, as required by Publication 24.

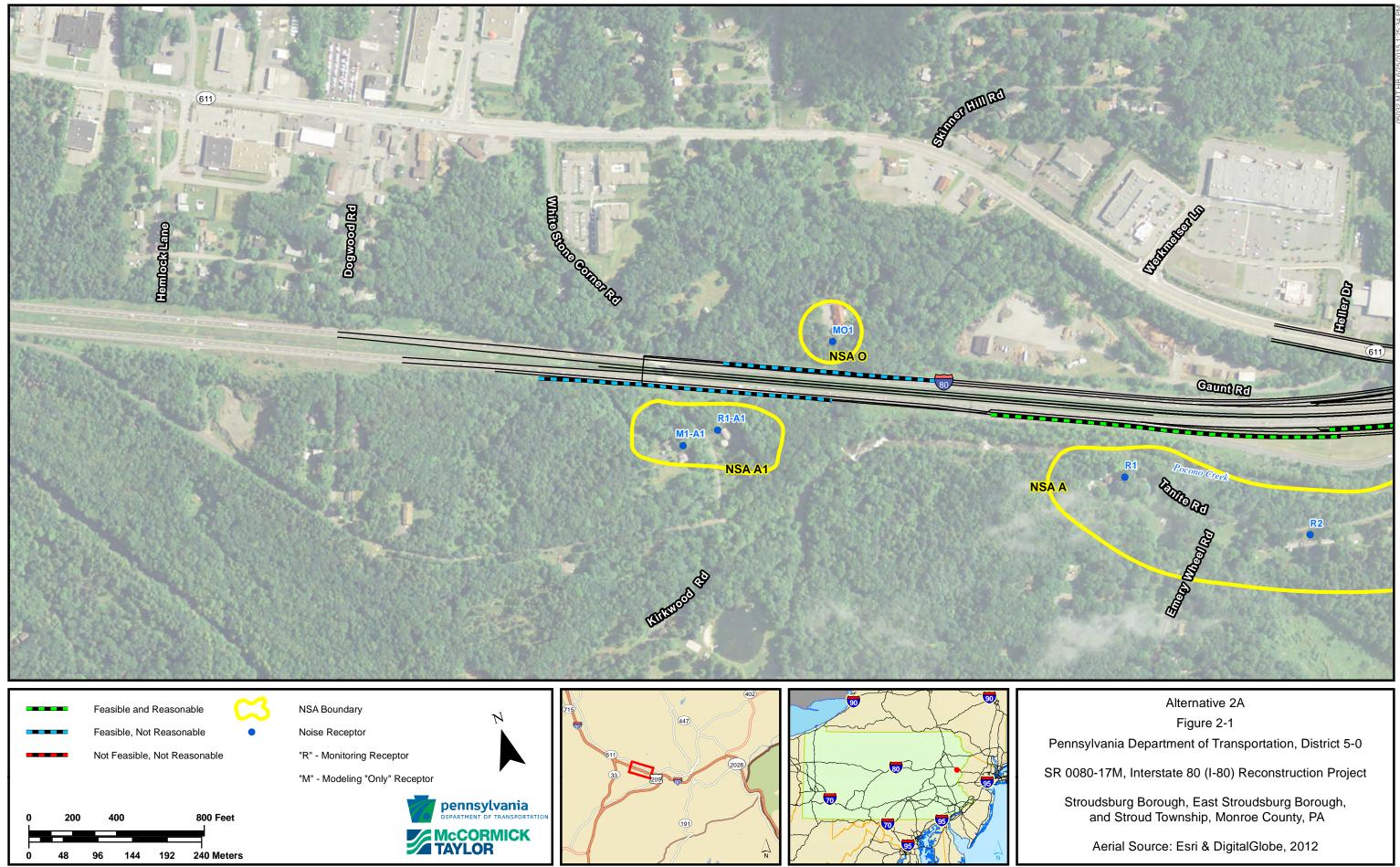
XI. Conclusion

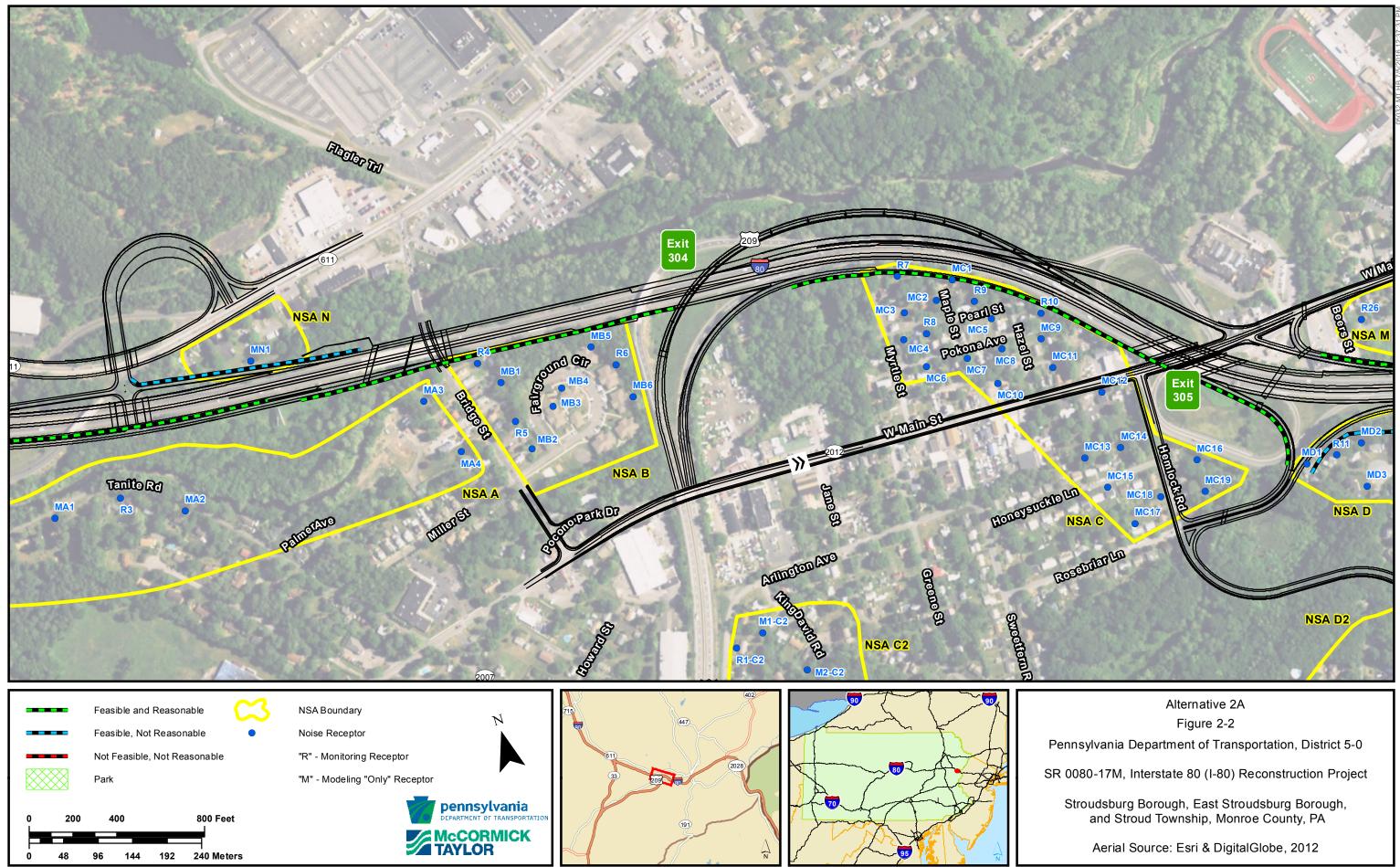
The results of the preliminary noise analysis indicate that Design Year (2045) noise levels are anticipated to exceed the FHWA/PennDOT Noise Abatement Criteria at almost half of the noise-sensitive receptor sites in the project area under all the alternatives. A noise barrier mitigation evaluation concluded by recommending noise barriers for residential communities contained within NSA A, B, C, F, and L and M for Alternative 2A. Under the Alternative 2B scenario, noise barriers are recommended for NSAs C and D, F, H, L and M, and N. Under the Alternative 2D scenario, noise barriers are recommended for NSAs C and D, C2, F, H, and L and M. *Figure 2-1 through Figure 4-5* shows the limits of these barriers. *Tables 5-1* through *Table 5-3* present the noise barrier feasibility and reasonableness summary information for all evaluated NSAs. *Table 6* provides the noise impact summary information for all alternatives considered in the analysis. Therefore, the results of the preliminary noise analysis indicate that noise mitigation is warranted, feasible, and reasonable under all alternative options, as per FHWA/PennDOT procedures. These barriers specifics will be refined and final optimization will occur during the Final Design phase of the project.

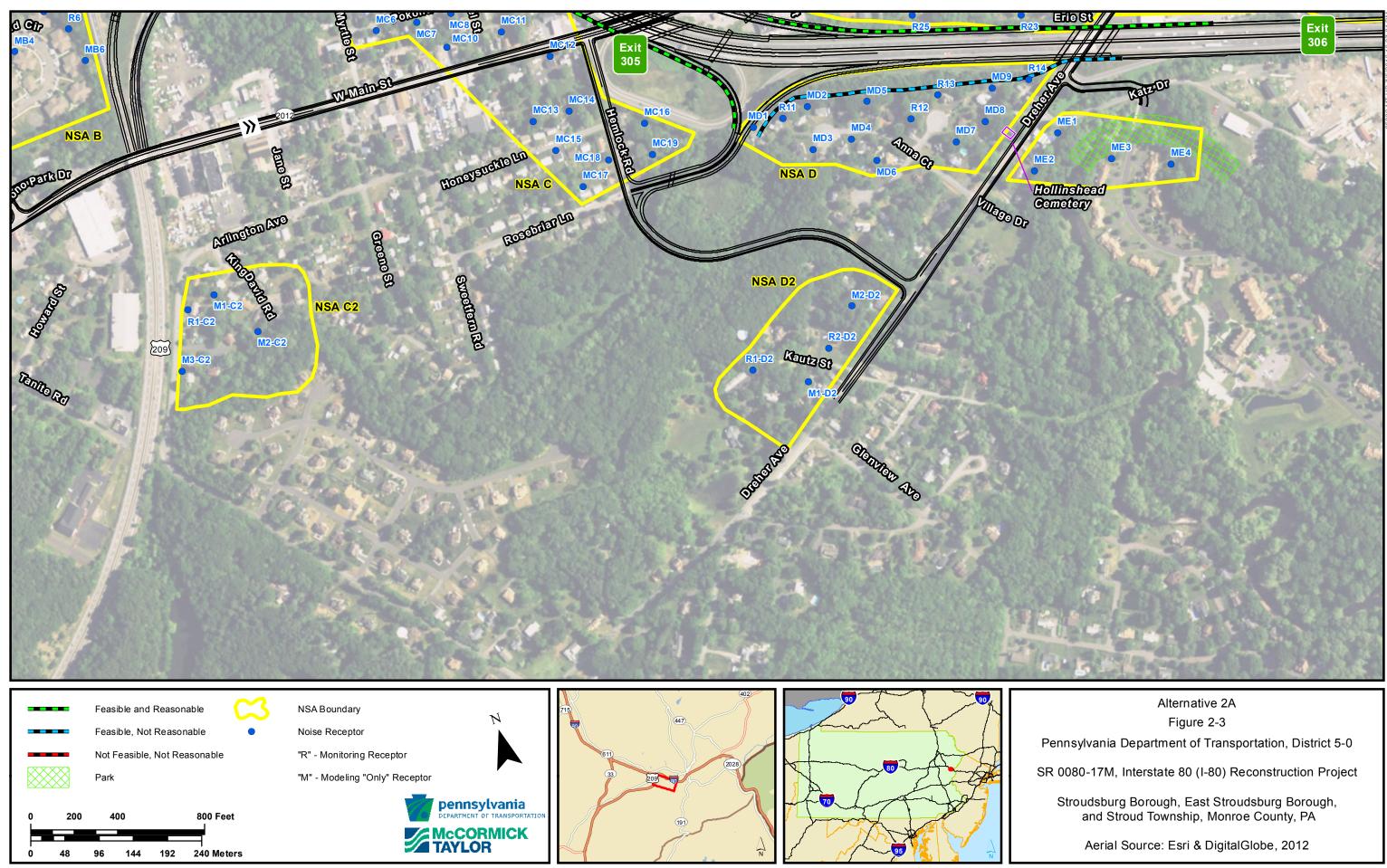
PennDOT is committed to the construction of warranted, feasible, and reasonable highway traffic noise abatement measures at the noise impacted locations identified in this report, contigent upon the following conditions: detailed noise analysis during the Final Design phase; analysis and determination of the feasibility and reasonableness of highway traffic noise abatement measures methodology and criteria; community input regarding desires, types, heights, and locations as well as aesthetic considerations; and safety and engineering aspects as related to the highway user and the adjacent property owner. Final recommendations on the construction of any noise abatement measures will be determined during the completion of the project's Final Design and public involvement processes.

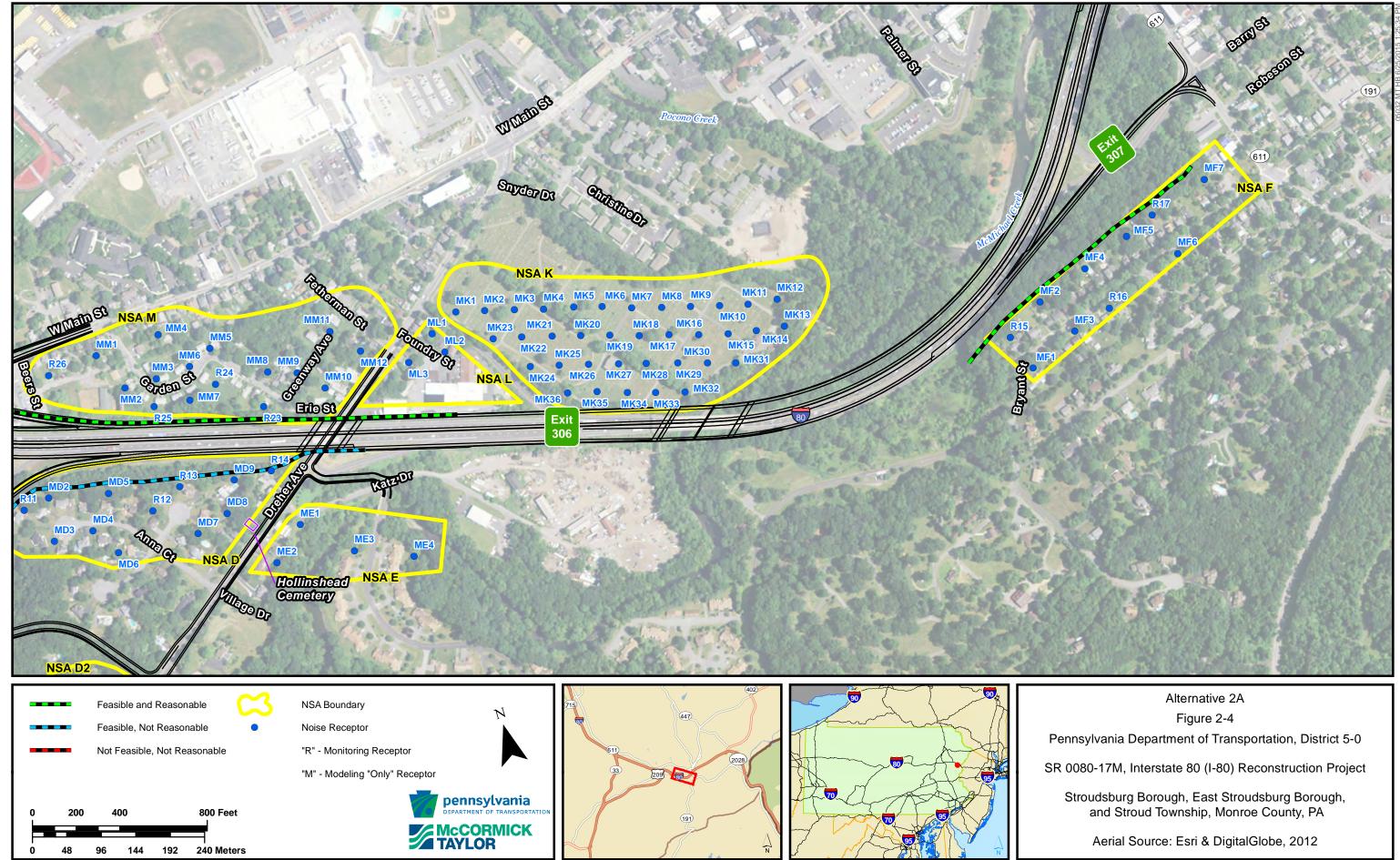


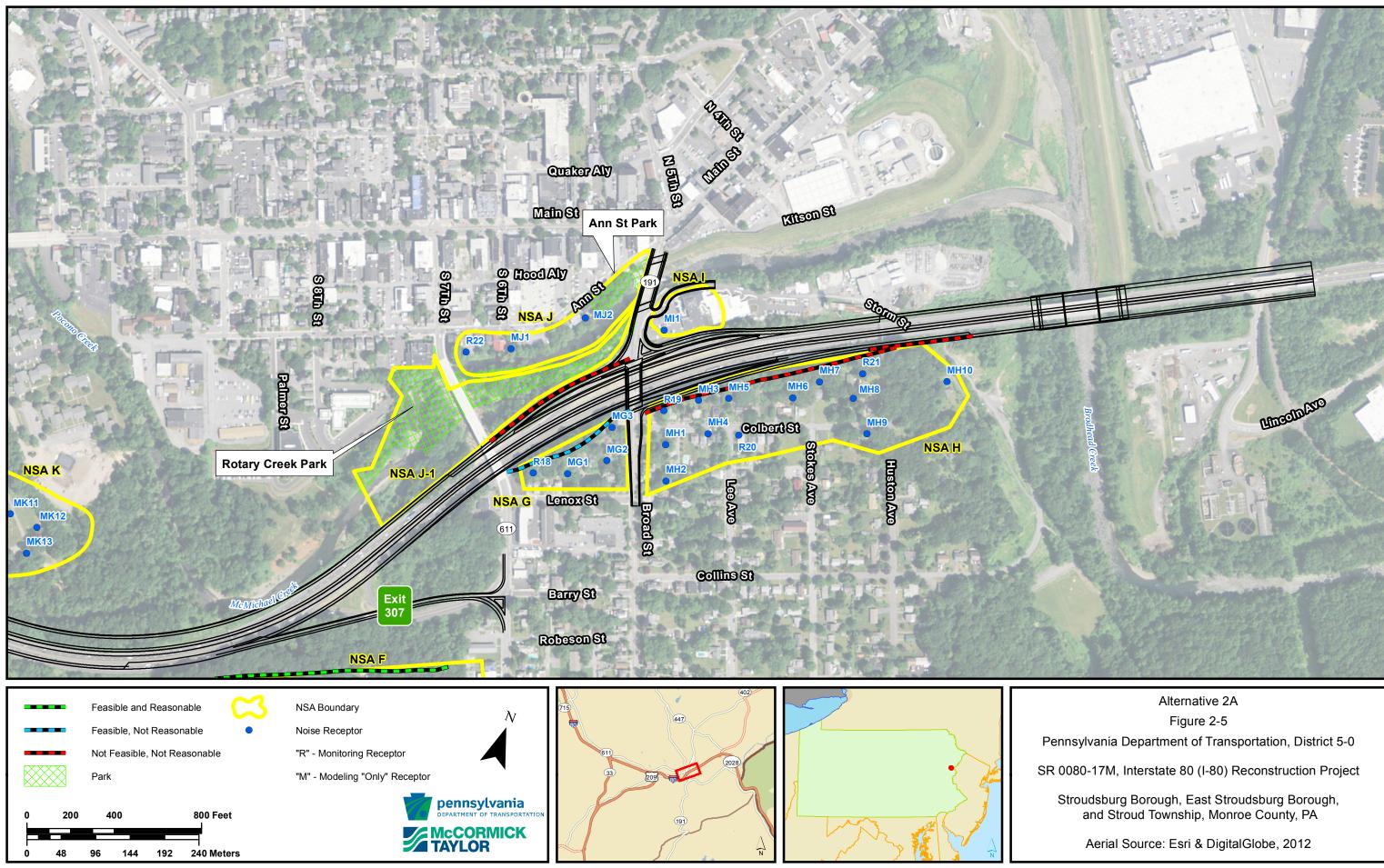


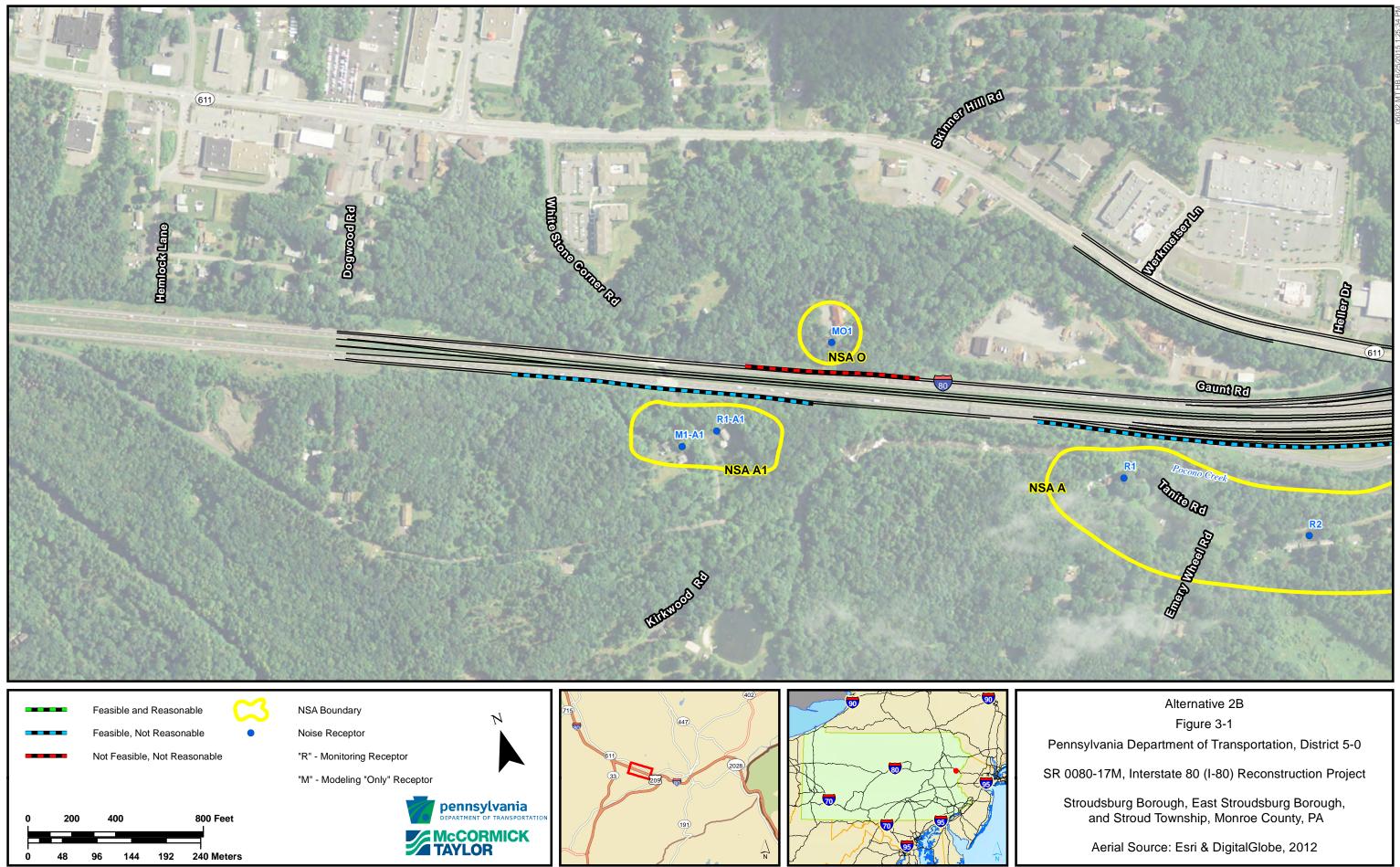


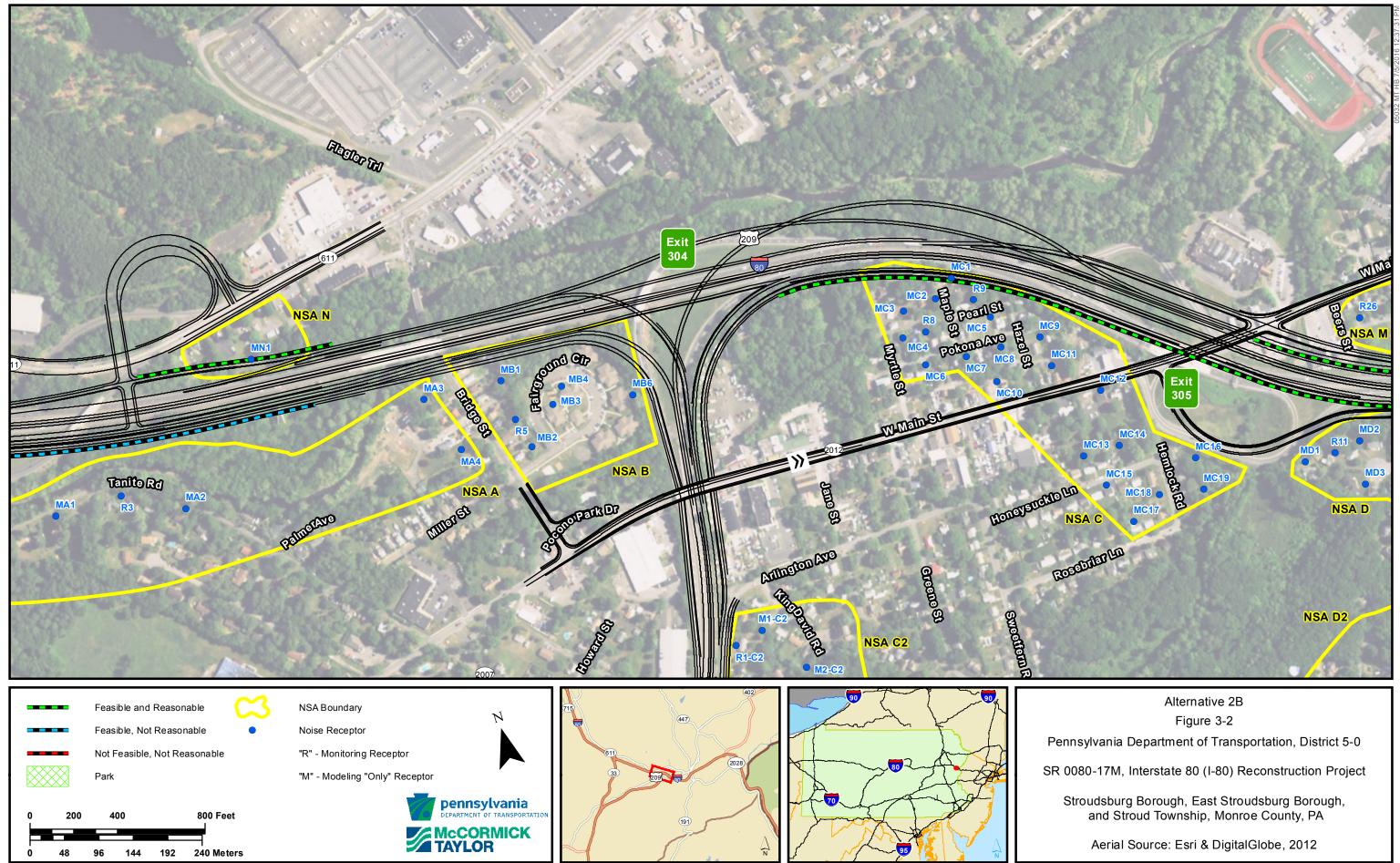


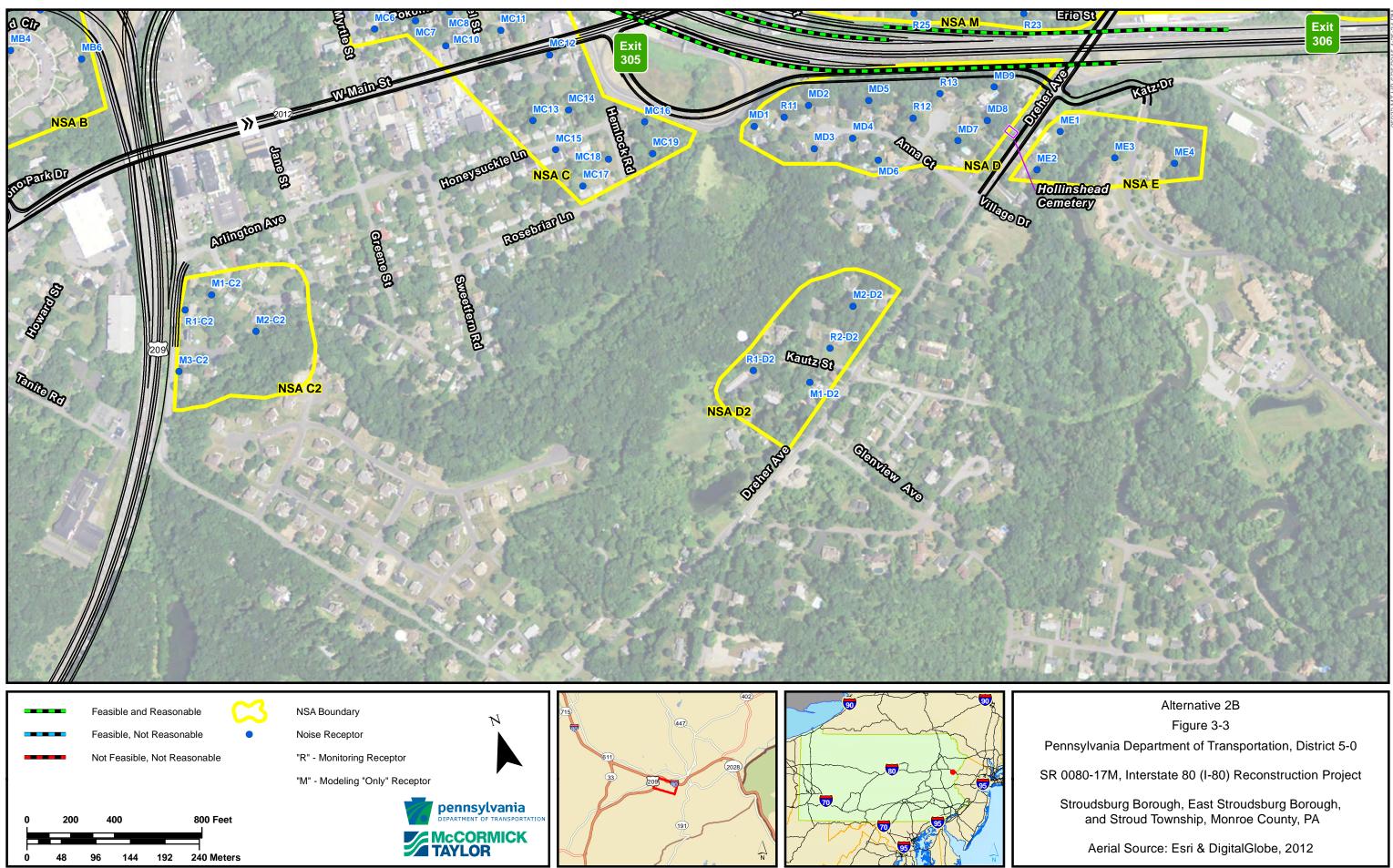


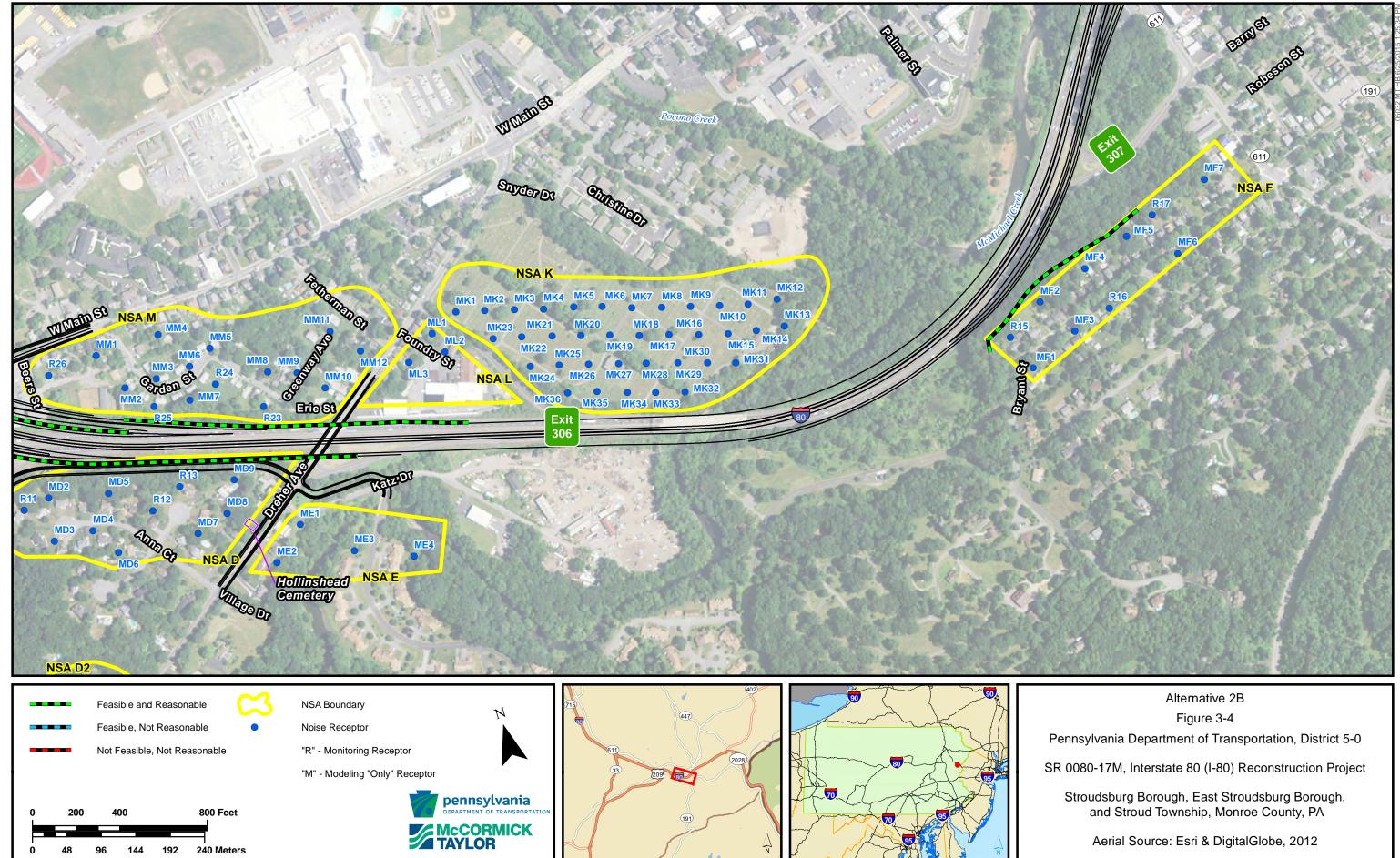


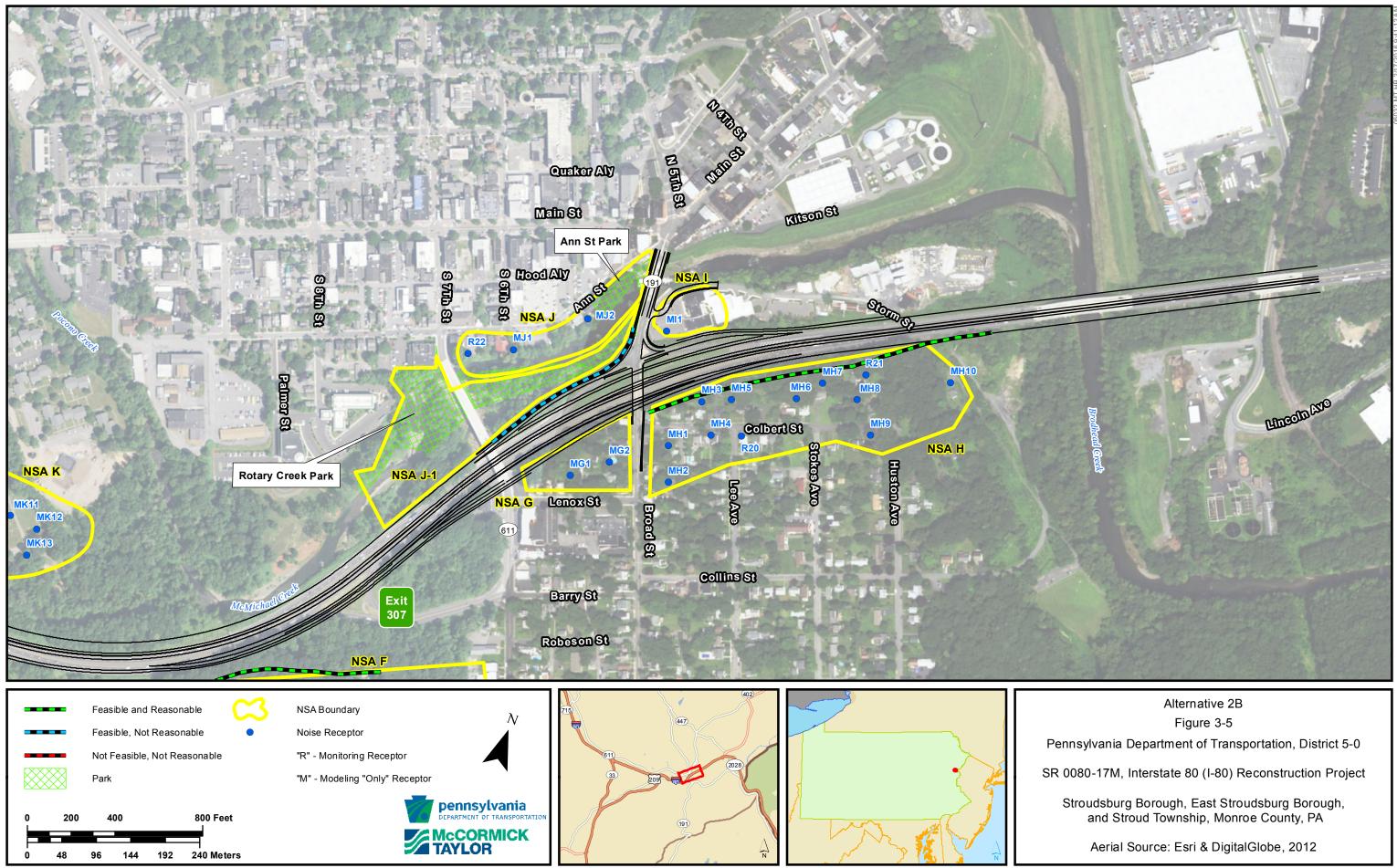


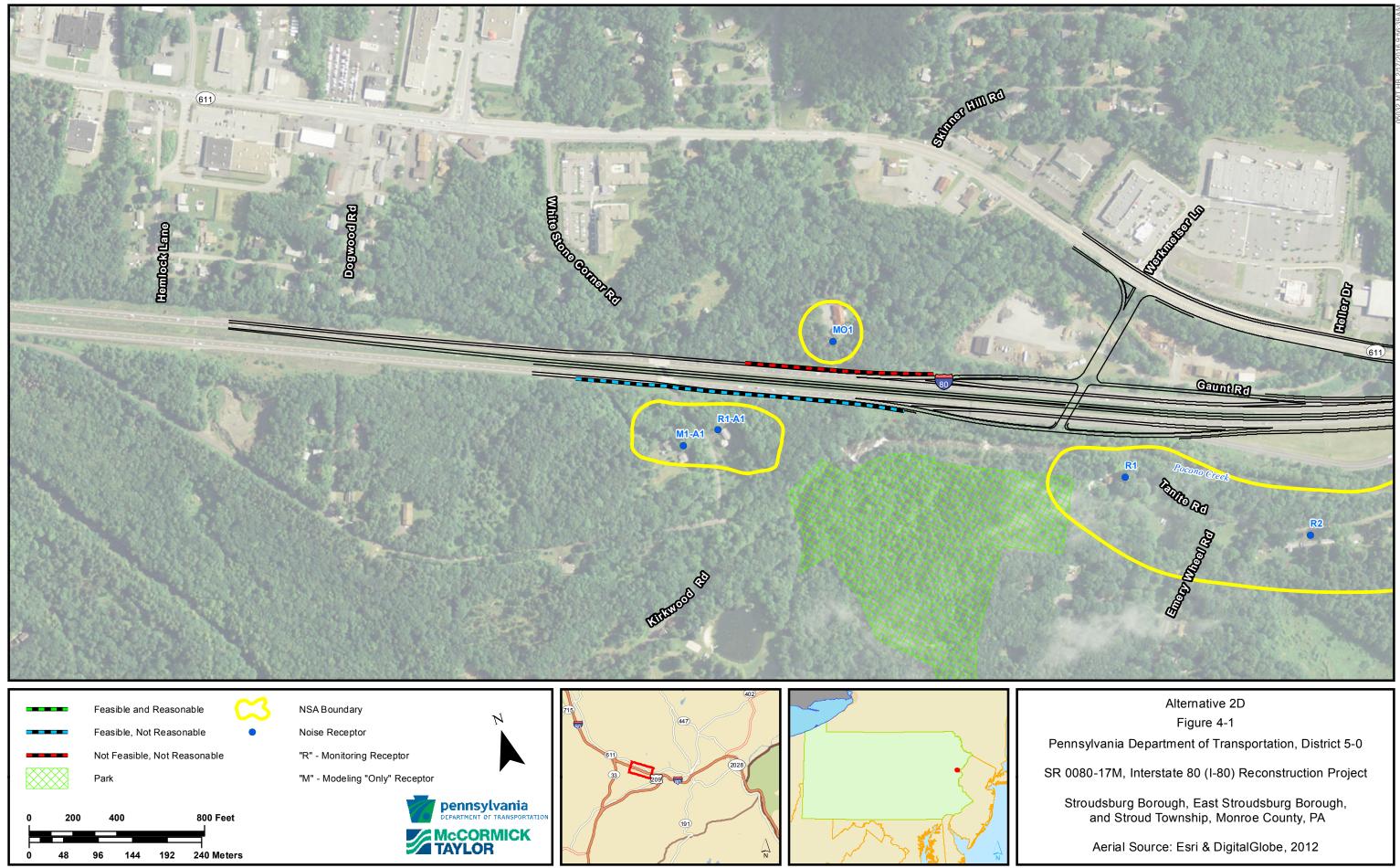


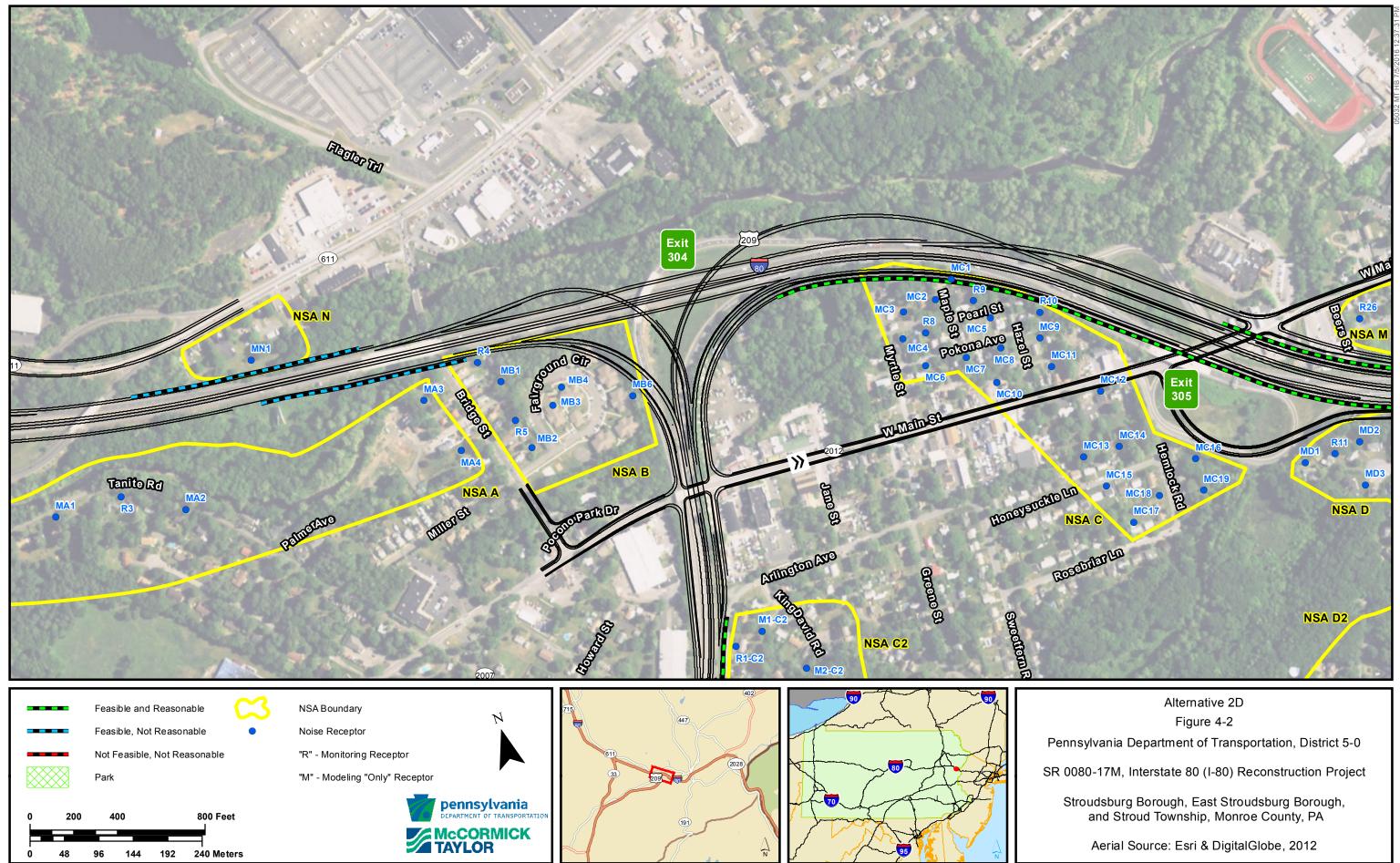


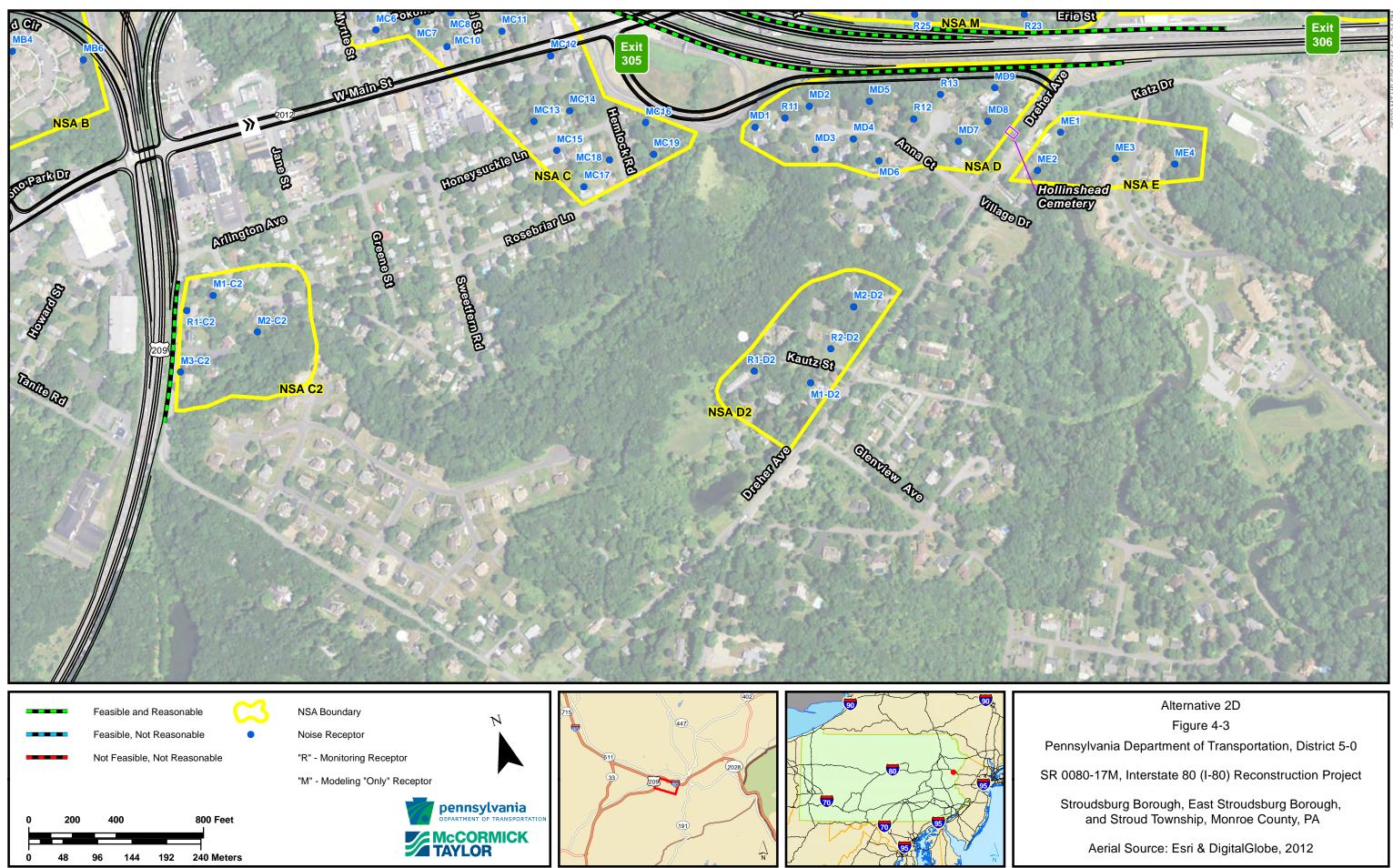


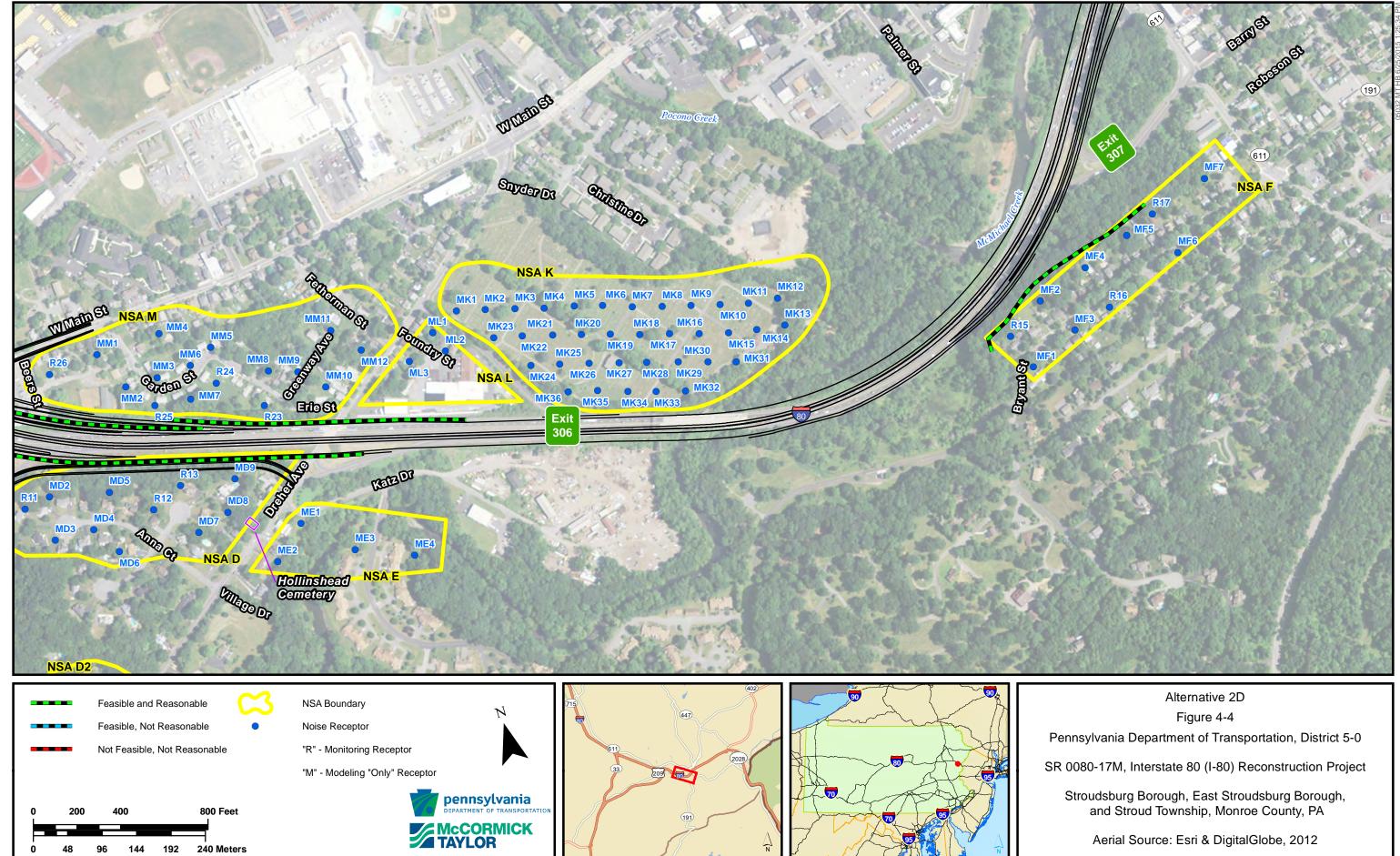


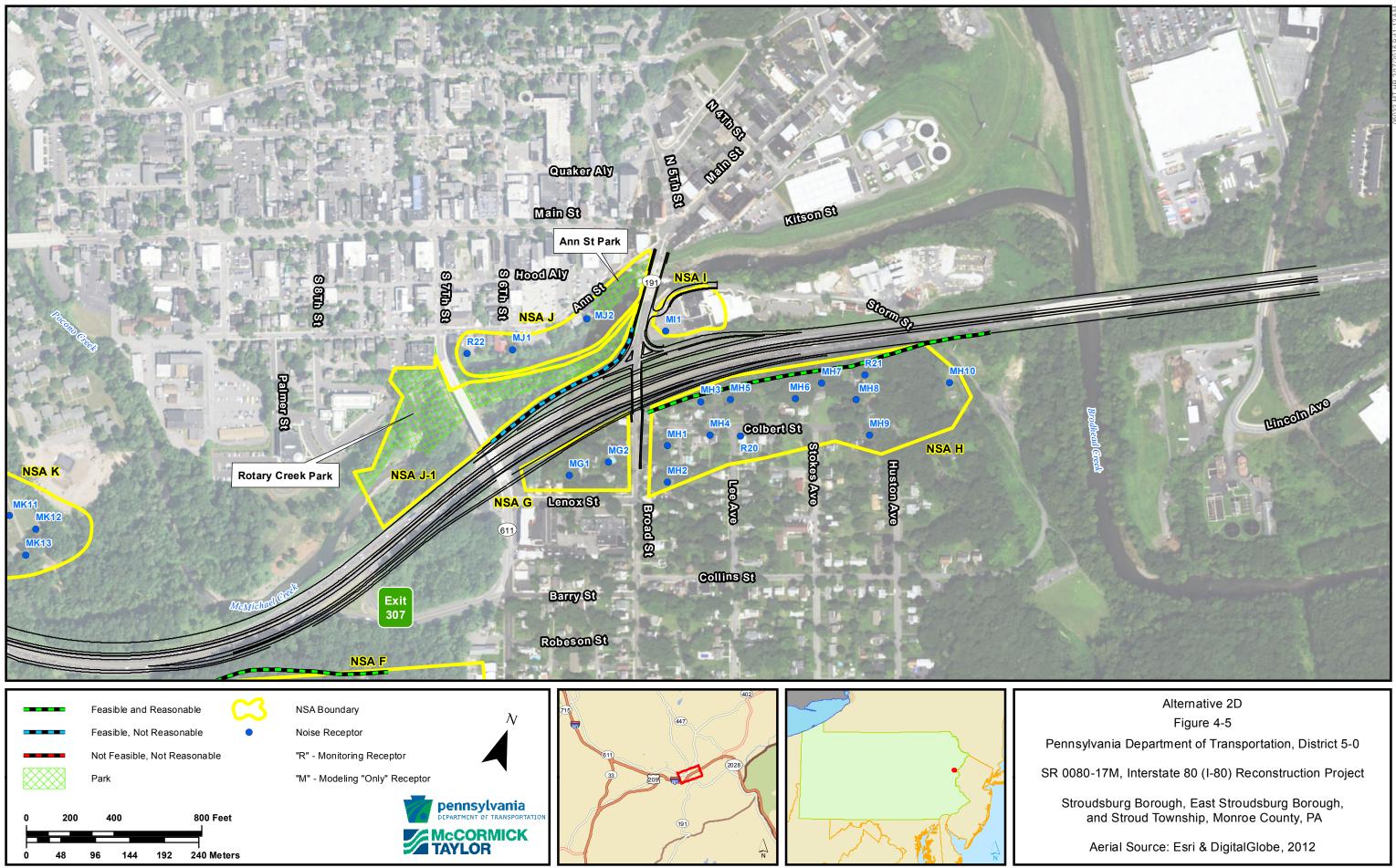












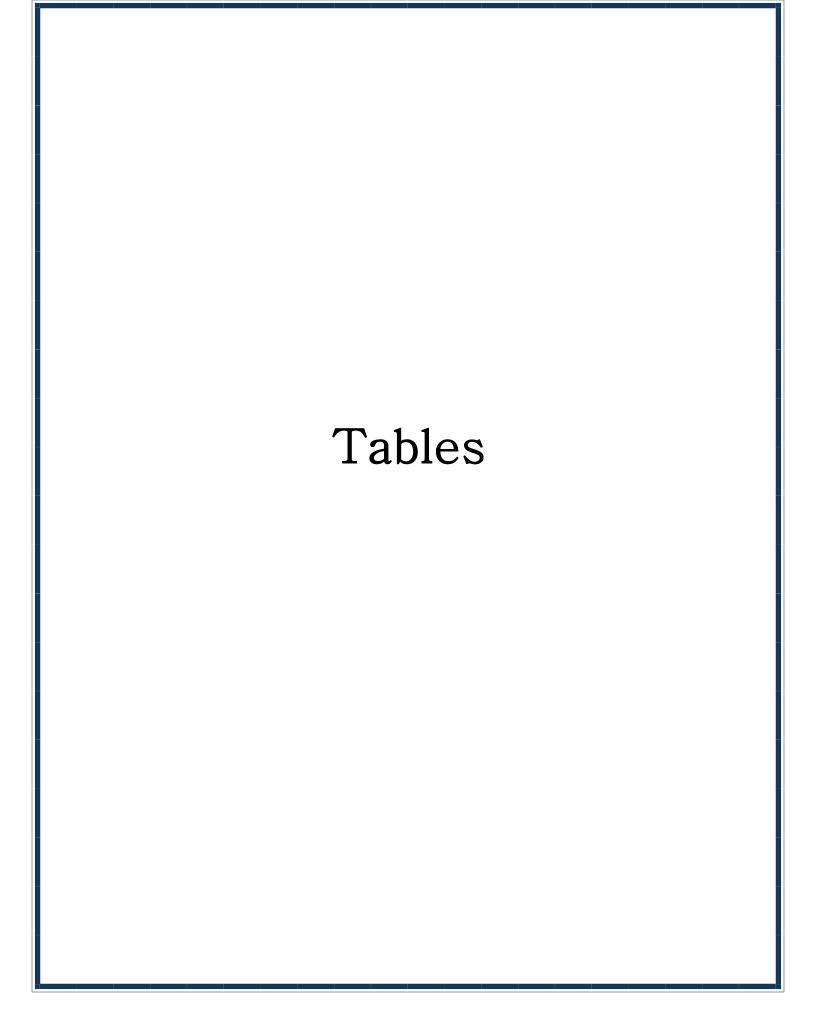


TABLE 1

I-80 Reconstruction Project

FHWA/PennDOT Noise Abatement Criteria Hourly-A-Weighted Sound Levels in Decibels (dB(A)) for Various Land Use Activity Categories*

Activity Category	$\begin{array}{l} \text{Activity} \\ \text{L}_{\text{eq}}\left(\textbf{h}\right)^{1} \end{array}$	Evaluation Location	Description of Activity Category
А	57 (Exterior)	Exterior	Lands on which serenity and quiet are of extraordinary significance and serve an important public need and where the preservation of those qualities is essential if the area is to continue to serve its intended purpose.
B ²	67 (Exterior)	Exterior	Residential.
C ²	67 (Exterior)	Exterior	Active sport areas, amphitheaters, auditoriums, campgrounds, cemeteries, day care centers, hospitals, libraries, medical facilities, parks, picnic areas, places of worship, public meeting rooms, public or non-profit institutional structures, radio studios, recording studios, recreation areas, Section 4(f) sites, schools, television studios, trails, and trail crossings.
D	52 (Exterior)	Interior	Auditoriums, day care centers, hospitals, libraries, medical facilities, places of worship, public meeting rooms, public or non-profit institutional structures, radio studios, recording studios, schools, and television studios.
E^2	72 (Exterior)	Exterior	Hotels, motels, offices, restaurants/bars, and other developed lands, properties of activities not included in A-D or F.
F		Exterior	Agriculture, airports, bus yards, emergency services, industrial logging, maintenance facilities, manufacturing, mining, rail yards, retail facilities, shipyards, utilities (water resources, water treatment, electrical), and warehousing
G			Undeveloped lands that are not permitted.
2	Includes undev	eloped lands perm	used as design standards for noise abatement purposes. nitted for this Activity Criteria. ((h) on all of its transportation improvement projects.

						Table 2						
					I-80 Re	econstruction	1 Project					
					Sou	nd Level Sun	•					
	1		2	3	4	5	6 Existing	7	8 Future	9 Future	10 Future	11 Future
NSA	Receptor Site	Site R	Representation	Monitored Noise Level	Modeled Noise Level	Difference (MonMod.)	Worst-Case (2013)	Criteria*	No-Build (2045)	Build Alt. 2A (2045)	Build Alt. 2B (2045)	Build Alt. 2D (2045)
NSA	R1-A1	1	Residence	63	63	0	64	66	66	67	67	66
A1	M1-A1 R1	2	Residences	65			64 68	66 66	64 69	65 69	67 68	65 65
	R1 R2	5	Residences	60	63	-2 -3	64	66	65	66	65	65
NSA A	R3 MA1	4	Residences Residences	61	63	-2	64 59	66 66	65 60	66 63	65 62	65 61
	MA2	1	Residence				63	66	64	65	65	64
	MA3 MA4	2 3	Residences Residences				68 64	66 66	69 65	67 64	61 61	67 64
	R4	2	Residences	65	68	-3	70	66	71	70	Acquired	62
	R5 R6	3	Residences Residences	56 64	58 64	-2 0	60 65	66 66	61 66	62 68	56 Acquired	62 Acquired
NSA	R5 3 Residence R6 9 Residence MB1 2 Residence MB2 2 Residence MB3 9 Residence MB4 9 Residence MB5 9 Residence MB6 9 Residence MB6 9 Residence R7 1 Residence R9 2 Residence R10 1 Residence MC1 1 Residence		Residences				66	66	67	68	57	64
В	R6 9 Residence MB1 2 Residence MB2 2 Residence MB3 9 Residence MB4 9 Residence MB5 9 Residence MB6 9 Residence R7 1 Residence R8 2 Residence R9 2 Residence R10 1 Residence MC1 1 Residence MC3 3 Residence		Residences Residences				60 63	66 66	61 64	63 66	56 57	62 64
	MB4 9 Residence MB5 9 Residence MB6 9 Residence R7 1 Residence R8 2 Residence R9 2 Residence R10 1 Residence	Residences				65	66	66	67	57	64	
	MB5 9 Residences MB6 9 Residences R7 1 Residences R8 2 Residences R9 2 Residences R10 1 Residence MC1 1 Residence						69 61	66 66	70 61	70 63	Acquired 58	Acquired 64
	R7		Residence	69	69	1	70	66	71	74	Acquired	Acquired
				59 67	58 68	1 -1	60 69	66 66	61 70	64 71	63 69	63 67
	R8 2 Residence R9 2 Residence R10 1 Residence MC1 1 Residence MC2 3 Residence MC3 3 Residence			69	68	1	68	66	69	72	Acquired	64
	MB5 9 Residence MB6 9 Residence R7 1 Residence R8 2 Residence R9 2 Residence R10 1 Residence MC1 1 Residence MC2 3 Residence MC3 3 Residence MC4 1 Residence MC5 3 Residence MC6 2 Residence MC7 2 Residence						68 67	66 66	69 68	Acquired 71	Acquired 69	Acquired 66
			Residences				66 64	66 66	67 65	69	68	68
			Residences				66	66	67	68 70	67 68	67 66
			Residences Residences				63 64	66 66	64 65	66 68	66 67	65 66
NSA C	MC8	2	Residences				64	66	65	68	67	65
	MC9 MC10	2	Residences Residences				66 65	66 66	67 65	69 68	67 67	64 65
	MC11	4	Residences Residences				66	66	67	69	67	65
	MC12 MC13	5 4	Residences				<u>69</u> 63	66 66	69 64	71 65	70 65	65 64
	MC14 MC15	2 5	Residences Residences				64 62	66 66	65 63	66 65	65 64	65 64
	MC16	2	Residences				64	66	65	66	66	65
	MC17 MC18	3	Residences Residences				60 61	66 66	61 62	64 66	63 64	63 64
	MC19	3	Residences				62	66	63	66	64	64
NSA	R1-C2 M1-C2	3	Residences Residences	62	64	-2	64 59	66 66	67 62	69 64	59 59	65 62
C2	M2-C2	2	Residences				57	66	59	61	58	58
	M3-C2	2	Residences				66	66	69	71	60	66
	R11 R12	1 2	Residence Residences	58 57	60 59	-3 -2	65 62	66 66	66 63	69 65	66 66	66 66
	R13 R14	2	Residences Residence	63 71	61 72	2	64 74	66 66	65 75	67 76	67 Acquired	68 Acquired
	MD1	1	Residence				55	66	56	Acquired	57	66
NSA	MD2 MD3	2	Residences Residences				58 57	66 66	59 58	61 61	60 60	60 63
D	MD4	2	Residences				58	66	59	62	62	62
	MD5 MD6	2 2	Residences Residences				60 60	66 66	61 61	63 64	63 64	63 64
	MD7 MD8	2	Residences Residences				61 62	66 66	62 63	65 65	66 67	66 67
	MD9	1	Residence				61	66	62	64	65	66
	MD9		Cemetery		 No Valid		61	66	62 58	64	65	<u>66</u>
NSA	R1-D1 R2-D2	2 2	Residences Residences	48 47		ation Site** ation Site**	57 57	66 66	58 58	61 61	58 58	58 58
D2	M1-D2 M2-D2	2	Residences				56 59	66 66	57 61	60 63	57 61	57 61
	M2-D2 ME1	1	Residences				59	66	59	63	61	63
NSA	ME2	2	Residences				59	66	60	60	62	61
E	ME3 ME4	4	Residences Residences				59 60	66 66	60 61	63 63	63 64	62 63
						-			· J			

		ble 2 Continu				_	6	7	8	9	10	11
NSA	1 Receptor Site	2 Site Repres		3 Monitored Noise Level	4 Modeled Noise Level	5 Difference (MonMod.)	Existing Worst-Case (2013)	Criteria*	Future No-Build (2045)	Future Build Alt. 2A (2045)	Future Build Alt. 2B (2045)	Future Build Alt. 2D (2045)
	R15 R16 R17	3 R	Residence esidences esidences	73 58 59	71 57 61	2 1 -3	73 60 63	66 66 66	74 61 64	75 63 66	75 61 64	75 61 63
NSA F	MF1 MF2 MF3	5 Ro 4 Ro	Residence esidences esidences	 	 		63 66 61	66 66 66	64 67 62	65 69 64	65 68 63	65 68 63
	MF4 MF5 MF6 MF7	2 R 3 R	esidences esidences esidences esidences	 	 		65 64 55 61	66 66 66 66	66 65 56 62	69 68 58 63	68 66 56 61	67 65 57 61
NSA G	R18 MG1	2 R 3 R	esidences esidences	71 		-1	75 52	66 66	76 53	77 60	Acquired 55	Acquired 56
•	MG2 MG3 R19	2 R	esidences esidences esidences	 <u>69</u>	 <u>66</u>		54 56 70	66 66 66	55 57 71	55 58 76	54 Acquired Acquired	54 Acquired Acquired
	R20 R21 MH1 MH2	1 R 4 R	esidences Residence esidences	51 67 	48 65 	3 1	52 69 55	66 66 66	53 70 56	55 72 54	60 75 52	57 73 47
NSA H	MH2 MH3 MH4 MH5	3 R 4 R	esidences esidences esidences esidences				55 59 53 58	66 66 66 66	57 60 54 59	55 63 56 62	53 65 55 68	49 65 55 68
	MH6 MH7 MH8	2 R 1 R	esidences Residence esidences	 	 	 	57 60 62	66 66 66	58 61 63	62 65 65	69 73 67	67 71 66
NSA	MH9 MH10		esidences Residence				60 66	66 66	61 67	62 67	63 69	63 69
I	MI1 R22	4 R	esidences	59	60	-1	Invalid NSA	66	66	66	66	65
NSA J	MJ1 MJ2		esidences esidences				66 65	66 66	67 66	67 63	67 64	67 63
	MK1 MK2 MK3	0.0037 C 0.0037 C	Cemetery Cemetery Cemetery	 	 	 	59 60 61	66 66 66	61 61 62	65 65 65	64 64 64	64 64 64
	MK4 MK5 MK6 MK7	0.0037 C 0.0037 C	Cemetery Cemetery Cemetery Cemetery	 			62 62 62 62	66 66 66 66	63 63 63 63	66 65 65 65	65 65 65 65	64 64 65
	MK8 MK9 MK10	0.0037 C 0.0037 C	Cemetery Cemetery Cemetery				62 63 63	66 66 66	63 64 64	65 65 65	65 65 66	65 66 66
	MK11 MK12 MK13	0.0037 C	Cemetery Cemetery Cemetery	 	 	 	63 63 65	66 66 66	64 64 <u>66</u>	65 65 <u>68</u>	66 67 69	66 66 69
	MK14 MK15 MK16	0.0037 C 0.0037 C	Cemetery Cemetery Cemetery	 	 		65 65 65	66 66 66	66 66 66	68 67 67	69 68 67	68 68 68
NSA K***	MK17 MK18 MK19 MK20	0.0037 C 0.0037 C	Cemetery Cemetery Cemetery Cemetery	 	 		64 64 63 63	66 66 66 66	65 65 64 64	67 67 66 67	67 67 66 66	68 67 66 66
	MK20 MK21 MK22 MK23	0.0037 C 0.0037 C	Cemetery Cemetery Cemetery Cemetery		 		63 63 60	66 66 66	64 64 62	67 66 66	66 65 64	66 65 65
	MK24 MK25 MK26	0.0037 C 0.0037 C	Cemetery Cemetery Cemetery	 	 	 	63 65 <u>66</u>	66 66 66	64 66 67	66 69 70	64 67 67	68 68 68
	MK27 MK28 MK29 MK20	0.0037 C 0.0037 C	Cemetery Cemetery Cemetery	 	 		66 67 67	66 66 66	67 68 68	69 70 70	67 69 69 70	69 70 70 70
	MK30 MK31 MK32 MK33	0.0037 C 0.0037 C	Cemetery Cemetery Cemetery Cemetery	 	 	 	67 68 70 69	66 66 66 66	68 69 71 70	70 70 73 73	70 70 71 70	70 71 72 71
	MK35 MK34 MK35 MK36	0.0037 C 0.0037 C	Cemetery Cemetery Cemetery Cemetery		 	 	69 68 66	66 66 66	70 69 67	73 72 71	69 68 66	71 71 70 70

	Ta	ble 2 Co	ontinued				6	7	8	9	10	11
	1 Receptor		2	3 Monitored	4 Modeled	5 Difference	Existing Worst-Case	Criteria*	Future No-Build	Future Build	Future Build	Future Build
NSA	Site	Site R	lepresentation	Noise Level	Noise Level	(MonMod.)	(2013)		(2045)	Alt. 2A (2045)	Alt. 2B (2045)	Alt. 2D (2045)
NSA	ML1	1	Residence				62	66	63	65	64	64
L	ML2	2	Residences				61	66	62	64	63	63
	ML3	2	Residences				63	66	64	67	65	65
	R23	2	Residences	65	67	-2	69	66	70	67	67	70
	R24	4	Residences	65	66	0	68	66	69	68	67	69
	R25	4	Residences	64	67	-3	69	66	70	66	66	70
	R26	4	Residences	64	65	-1	67	66	68	70	69	70
	MM1	3	Residences				68	66	69	71	70	70
	MM2	4	Residences				73	66	74	74	73	74
	MM3	4	Residences				72	66	73	74	72	73
NSA	MM4	3	Residences				68	66	69	70	68	69
Μ	MM5	4	Residences				69	66	70	70	69	70
	MM6	4	Residences				71	66	72	73	71	72
	MM7	4	Residences				75	66	76	75	74	76
	MM8	2	Residences				72	66	73	71	71	72
	MM9	3	Residences				68	66	69	69	68	69
	MM10	3	Residences				69	66	70	71	70	70
	MM11	2	Residences				66	66	67	68	67	67
	MM12	1	Residence				65	66	66	68	66	67
NSA N	MN1	4	Offices				75	72	75	75	77	77
NSA O	MO1	1	Residence				71	66	72	74	68	66
Note Note	No engine All sound Column 5 Criteria b	o be acc eering cl levels d - Differe ased on	quired under this hanges in the vio locumented as o ence (ModMon levels "approac	cinity under this ne hour Leq (Le .) may not matc hing" the absolu	eq(h)) h the subtractio ite criteria or tha	build noise value n do to rounding at meets the "sub	functions stantial increase	e" criterion				

- ** The monitored sound level at this site is considered ambient, with no roadway noise influence.
 *** Indeividual receptor values based on the Equivalent Residential Unit (ERU); PennDOT Publication 24, Appendix E, Cemetery Case (2)

Distan	Table 3 d Lands - Noise Leve ice from Centerline (1 ear (2045) Noise Level S	feet)*											
Receptor SiteDistanceSound LevelUndeveloped Land 110077													
Undeveloped Land 2	200	72											
Undeveloped Land 3	300	67											
Undeveloped Land 4	400	67											
Undeveloped Land 5	500	66											
Undeveloped Land 6	550	65											
* From centerline of I-80 e Red text denotes sound	eastbound alignment. levels that are at or above the 66	dB(A) threshold.											

							80 Reconst Alterr	ble 4-1 ruction Pr <i>aative 2A</i> Aitigation 1	•	1							
				Barrier 8 F	Height	Barrier 10 I	Height		Height Feet		Height Feet		Height Feet		Height Feet		r Height Feet
NSA	Receptor Site	Site Representation	Future Build Noise Level (2045)	Mitigated Noise Level	Insertion Loss (IL)	Mitigated Noise Level	Insertion Loss (IL)	Mitigated Noise Level	Insertion Loss (IL)	Mitigated Noise Level	Insertion Loss (IL)	Mitigated Noise Level	Insertion Loss (IL)	Mitigated Noise Level	Insertion Loss (IL)	Mitigated Noise Level	Insertion Loss (IL)
A1	R1-A1	1 Residence	67	66	1	65	2	64	3	62	5	61	6	60	6	60	7
	M1-A1	2 Residences	65	64	1	63	2	62	3	61	4	60	5	59	6	59	6
	R1	3 Residence	69	65	3	64	5	63	6	62	7	61	7	61	8	61	8
	R2	5 Residences	66	64	2	62	4	61	5	60	6	59	7	59	7	58	7
A	R3	4 Residences	66	62	5	60	6	60	7	59	7	59	8	59	8	58	8
	MA1 MA2	5 Residences 1 Residence	63 65	59 61	4	58 60	5 5	57 59	6 6	57 59	6 6	56 59	7 6	56 59	7 6	56 58	7
															_		· · ·
	R4	2 Residences	70	61	9	61	10	60	10	60	10	59	11	59	11	59	12
	R5	3 Residences	62	59	3	57	5	56	6	56	6	55	7	55	7	55	8
	R6	9 Residences	68	64	3	63	5	62	6	61	6	61	6	61	7	61	7
	MA3	2 Residences 3 Residences	67 64	61 60	6 4	60 59	7	59 58	7	59 57	8	59 57	8	58 57	8 7	58 56	9 8
В	MA4 MB1	3 Residences 2 Residences	68	61	4	60	8	60	8	60	8	59	9	59	9	58	<u> </u>
Б	MB1 MB2	2 Residences 2 Residences	63	60	3	59	4	58	6	57	6	56	9 7	56	9 7	56	9 8
	MB2 MB3	2 Residences 9 Residences	66	60	4	60	6	59	7	57	9	58	8	57	9	57	<u> </u>
	MB3 MB4	9 Residences	67	62	5	60	7	59	8	59	8	58	9	58	9	57	10
	MB4 MB5	9 Residences	70	63	7	62	8	62	8	61	9	61	9	60	9 10	60	10
	MB5 MB6	9 Residences	63	62	1	61	2	61	2	61	3	60	3	60	3	60	3
															_		
	R7	1 Residence	74	64	- 11	63	11	62	12	62	12	62	13	61	13	61	13
	R8	2 Residences	64	62	2	61	3	60	5	59	5	59	6	58	6	58	7
	R9	2 Residences	71	64	8	63	9	62	9	61	10	61	11	60	11	60	11
	R10	1 Residence	72	63	10	62	10	62	11	61	11	60	12	60	12	60	13
	MC2	3 Residences	71	63	7	62	8	62	9	61	10	60	10	60	11	59	11
	MC3	3 Residences	69	66	4	64	6	62	7	61	8	61	9	60	9	60	10
	MC4 MC5	1 Residence	68 70	65 63	3	64 62	3	63 61	5 9	62 61	6 9	61 60	7 10	61 60	7 10	60 59	7
	MC5 MC6	3 Residences 2 Residences	70 66	64	2	62	3	61	5	61	9 5	60	6	60 60	6	59 60	7
	MC6 MC7	2 Residences 2 Residences	68	64	3	64	4	62	6	61	6	61	7	60	7	60	8
	MC7 MC8	2 Residences	68	64	3	63	5	61	7	61	7	60	8	60	8	59	9
C	MC9	2 Residences	69	62	7	61	8	60	9	59	9	59	10	59	10	58	11
	MC10	2 Residences	68	66	2	65	3	64	4	63	5	63	5	63	5	62	5
	MC11	4 Residences	69	64	5	63	6	62	7	61	7	61	8	61	8	61	8
	MC12	5 Residences	71	69	2	68	3	68	3	68	3	68	3	68	3	68	3
	MC13	4 Residences	65	62	4	61	5	59	6	59	7	58	7	58	8	58	8
	MC14	2 Residences	66	62	4	61	6	60	7	59	7	59	7	59	8	58	8
	MC15	5 Residences	65	61	3	60	4	59	6	58	6	58	7	57	7	57	7
	MC16	2 Residences	66	62	4	62	5	61	5	61	5	60	6	60	6	60	6
	MC17	3 Residences	64	61	3	60	3	59	4	59	5	58	5	58	6	58	6
	MC18	2 Residences	66	64	2	64	2	63	3	63	3	63	3	63	3	63	3
	MC19	3 Residences	66	64	2	63	2	63	3	63	3	63	3	62	3	62	3

	Table 4-1	Continued		Barrier	Height												
			Future Build	8 F	eet	10	Feet	12	Feet	14 1	Feet	16 1	Feet	18	Feet	20	Feet
NSA	Receptor Site	Site Representation	Noise Level (2045)	Mitigated Noise Level	Insertion Loss (IL)												
	R11	1 Residence	69	63	6	62	7	62	7	61	8	61	9	60	9	60	10
	R12	2 Residences	65	65	0	65	0	65	0	64	1	63	2	63	3	62	3
	R13	2 Residences	67	67	0	67	0	66	1	65	2	65	3	64	3	63	4
	R14	1 Residence	76	72	4	70	6	69	7	68	8	68	9	67	9	67	9
	MD2	2 Residences	61	61	0	61	0	61	1	60	1	60	2	59	2	59	3
	MD3	2 Residences	61	60	0	60	1	60	1	59	1	59	2	59	2	59	2
D	MD4	2 Residences	62	62	1	61	1	61	1	60	2	60	2	60	2	59	3
	MD5	2 Residences	63	63	0	63	0	63	0	63	1	62	1	61	2	61	2
	MD6	2 Residences	64	64	1	63	1	62	2	62	2	61	3	61	3	60	4
	MD7	2 Residences	65	65	0	65	0	64	0	64	1	63	1	63	2	62	2
	MD8	2 Residences	65	65	0	64	0	64	1	64	1	64	1	63	2	63	2
	MD9	1 Residence	64	64	0	65	0	64	0	63	1	63	1	62	2	62	2
	R15	1 Residence	75	69	6	67	8	66	9	65	10	64	- 11	63	12	63	12
	R16	3 Residences	63	61	2	61	2	60	3	60	3	60	3	59	3	59	4
	R17	5 Residences	66	66	0	66	0	66	1	66	1	65	1	65	2	64	2
	MF1	1 Residence	65	64	1	64	1	64	1	64	1	64	1	64	1	64	1
F	MF2	5 Residences	69	64	5	64	5	63	6	62	7	62	7	62	7	61	8
г	MF3	4 Residences	64	62	1	62	1	62	1	62	1	62	2	62	2	62	2
	MF4	4 Residences	69	63	6	62	7	61	8	61	8	60	9	60	9	59	10
	MF5	2 Residences	68	64	4	63	5	62	6	61	7	60	8	59	9	59	9
	MF6	3 Residences	58	58	0	58	0	58	0	57	1	57	1	57	1	57	1
	MF7	3 Residences	63	63	0	63	0	63	0	63	0	63	0	63	1	63	1
	R18	2 Residences	77	74	3	72	4	71	5	71	6	70	6	70	7	70	7
	MG1	3 Residences	60	60	0	60	0	60	0	60	0	60	0	60	0	60	0
G	MG2	3 Residences	55	55	0	55	0	55	0	55	0	54	0	54	0	54	1
	MG3	2 Residences	58	58	0	58	0	58	0	57	1	57	1	57	1	57	1
	R19	2 Residences	76	67	9	65	11	64	12	64	12	63	13	63	13	62	14
	R19 R20	4 Residences	55	55	9	55	0	55	0	55	0	55	0	55	0	55	0
	R20 R21	1 Residence	72	70	2	<u>69</u>	2	<u>69</u>	3	69	3	68	3	68	4	68	4
	MH1	4 Residences	54	54	0	54	0	54	0	54	0	54	0	54	0	54	0
	MH2	4 Residences	55	55	0	55	0	55	0	55	0	55	0	55	0	55	0
	MH3	3 Residences	63	61	2	61	2	61	2	60	3	60	3	60	3	60	3
н	MH4	4 Residences	56	56	0	56	0	56	0	56	0	56	0	58	-2	56	0
	MH5	3 Residences	62	62	1	61	1	61	1	61	1	61	1	61	2	60	2
	MH6	2 Residences	62	61	1	61	1	61	1	60	1	60	1	60	2	60	2
	MH7	1 Residence	65	65	0	64	0	64	1	64	1	64	1	64	1	63	2
	MH8	2 Residences	65	65	0	65	0	65	0	65	0	65	0	65	0	65	1
	MH9	2 Residences	62	62	0	63	0	62	0	62	0	61	1	61	1	60	2
	MH10	1 Residence	67	65	2	65	3	64	3	64	3	64	3	64	4	64	4

	Table 4-1	Continued		•	Height		r Height										
			Future Build	8 F	Feet	10 1	Feet		Feet	14 1	Feet	16	Feet		Feet		Feet
NSA	Receptor Site	Site Representation	Noise Level (2045)	Mitigated Noise Level	Insertion Loss (IL)												
	R22	4 Residences	66	64	1	64	2	63	2	63	2	63	3	63	3	63	3
J	MJ1	3 Residences	67	65	2	64	3	64	3	64	3	63	3	63	4	63	4
	MJ2	3 Residences	63	61	2	61	2	61	3	60	3	60	3	60	3	60	3
	MK1	0 Cemetery	65	64.5	0	63.8	1	63.6	1	63.4	2	63.3	2	63.3	2	63.2	2
	MK2	0 Cemetery	65	64.3	1	63.1	2	62.7	3	62.5	3	62.3	3	62.2	3	62.1	3
	MK3	0 Cemetery	65	64	1	62.9	2	61.9	3	61.5	4	61.3	4	61.1	4	61	4
	MK4	0 Cemetery	66	63.8	2	62.6	3	61.2	4	60.8	5	60.4	5	60.2	5	60	6
	MK5	0 Cemetery	65	63.5	2	62.3	3	60.8	5	60.1	5	59.7	6	59.4	6	59.2	6
	MK6	0 Cemetery	65	63.3	2	62.3	3	60.5	5	59.8	5	59.3	6	59	6	58.7	7
	MK7	0 Cemetery	65	63.4	2	62.8	2	60.5	5	59.6	6	59.1	6	58.7	7	58.4	7
	MK8	0 Cemetery	65	63.6	2	63	2	60.7	5	59.6	6	59	6	58.6	7	58.3	7
	MK9	0 Cemetery	65	63.7	1	63.1	2	61	4	59.7	5	59.2	6	58.7	6	58.4	7
	MK10	0 Cemetery	65	63.9	1	63.6	1	61.3	4	59.9	5	59.3	6	58.8	6	58.5	7
	MK11	0 Cemetery	65	64.1	1	63.8	1	61.7	4	60.3	5	59.7	6	59.2	6	58.8	6
	MK12	0 Cemetery	65	64.4	1	63.9	2	62.1	3	60.7	5	60.2	5	59.8	6	59.4	6
	MK13	0 Cemetery	68	66	2	65.5	2	62.7	5	61.8	6	61.2	7	60.7	7	60.3	8
	MK14	0 Cemetery	68	65.8	2	65	3	62.3	5	61.3	6	60.7	7	60.1	7	59.7	8
	MK15	0 Cemetery	67	65.7	2	64.5	3	62	5	60.9	7	60.3	7	59.7	8	59.2	8
	MK16	0 Cemetery	67	65.4	2	64	3	61.6	6	60.6	7	59.8	7	59.3	8	58.8	8
	MK17	0 Cemetery	67	65.2	2	63.5	4	61.3	6	60.3	7	59.7	7	59.1	8	58.7	8
к	MK18	0 Cemetery	67	65	2	62.4	5	61.2	6	60.3	7	59.7	7	59.2	8	58.8	8
ĸ	MK19	0 Cemetery	66	64.4	2	61.9	5	60.8	6	60.1	6	59.5	7	59.1	7	58.7	8
	MK20	0 Cemetery	67	64.4	3	62	5	61.1	6	60.4	7	59.8	7	59.5	8	59.1	8
	MK21	0 Cemetery	67	64.6	3	62.2	5	61.5	6	60.9	6	60.5	7	60.1	7	59.9	7
	MK22	0 Cemetery	66	64.8	1	62.9	3	62.3	4	62	4	61.7	4	61.5	5	61.3	5
	MK23	0 Cemetery	66	64.9	1	64	2	63.7	2	63.5	2	63.3	2	63.2	2	63.1	2
	MK24	0 Cemetery	66	61.4	5	60.4	6	59.7	7	59.1	7	58.6	8	58.2	8	57.9	8
	MK25	0 Cemetery	69	63.2	6	62.1	7	61.4	8	60.8	8	60.2	9	59.7	9	59.3	10
	MK26	0 Cemetery	70	63.7	6	62.4	7	61.5	8	60.9	9	60.2	9	59.7	10	59.2	10
	MK27	0 Cemetery	69	64.8	4	62.1	7	61	8	60.2	9	59.5	10	58.9	10	58.4	11
	MK28	0 Cemetery	70	65.9	4	63.5	7	62.5	8	61.7	8	61	9	60.5	10	59.9	10
	MK29	0 Cemetery	70	66.2	4	63.9	6	62.7	7	62	8	61.3	9	60.7	9	60.2	10
	MK30	0 Cemetery	70	66.6	3	64.3	6	63	7	62.2	8	61.5	8	60.9	9	60.4	10
	MK31	0 Cemetery	70	67.1	3	64.7	6	63.3	7	62.5	8	61.8	8	61.3	9	60.8	9
	MK32	0 Cemetery	73	65.3	8	64.5	9	63.8	9	63.2	10	62.6	- 11	62.1	11	61.6	12
	MK33	0 Cemetery	73	64.9	8	64.2	9	63.5	10	62.9	10	62.3	- 11	61.8	- 11	61.3	12
	MK34	0 Cemetery	73	64.6	8	63.8	9	63.2	10	62.7	10	62.1	- 11	61.6	- 11	61.1	12
	MK35	0 Cemetery	72	63.9	8	63.3	9	62.7	9	62.2	10	61.7	10	61.2	- 11	60.7	11
	MK36	0 Cemetery	71	62.9	8	62.3	8	61.7	9	61.2	10	60.6	10	60.2	- 11	59.7	- 11

	Table 4-1	Continued	Future Build	1	Height eet		Height Feet		Height Feet	Barrier 14 I	Height Feet		· Height Feet	Barrier 18 I	Height Feet		Height Feet
NSA	Receptor Site	Site Representation	Noise Level (2045)	Mitigated Noise Level	Insertion Loss (IL)	Mitigated Noise Level	Insertion Loss (IL)	Mitigated Noise Level	Insertion Loss (IL)	Mitigated Noise Level	Insertion Loss (IL)						
	244			(2)		(2)	-	(2)							-	60	
	R23 R24	2 Residences 4 Residences	67 68	63 64	4	62 63	5	62 62	5	61 61	6 7	61 61	6 7	60 60	7	60 60	7
	R24 R25	4 Residences 4 Residences	66	64	2	63	3	62	6 4	61	4	61	5	60	5	60	<u>8</u> 6
	R25 R26	4 Residences 4 Residences	70	69	2	63 68	2	63 67	3	62	4	66	4	61 66	4	60 66	4
	ML1	4 Residences	65	61	4	59	6	59	6	59	6	58	4	58	4	58	4
	ML1 ML2	2 Residences	64	59	4	58	6	58	7	57	7	57	7	57	7	57	8
	ML2 ML3	2 Residences 2 Residences	67	59 60	7	59	8	59	8	58	9	58	9	57	10	57	0 10
	ML3 MM1	2 Residences 3 Residences	71	69	2	69	2	68	2	58 67	4	66	4	66	5	65	5
	MM2	4 Residences	74	71	2	71	3	70	3	67	6	66	7	66	8	65	9
L/M	MM3	4 Residences	74	71	3	70	4	70	4	66	8	65	9	65	9	64	10
	MM4	3 Residences	70	67	3	67	3	66	4	64	6	63	7	63	7	62	8
	MM5	4 Residences	70	68	2	68	2	67	3	64	6	64	6	63	7	63	7
	MM6	4 Residences	73	70	3	69	3	69	4	65	7	65	8	64	9	64	9
	MM7	4 Residences	75	73	2	72	3	72	3	68	7	67	8	66	9	65	10
	MM8	2 Residences	71	69	2	68	4	66	6	65	7	64	7	64	8	63	8
	MM9	3 Residences	69	64	6	63	6	62	7	62	7	62	8	61	8	61	9
	MM10	3 Residences	71	64	7	63	8	63	8	62	9	62	9	61	10	61	10
	MM11	2 Residences	68	65	3	63	5	62	5	62	6	62	6	61	6	61	7
	MM12	1 Residence	68	62	6	61	6	61	7	60	7	60	8	60	8	60	8
N	MN1*	4 Commercial	75	68	7	67	8	66	9	65	10	64	11	64	11	63	12
0	MO1	1 Residence	74	73	1	72	1	72	2	71	3	69	5	68	6	66	8
	*	Category E land u	ıse (72 dBA threshol	d)							All sound	levels do	cumented	as one ho	our Leq (L	eq(h))	
		Impacted Rec	idences								evaluation t be "not rea	to determine sonable" do	included in t a barries fe to cost calcu been optimiz	asibility. NS ulation for Al	SA K was de Il Alternative	termined to	
		reasible/Optir	nized Barrier Mo	baelea							Barriers C a	and L/M hav	mized at 10	nized at 14 f			

							I-80 Recons Alter	rnative 2B	Project • Evaluation	n							
			Future Build		Height Seet		Height Feet		Height Feet	Barrier 14 I	Height Feet	Barrier I 16 Fe	-		Height Feet		· Height Feet
NSA	Receptor Site	Site Representation	Noise Level (2045)	Mitigated Noise Level	Insertion Loss (IL)	Mitigated Noise Level	Insertion Loss (IL)	Mitigated Noise Level	Insertion Loss (IL)	Mitigated Noise Level	Insertion Loss (IL)	Mitigated Noise Level	Insertion Loss (IL)	Mitigated Noise Level	Insertion Loss (IL)	Mitigated Noise Level	Insertion Loss (IL)
	R1-A1	1 Residence	67	62	6	61	7	60	7	59	8	59	8	59	9	58	9
A1	M1-A1	2 Residences	67	62	5	60	6	59	7	59	8	58	8	58	9	58	9
	R1	3 Residences	68	65	3	64	4	63	5	62	5	62	6	61	6	61	7
	R1 R2	5 Residences	65	64	1	63	2	62	3	62	3	61	4	61	4	61	4
Α	R2 R3	4 Residences	65	65	0	65	0	65	0	65	0	65	1	65	1	64	2
	MA1	5 Residences	62	62	0	62	0	62	0	62	0	62	0	61	1	61	1
	MA2	1 Residence	65	65	0	65	0	64	0	64	0	64	0	64	1	64	1
В								Not Warra	nted								
	R8	2 Residences	63	62	1	61	2	60	3	60	3	60	3	59	4	59	4
	R9	2 Residences	69	63	6	62	7	61	8	61	8	60	9	60	9	59	10
	MC2	3 Residences	69	62	6	61	7	61	8	60	9	60	9	59	10	59	10
	MC3	3 Residences	68	64	4	64	5	63	5	63	5	62	6	61	7	61	7
	MC4	1 Residence	67	65	2	64	3	63	4	63	4	62	5	62	5	62	5
	MC5	3 Residences	68	63	5	62	6	61	7	61	7	61	7	60	8	60	8
	MC6	2 Residences	66	65	1	64	2	63	4	62	4	62	4	62	4	62	5
	MC7	2 Residences	67	65	2	64	3	63	4	63	4	62	4	62	5	62	5
	MC8	2 Residences	67	64	3	63	4	62	4	62	5	61	5	61	6	61	6
с	MC9	2 Residences	67	63	5	61	6	61	7	60	7	60	8	59	8	59	9
-	MC10	2 Residences	67	66	1	65	2	64	3	64	3	64	3	64	3	64	4
	MC11	4 Residences	67	63	3	63	4	62	4	62	5	61	5	61	5	61	6
	MC12	5 Residences	70	68	1	68	1	68	2	68	2	68	2	68	2	68	2
	MC13	4 Residences	65	62	3	61	4	60	5	59	5	59	6	59	6	58	6
	MC14	2 Residences 5 Residences	65	62	4	61	5	60	5	59	6	59	6	59	7	58	7
	MC15 MC16	5 Residences 2 Residences	64	61	3	60	4	59	5	59	5	58	6	58	6 7	57 59	7
	MC16 MC17	2 Residences 3 Residences	66 63	62 61	4	61 60	3	60 58	5	60 58	6 5	59 57	6 6	59 57	6	59	6
	MC17 MC18	2 Residences	64	61	3	60	4	58 59	5	58	6	58	6	57	7	57	7
	MC19	3 Residences	64	61	3	60	4	59	5	58	6	58	6	57	7	57	7
	R11	1 Residence	66	64	2	63	3	62	4	60	6	60	6	59	7	59	7
	R12	2 Residences	66	65	1	65	1	64	2	64	2	63	3	61	4	61	5
	R13	2 Residences	67	67	1	66	1	66	2	65	2	64	3	63	4	62	6
	MD1	1 Residence	57	56	1	55	2	54	3	54	4	53	4	53	4	52	5
	MD2	2 Residences	60	59	1	59	1	58	2	57	3	56	4	56	5	55	5
D	MD3	2 Residences	60	59	1	59	2	58	2	57	3	57	4	56	4	56	4
	MD4	2 Residences	62	60	1	60	1	60	2	59	3	58	4	57	4	57	5
	MD5	2 Residences	63	62	1	62	1	62	1	61	2	60	3	59	4	58	5
	MD6	2 Residences	64	63	1	63	1	62	1	62	2	61	3	60	4	60	4
	MD7	2 Residences	66	64	1	64	2	64	2	62	3	62	4	61	5	61	5
	MD8	2 Residences	67	64	2	63	3	62	5	61	5	61	6	61	6	60	6
	MD9	1 Residence	65	63	2	62	2	62	3	60	4	60	5	59	6	59	6

	Table 4-2	Continued		Barrier		Barrier	-		Height		Height	Barrier I	-		Height		Height
_			Future Build		eet		Feet		Feet		Feet	16 F	eet		Feet		Feet
NSA	Receptor Site	Site Representation	Noise Level (2045)	Mitigated Noise Level	Insertion Loss (IL)	Mitigated Noise Level	Insertion Loss (IL)	Mitigated Noise Level	Insertion Loss (IL)	Mitigated Noise Level	Insertion Loss (IL)						
C2								Not Warra	nted								
Е								Not Warra	nted								
	R15	1 Residence	75	68	7	66	9	65	10	64	- 11	63	12	62	13	61	13
	R15	3 Residences	61	59	3	58	3	58	4	57	4	57	4	56	5	56	5
	R17	5 Residences	64	62	2	62	2	62	2	62	2	62	2	62	2	62	2
	MF1	1 Residence	65	64	0	64	0	64	0	64		64	-	64	-	64	
F	MF2	5 Residences	68	63	5	63	6	62	6	61	7	61	8	60	8	60	9
	MF3	4 Residences	63	61	1	61	2	61	2	60	2	60	3	60	3	60	3
	MF4	4 Residences	68	62	6	61	7	60	7	60	8	59	9	59	9	58	10
	MF5	2 Residences	66	60	6	59	6	59	7	58	8	57	8	57	9	56	9
	MF6	3 Residences	56	55	1	55	1	55	2	55	2	54	2	54	2	54	2
G								Not Warra	nted								
	R20	4 Residences	60	55	5	54	5	54	5	54	5	54	6	54	6	54	6
	R21	1 Residence	75	69	6	69	6	68	7	68	7	67	8	67	8	67	8
	MH1	4 Residences	52	52	0	52	0	52	0	52	0	52	0	52	0	52	0
	MH2	4 Residences	53	53	0	53	0	53	0	53	0	53	0	53	0	53	0
	MH3	3 Residences	65	60	5	60	5	59	6	59	6	59	7	58	7	58	7
н	MH4	4 Residences	55	55	0	55	0	55	0	55	0	55	0	55	0	55	0
"	MH5	3 Residences	68	60	8	60	8	60	8	60	8	59	9	59	9	59	9
	MH6	2 Residences	69	59	10	59	10	58	- 11	58	- 11	58	11	57	- 11	57	12
	MH7	1 Residence	73	63	10	63	10	63	10	63	- 11	62	11	62	11	62	- 11
	MH8	2 Residences	67	64	3	64	3	64	3	64	3	63	4	63	4	63	4
	MH9	2 Residences	63	60	3	60	3	60	3	60	3	59	4	59	5	58	5
	MH10	1 Residence	69	66	4	65	4	64	6	63	6	63	7	63	7	62	7
	R22	4 Residences	66	64	2	63	3	62	4	62	4	62	4	62	4	62	4
J	MJ1	3 Residences	67	63	4	62	5	61	6	61	6	60	7	60	7	60	7
	MJ2	3 Residences	64	60	3	60	4	59	5	59	5	59	5	59	5	58	5
									-								

	Table 4-2	Continued			Height Feet	Barrier 10 I	Height Feet	Barrier 12 I	0		Height Feet	Barrier I 16 Fe	0		Height Feet		Height Feet
NSA	Receptor Site	Site Representation	Future Build Noise Level (2045)	Mitigated Noise Level	Insertion Loss (IL)	Mitigated Noise Level	Insertion Loss (IL)	Mitigated Noise Level	Insertion Loss (IL)	Mitigated Noise Level	Insertion Loss (IL)						
	R23	2 Residences	67	64	3	62	4	61	5	61	6	60	6	60	7	60	7
	R25	4 Residences	67	63	4	62	5	61	6	60	7	60	7	59	8	59	8
	R25	4 Residences	66	65	1	64	2	62	3	62	4	61	4	61	5	61	5
	R26	4 Residences	69	68	1	68	2	66	3	66	3	66	4	66	4	66	4
	ML1	1 Residence	64	61	3	59	4	59	5	58	5	58	5	58	5	58	6
	ML2	2 Residences	63	59	4	58	4	58	5	57	6	57	6	57	6	56	6
	ML3	2 Residences	65	61	4	59	5	58	6	58	7	57	8	57	8	57	8
	MM1	3 Residences	70	68	2	68	2	68	2	66	4	65	5	65	5	65	5
	MM2	4 Residences	73	71	2	70	3	70	3	68	5	67	6	67	6	66	7
L/M	MM3	4 Residences	72	70	2	69	3	68	4	66	6	65	7	64	8	64	8
	MM4	3 Residences	68	67	2	66	2	66	3	64	5	63	6	62	6	62	7
	MM5	4 Residences	69	67	2	67	2	65	4	64	6	63	7	62	7	62	7
	MM6	4 Residences	71	68	2	68	3	67	4	65	6	64	7	63	7	63	8
	MM7	4 Residences	74	72	2	71	3	70	4	68	7	66	8	65	9	65	10
	MM8	2 Residences	71	68	3	67	4	65	7	64	7	63	8	62	9	62	9
	MM9	3 Residences	68	63	5	62	6	61	7	61	8	60	8	60	9	59	9
	MM10	3 Residences	70	64	6	63	7	62	8	61	8	61	9	60	9	60	10
	MM11	2 Residences	67	65	2	62	4	61	6	61	6	60	7	60	7	60	7
	MM12	1 Residence	66	62	4	61	5	60	6	60	7	59	7	59	7	59	7
N	MN1	4 Offices	77	66	10	65	12	64	13	63	14	62	15	61	15	61	16
0	M01	1 Residence	68	67	1	67	1	67	1	66	2	66	2	65	3	64	4
	*	Impacted Reco	-								Note: NSA NSA K was All Alternati Barriers C/I Barriers F a Barriers H I	levels docur K was not inclu determined to ives. D and L/M have bas been optimi as been optimi	ided in the A be "not reas been optim optimized ized at 12 fe	Iternative 2 conable" do nized at 14 fo at 8 feet. cet.	B Mitigation to cost calcu	Evaluation.	

Table 4-3 I-80 Reconstruction Project																	
							Alter	native 2D Mitigation (Ū								
				Barrier	Height		Height	Barrier			Height	Barrier	Height	Barrier	Height	Barrie	r Height
			Future Build	8 Feet		10 Feet		12 Feet		14 Feet		16 Feet		18 Feet		20 Feet	
NSA	Receptor Site	Site Representation	Noise Level (2045)	Mitigated Noise Level	Insertion Loss (IL)												
A1	R1-A1	1 Residence	66	62	4	60	5	60	6	59	7	58	7	58	8	58	8
	M1-A1	2 Residences	65	62	4	60	6	59	7	58	7	58	7	58	8	58	8
Α	MA3	2 Residences	67	61	6	60	7	60	7	60	8	60	8	59	8	59	8
	MA4	3 Residences	64	61	3	61	4	60	4	60	4	60	4	60	4	60	4
В	B Not Warranted																
С	R8	2 Residences	63	62	1	61	2	61	2	60	3	60	3	60	3	59	4
	R9	2 Residences	67	62	4	62	5	62	5	61	5	61	6	60	6	60	7
	R10	1 Residence	64	61	3	61	3	61	3	60	4	60	4	59	5	59	5
	MC2	3 Residences	66	63	4	61	5	61	6	60	6	60	7	59	7	59	8
	MC3	3 Residences	68	65	3	64	4	63	5	62	6	61	7	60	7	60	8
	MC4	1 Residence	67	66	1	65	2	64	3	64	3	63	3	63	4	62	4
	MC5	3 Residences	66	63	3	62	4	61 63	5	61 63	5	60	6	60 62	6	59 62	7
	MC6	2 Residences 2 Residences	65	65 65	1	64 64	2	63	3	63	3	62 62	3	62	4	62	4
	MC7 MC8	2 Residences 2 Residences	66 65	63	2	63	3	62	3	61	4	61	4	60	5	60	6
	MC8 MC9	2 Residences 2 Residences	64	61	2	60	4	60	4	59	5	59		59	5	58	6
	MC10	2 Residences	65	64	1	63	2	62	3	62	4	61	4	61	5	60	5
	MC10 MC11	4 Residences	65	62	3	61	3	60	4	60	5	59	6	59	6	59	6
	MC12	5 Residences	65	62	4	61	4	60	5	60	5	59	6	59	6	59	7
	MC13	4 Residences	64	62	2	61	4	60	4	59	5	59	6	58	6	58	6
	MC14	2 Residences	65	62	3	60	4	59	5	59	6	58	6	58	7	58	7
	MC15	5 Residences	64	61	2	60	3	59	5	58	5	58	6	57	6	57	7
	MC16	2 Residences	65	62	4	60	5	59	6	59	7	58	7	58	8	57	8
	MC17	3 Residences	63	60	2	60	3	58	4	58	5	57	6	57	6	56	7
	MC18	2 Residences	64	61	3	60	4	59	5	58	6	57	6	57	7	57	7
	MC19	3 Residences	64	61	3	60	4	59	5	58	6	57	7	57	7	57	8
D	R11	1 Residence	66	64	2	63	3	62	4	61	6	60	6	59	7	58	8
	R12	2 Residences	66	64	2	64	2	63	3	63	3	62	4	61	5	60	6
	R13	2 Residences	68	66	2	65	3	65	3	64	4	63	5	62	5	61	6
	MD1	1 Residence	66	62	4	61	5	60	6	59	7	59	7	58	8	58	8
	MD2	2 Residences	60	59	1	59	2	59	2	58	3	56	4	56	5	55	5
	MD3	2 Residences	63	61	2	60	3	59 60	4	58 59	5	57	6	57	6 5	56	6
	MD4 MD5	2 Residences 2 Residences	62 63	60 62	2	60 62	2	60 62	2	59 61	3	58 60	4	57 59	5	57 58	5
	MD5 MD6	2 Residences 2 Residences	63 64	62	1	62	2	62 62	2	61	3	60	4	59 60	4	58 59	4
	MD6 MD7	2 Residences 2 Residences	66	62 62	3	62 61	4	62 61	4	61	5	60	4	60 60	4	59 60	6
	MD7 MD8	2 Residences 2 Residences	67	61	5	61	6	61	6	61	6	61	6	60	7	60	7
	MD8 MD9	2 Residence	66	61	6	60	6	60	6	59	7	59	7	58	8	58	8
	MD9	1 Residence	00	01	0	00	0	00	0	37	1	37	- 1	50	0	50	0

	Table 4-3	Continued	Future Build	Barrier 8 F	Height eet	Barrier 10 I	0		Height Feet		Height Feet		Height Feet	Barrier 18 I	Height Feet	Barrier 20 I	Height Feet
NSA	Receptor Site	Site Representation	Noise Level (2045)	Mitigated Noise Level	Insertion Loss (IL)												
	R1-C2	3 Residences	65	57	8	56	9	55	10	55	10	54	11	54	11	53	12
	M1-C2	4 Residences	62	58	0 4	57	9 5	57	5	57	5	57	5	57	5	57	5
C2	M1-C2 M2-C2	2 Residences	58	54	4	54	5	53	5	53	6	53	6	52	6	52	6
	M2-C2 M3-C2	2 Residences 2 Residences	58 66	59	7	58	8	57	9	57	9	56	10	56	10	55	11
	N13-C2	2 Residences	00	37	1	- 58	0	51	,	51		50	10	50	10	35	11
	R15	1 Residence	75	67	8	66	9	65	10	64	- 11	63	12	62	13	61	14
	R16	3 Residences	61	59	2	58	3	58	3	57	4	57	5	56	5	56	5
	R17	5 Residences	63	60	4	59	4	59	5	58	5	58	5	58	6	57	6
F	MF1	1 Residence	65	64	0	64	0	64	0	64	0	64	0	64	1	64	1
Î.	MF2	5 Residences	68	63	5	63	5	62	6	61	7	61	7	60	8	60	8
	MF3	4 Residences	63	61	1	61	2	60	2	60	3	60	3	59	3	59	3
	MF4	4 Residences	67	62	6	61	6	60	7	60	7	59	8	59	8	58	9
	MF5	2 Residences	65	60	5	59	6	59	6	58	7	57	8	57	8	56	9
	R20	4 Residences	57	54	3	54	3	54	3	54	3	54	3	53	3	53	3
	R21	1 Residence	73	69	4	68	5	68	6	67	6	67	6	67	7	66	7
	MH1	4 Residences	47	47	0	47	0	47	0	47	0	47	0	47	0	47	0
	MH2	4 Residences	49	49	0	49	0	49	0	49	0	49	0	49	0	49	0
	MH3	3 Residences	65	60	5	60	5	59	5	59	6	59	6	59	6	58	7
	MH4	4 Residences	55	55	0	55	0	55	0	55	0	55	0	55	0	55	0
н	MH5	3 Residences	68	60	7	60	8	60	8	59	8	59	9	59	9	59	9
	MH6	2 Residences	67	59	8	59	8	58	9	58	9	58	9	57	10	57	10
	MH7	1 Residence	71	63	8	63	8	63	9	63	9	62	9	62	9	62	10
	MH8	2 Residences	66	64	2	64	2	64	2	64	2	63	3	63	3	63	3
	MH9	2 Residences	63	61	2	60	2	60	3	60	3	59	3	59	4	58	4
	MH10	1 Residence	69	66	3	64	5	63	6	63	6	62	7	62	7	62	7
	D 22	4		(4	2	(2	2	0	2	0	2	6	2	6	2	(2)	
	R22	4 Residences	65	64	2	63	2	62	3	62	3	62	3	62	3	62	3
J	MJ1	3 Residences	67	63	3	62 60	5	61 50	5	61 58	6	60	6 5	60 58	6	60	,
	MJ2	3 Residences	63	61	2	60	3	59	4	58	5	58	3	58	5	58	5

	Table 4-3	Continued	Estern De 11	Barrier 8 F	Height eet		Height Feet	Barrier 12 I	U	Barrier 14 I	U		Height Feet	Barrier 18 I	Height Feet		Height Feet
NSA	Receptor Site	Site Representation	Future Build Noise Level (2045)	Mitigated Noise Level	Insertion Loss (IL)	Mitigated Noise Level	Insertion Loss (IL)	Mitigated Noise Level	Insertion Loss (IL)	Mitigated Noise Level	Insertion Loss (IL)						
							-			-			-	-		-	
	R23	2 Residences	70	63	7	62	8	61	9	61	9	60	10	59	11	59	11
	R23	4 Residences	69	63	6	62	7	61	8	60	9	59	10	59	10	59	10
	R25	4 Residences	70	66	4	64	6	63	7	63	7	62	8	62	8	62	8
	R26	4 Residences	70	68	2	66	4	65	6	64	7	63	7	63	7	63	8
	ML1	1 Residence	64	61	3	60	4	59	5	59	5	59	5	59	5	59	5
	ML2	2 Residences	63	59	4	58	5	58	5	57	6	57	6	57	6	57	6
	ML3	2 Residences	65	60	5	59	6	59	6	58	7	58	7	57	8	57	8
	MM1	3 Residences	70	68	2	68	2	67	3	64	6	63	7	63	7	62	8
	MM2	4 Residences	74	71	3	70	4	70	4	67	7	66	8	65	9	64	10
L/M	MM3	4 Residences	73	70	3	69	4	69	4	66	7	65	9	64	9	63	10
	MM4	3 Residences	69	67	3	66	3	66	4	63	6	62	7	62	8	61	8
	MM5	4 Residences	70	67	3	67	3	66	4	64	7	62	8	62	8	62	9
	MM6	4 Residences	72	69	3	68	4	68	4	65	7	63	9	63	9	62	10
	MM7	4 Residences	76	72	4	71	4	71	5	67	8	65	10	64	11	64	12
	MM8	2 Residences	72	68	4	67	5	65	7	64	9	63	9	63	10	62	10
	MM9	3 Residences	69	63	6	62	7	61	8	60	9	60	9	59	10	59	10
	MM10	3 Residences	70	63	7	62	8	61	9	61	9	60	10	60	10	60	11
	MM11	2 Residences	67	64	3	63	5	62	6	61	6	61	7	61	7	61	7
	MM12	1 Residence	67	61	5	61	6	60	7	60	7	59	7	59	8	59	8
Ν	MN1	4 Offices	77	73	4	72	5	68	8	67	10	66	11	66	11	65	12
0	MO1	1 Residence	66	66	0	66	0	66	1	65	1	65	1	64	2	63	3
	*	Impacted Rec Protected Res	-								Note: NSA Evaluation calculation Barrier C/D Barriers C2 Barrier H h Barrier J ha	K was not ir NSA K was for All Alterr has been o	ncluded in the s determined natives. ptimized at been optim mized at 12 mized at 20	iized at 8 fee feet. feet.	e 2D Mitigati reasonable"	ion	

		Noise Abate	I-80 Reconst ement Feasibilit		oject oleness Evaluation		
NSA	Number of Benefited Receptors	Combined Noise Barrier Length	Feasible Noise Barrier Height	Square Footage	Total sf. per benefit (max 2000 sf.)	Feasible?	Reasonable?
A1	1	1,344	20	26,880	26,880	Yes	NO
Α	18	3,000	12	36,000	2,000	Yes	YES
В	50	1,761	12	21,132	423	Yes	YES
С	36	2,575	14	36,050	1,001	Yes	YES
D	2	1,780	10	17,800	8,900	Yes	NO
F	12	1,366	10	13,660	1,138	Yes	YES
G	2	640	18	11,520	5,760	Yes	NO
H* J*	-			Not Feasib	ole		
K**	0.06	2,188	10	21,880	364,667	Yes	NO
L/M	45	2,060	14	28,840	641	Yes	YES
Ν	4	1,065	8	8,520	2,130	Yes	NO
0	1	1,000	20	20,000	20,000	Yes	NO
* **				•	b) of impacted receptor each benefitted site; PU		E, Table E2.

	Table 5-2 I-80 Reconstruction Project Noise Abatement Feasibility/Reasonableness Evaluation Alternative 2B											
NSA	Number of Benefited Receptors	Combined Noise Barrier Length	Feasible Noise Barrier Height	Square Footage	Total sf. per benefit (max 2000 sf.)	Feasible?	Reasonable?					
A1	3	1,383	10	13,830	4,610	Yes	NO					
Α	3	2,952	20	59,040	19,680	Yes	NO					
C/D	43	4,172	14	58,408	1,358	Yes	YES					
F	12	975	8	7,800	650	Yes	YES					
Н	15	1,614	12	19,368	1,291	Yes	YES					
J	6	853	16	13,648	2,275	Yes	NO					
L/M	45	2,454	14	34,356	763	Yes	YES					
N	4	902	8	7,216	1,804	Yes	YES					
11	Not Feasible											

	Table 5-3 I-80 Reconstruction Project Noise Abatement Feasibility/Reasonableness Evaluation Alternative 2D											
NSA	Number of Benefited Receptors	Combined Noise Barrier Length	Feasible Noise Barrier Height	Square Footage	Total sf. per benefit (max 2000 sf.)	Feasible?	Reasonable?					
Α	2	959	10	9,590	4,795	Yes	NO					
A1	3	1,502	12	18,024	6,008	Yes	NO					
C/D	54	4,205	16	67,280	1,246	Yes	YES					
C2	5	655	8	5,240	1,048	Yes	YES					
F	12	1,019	8	8,152	679	Yes	YES					
Н	11	1,614	12	19,368	1,761	Yes	YES					
J	6	853	20	17,060	2,843	Yes	NO					
L/M	25	2,756	10	27,560	1,102	Yes	YES					
Ν	4	1,065	12	12,780	3,195	Yes	NO					
O *				Not Feasib	le	-						
* Note:					%) of impacted receptor asonable under all Alter							

				Table Noise Impact S					
NSA	Number of Land Uses		Number	Noise Mitigation Evaluation**					
		Existing Worst Case	Future No-Build	Alternative 2A	Alternative 2B	Alternative 2D	Warranted?	Feasible?	Reasonable?
A1	3	0	1	1	3	1	A,B,D	A,B,D	
А	23	5	5	14	3	2	A,B,D	A,B,D	А
В	54	13	31	40	0	0	А	А	А
С	57	25	25	42	33	14	A,B,D	A,B,D	A,B,D
C2	11	2	5	0	0	2	D	D	D
D	22	1	2	4	9	11	A,B,D	A,B,D	B,D
D2	8	0	0	0	0	0			
Е	11	0	0	0	0	0			
F	31	6	10	17	12	10	A,B,D	A,B,D	A,B,D
G	10	2	2	2	0	2			
Н	33	4	4	4	10	6	A,B,D	B,D	B,D
J	10	3	10	7	7	3	A,B,D	B,D	
K	0.13	0.04	0.06	0.09	0.09	0.1	A,B,D	A,B,D	
L	5	0	0	2	0	0	А	A,B,D	A,B,D
М	51	49	51	51	51	51	A,B,D	A,B,D	A,B,D
Ν	4	4	4	4	4	4	A,B,D	A,B,D	В
0	1	1	1	1	1	1	A,B,D	А	
Total	334	115	151	189	133	107			

* - Reference Table 2 and Tables 4-1 through 4-3 for complete results.

** - Reference Tables 5-1 through 5-3 for complete results.

APPENDIX A

NOISE METER AND ACOUSTICAL CALIBRATOR CALIBRATION CERTIFICATES

Certificate number: 2KNC0171 Issue date: 25/12/2012 (DD/MM/YYYY)

CALIBRATION CERTIFICATE

Customer name:

Scantek, Inc.

Product type:	SOUND CALIBRATOR
Model name:	NC - 74
Serial number:	35125820
Calibration date:	27/11/2012 (DD/MM/YYYY)
Ambient condition:	Temperature 25 °C Relative Humidity 41 %

We hereby certify that the above product was tested and calibrated according to the prescribed RION procedures, and that it fulfills all specification requirements, as listed on the appended sheet. The measuring equipment and reference devices used for testing and calibrating this unit are managed under the RION traceability system and are traceable according to official Japanese standards and official standards of countries belonging to the International Committee of Weights and Measures.

RION primary standards

Model	Model number	Controlled number	Cal due date
(Acoustic)			
Condenser microphone	4160	1843697	02/2014
(Electric)			
DC Reference standard	732B	6265015	09/2014
Standard resistor	742A-1	6480018	11/2013
Standard resistor	742A-10k	6390001	06/2014
Digital multimeter	3458A	2823A13632	03/2013
Universal counter	53132A	MY40005574	08/2013
Distortion Meter	VA-2230A	11076061	12/2012

RION working standards

Model	Model number	Controlled number	Cal due date
(Acoustic) Condenser microphone	4160	CM-0335	10/2013
(Electric) Measuring amplifier	NA-42SK	NA-1063	12/2012

Manager, Quality Control Dept.



CALIBRATION CERTIFICATE

Customer name:

Scantek, Inc.

Product type:SOUND LEVEL METERModel name:N L - 4 2Serial number:0 1 2 2 2 8 9 1Calibration date:21/01/2013 (DD/MM/YYYY)Ambient condition :Temperature 25 °C Relative Humidity 38 %

We hereby certify that the above product was tested and calibrated according to the prescribed RION procedures, and that it fulfills all specification requirements, as listed on the appended sheet. The measuring equipment and reference devices used for testing and calibrating this unit are managed under the RION traceability system and are traceable according to official Japanese standards and official standards of countries belonging to the International Committee of Weights and Measures.

Verification Standard for Acoustics

Model	Model number	Controlled number	Cal due date
(Acoustic) Condenser microphone	4160	1843696	03/2013
RION primary standards			
Model	Model number	Controlled number	Cal due date
(Electric)			
DC Reference standard	732B	6265015	09/2014
Standard resistor	742A-1	6480018	11/2013
Standard resistor	742A-10k	6390001	06/2014
Digital multimeter	3458A	2823A13632	03/2013
Universal counter	53132A	3404A01375	03/2013
ION working standards			
Model	Model number	Controlled number	Cal due date
(Acoustic)			
Condenser microphone for sound level meter	UC-33P	CM-0332	07/2013
Sound level meter	NA-42改	NA-1104	07/2013
(Electric)			
Sound level meter	NA-42改	NA-1104	07/2013
Attenuator	TPA-302B	AT-1134	10/2013
Function generator	33120A	SY-1152	03/2013

larungamon Manager, Quality Control Dept.

Certificate number: 3 K N L 0 0 1 3 Issue date: 29/01/2013 (DD/MM/YYYY)

CALIBRATION CERTIFICATE

Customer name:

Scantek, Inc.

Product type:SOUND LEVEL METERModel name:N L - 4 2Serial number:0 1 2 2 2 8 7 5Calibration date:21/01/2013 (DD/MM/YYYY)Ambient condition :Temperature 25 °C Relative Humidity 38 %

We hereby certify that the above product was tested and calibrated according to the prescribed RION procedures, and that it fulfills all specification requirements, as listed on the appended sheet. The measuring equipment and reference devices used for testing and calibrating this unit are managed under the RION traceability system and are traceable according to official Japanese standards and official standards of countries belonging to the International Committee of Weights and Measures.

Verification Standard for Acoustics

Model	Model number	Controlled number	Cal due date
(Acoustic)			
Condenser microphone	4160	1843696	03/2013
RION primary standards			
Model	Model number	Controlled number	Cal due date
(Electric)			
DC Reference standard	732B	6265015	09/2014
Standard resistor	742A-1	6480018	11/2013
Standard resistor	742A-10k	6390001	06/2014
Digital multimeter	3458A	2823A13632	03/2013
Universal counter	53132A	3404A01375	03/2013
RION working standards			
Model	Model number	Controlled number	Cal due date
(Acoustic)			
Condenser microphone for sound level meter	UC-33P	CM-0332	07/2013
Sound level meter	NA-42改	NA-1104	07/2013
(Electric)			
Sound level meter	NA-42改	NA-1104	07/2013
Attenuator	TPA-302B	AT-1134	10/2013
	33120A	SY-1152	03/2013

Manager, Quality Control Dept.



20110516-3

Certificate number: 3 K N L 0 0 1 1 Issue date: 29/01/2013 (DD/MM/YYYY)

CALIBRATION CERTIFICATE

Customer name:

Scantek, Inc.

Product type:SOUND LEVEL METERModel name:N L - 4 2Serial number:0 1 2 2 2 8 7 3Calibration date:21/01/2013 (DD/MM/YYYY)Ambient condition :Temperature 25 °C Relative Humidity 38 %

We hereby certify that the above product was tested and calibrated according to the prescribed RION procedures, and that it fulfills all specification requirements, as listed on the appended sheet. The measuring equipment and reference devices used for testing and calibrating this unit are managed under the RION traceability system and are traceable according to official Japanese standards and official standards of countries belonging to the International Committee of Weights and Measures.

Verification Standard for Acoustics

Model	Model number	Controlled number	Cal due date
(Acoustic)			
Condenser microphone	4160	1843696	03/2013
RION primary standards			
Model	Model number	Controlled number	Cal due date
(Electric)			
DC Reference standard	732B	6265015	09/2014
Standard resistor	742A-1	6480018	11/2013
Standard resistor	742A-10k	6390001	06/2014
Digital multimeter	3458A	2823A13632	03/2013
Universal counter	53132A	3404A01375	03/2013
RION working standards			
Model	Model number	Controlled number	Cal due date
(Acoustic)			
Condenser microphone for sound level meter	UC-33P	CM-0332	07/2013
Sound level meter	NA-42改	NA-1104	07/2013
(Electric)			
Sound level meter	NA-42改	NA-1104	07/2013
Attenuator	TPA-302B	AT-1134	10/2013
Function generator	33120A	SY-1152	03/2013

1. V lawing ama Manager, Quality Control Dept.



Certificate number: 3 K N L 0 0 1 5 Issue date: 29/01/2013 (DD/MM/YYYY)

CALIBRATION CERTIFICATE

Customer name: Scar

Scantek, Inc.

Product type:SOUND LEVEL METERModel name:N L - 4 2Serial number:0 1 1 2 2 5 8 0Calibration date:08/01/2013 (DD/MM/YYYY)Ambient condition :Temperature 25 °C Relative Humidity 38 %

We hereby certify that the above product was tested and calibrated according to the prescribed RION procedures, and that it fulfills all specification requirements, as listed on the appended sheet. The measuring equipment and reference devices used for testing and calibrating this unit are managed under the RION traceability system and are traceable according to official Japanese standards and official standards of countries belonging to the International Committee of Weights and Measures.

RION primary standards

Model number	Controlled number	Cal due date
4160	1843697	02/2014
732B	6265015	09/2014
742A-1	6480018	11/2013
742A-10k	6390001	06/2014
3458A	2823A13632	03/2013
53132A	3404A01375	03/2013
	4160 732B 742A-1 742A-10k 3458A	4160 1843697 732B 6265015 742A-1 6480018 742A-10k 6390001 3458A 2823A13632

RION working standards

Model	Model number	Controlled number	Cal due date
(Acoustic) Condenser microphone	UC-27	CM-0300	01/2013
(Electric)			
Measuring amplifier	XN-88	NA-1036	01/2013
Attenuator	TPA-302B	AT-1145	07/2013
Function generator	33120A	SY-1146	09/2013

CU.V aruya Manager, Quality Control Dept.



Certificate number: 3 K N L 0 0 1 2 Issue date: 29/01/2013 (DD/MM/YYYY)

CALIBRATION CERTIFICATE

Customer name:

Scantek, Inc.

Product type:SOUND LEVEL METERModel name:N L - 4 2Serial number:0 1 2 2 2 8 7 4Calibration date:21/01/2013 (DD/MM/YYYY)Ambient condition :Temperature 25 °C Relative Humidity 38 %

We hereby certify that the above product was tested and calibrated according to the prescribed RION procedures, and that it fulfills all specification requirements, as listed on the appended sheet. The measuring equipment and reference devices used for testing and calibrating this unit are managed under the RION traceability system and are traceable according to official Japanese standards and official standards of countries belonging to the International Committee of Weights and Measures.

Verification Standard for Acoustics

Model	Model number	Controlled number	Cal due date
(Acoustic) Condenser microphone	4160	1843696	03/2013
RION primary standards			
Model	Model number	Controlled number	Cal due date
(Electric)			
DC Reference standard	732B	6265015	09/2014
Standard resistor	742A-1	6480018	11/2013
Standard resistor	742A-10k	6390001	06/2014
Digital multimeter	3458A	2823A13632	03/2013
Universal counter	53132A	3404A01375	03/2013
RION working standards			
Model	Model number	Controlled number	Cal due date
(Acoustic)			-
Condenser microphone for sound level meter	UC-33P	CM-0332	07/2013
Sound level meter	NA-42改	NA-1104	07/2013
(Electric)			
Sound level meter	NA-42改	NA-1104	07/2013
Attenuator	TPA-302B	AT-1134	10/2013
Function generator	33120A	SY-1152	03/2013

Manager, Quality Control Dept.

APPENDIX B Noise Monitoring Data Forms

I-80 Recon	I-80 Reconstruction Project
Site # R1 Description : 300 Tanite Rd, Stroudsburg, PA 18360 Meter # 1	
: JND/JCL ing Data: AM Peak Off-Peak PM Peak Date 7/16/13	Atmospheric Data
Time 12:10 PM 12:20 PM 12:20 PM 12:20 PM MIN 10 MIN MIN	Wind Speed (mph) 5 - 8 Temp. (°F)
way tion c Count: 0 0 0 0 0 0	60 60
Site Data: Site Surface (alpha): Shielding Factor : Pavement Type :	
ED COL	AM Peak:
	Off-Peak:
Profile View:	
Fome view:	
McCormick Taylor, Inc	

McCormick Taylor, Inc	Profile View:	Site Data: Site Surface (alpha): Shielding Factor : Pavement Type :	*# 5 By: JCL/AD AM Peak Off-Peak PM Peak Start Time 8:25 AM MIN MIN Leq. Leq. MIN MIN MIN Direction 15 MIN MIN MIN MIN Direction EB WB Beech St MIN MIN MT 194 170 12 0 0 0 0 MT 194 170 12 0	I-80 Recon Site # R1-A1 Description : 314 Beech St, Stroudsburg, PA 18360
	Off-Peak:	AM Peak: Beech St - 30 mph Monitoring Notes	Atmospheric Data Wind Speed (mpb) Temp. (°F) Humidity (%)	I-80 Reconstruction Project

	1-80	I-80 Reconstruction Project
Site # R1-C2	Description: 1927 Arlington Ave, Stroudsburg, PA 18360	ourg, PA 18360
Meter # 1 Done By: JCL/AD		
Monitoring Data: Date Start Time End Time Duration Leq.	AM Peak 7/23/14 9:10 AM 9:25 AM 15 MIN MIN MIN MIN	Atmospheric Data (mph) Temp. (°F)
Traffic Data Roadway Direction Traffic Count: Cars MT HT HT	209 Arlington 177 106 165 9 4 4 0 0	
Site Data: Site Surface (alpha):	Shielding Factor:	Pavement Type : Monitoring Notes
		AM Peak: 209 - 55 mph Arlington Ave - 30 mph
	le le le le le le le le le le le le le l	Off-Peak:
	ton A	PM Peak
McCormick Taylor, Inc		

Site # RLO2 Description: 1020 Delay: 80. Biology, PA 16300 Meter #
--

			I-80 R	I-80 Reconstruction Proj	tion Project
Site # R2-D2	Description :	1238 Dewberry	1238 Dewberry Ln, Stroudsburg, PA 18360	PA 18360	
Meter # 1 Done By: JCL/AD					
Monitoring Data: Date Start Time	AM Peak 7/23/14	Off-Peak	PM Peak	Atmospheric Data Wind Speed	
End Time Duration	10:12 CM 10:27 15 MIN	MIN	Min	(mph) Temp. (°F)	
Traffic Data Roadway Direction	-	-		Humidity (%)	
Traffic Count: Cars MT HT HT	0	0	0		
Site Data: Site Surface (alpha):		Shielding Factor :	Pavement Type :	t Type :	
				Z	AM Peak:
C			-	=	
	P. C.	ALC .			
Aney	S* ·			E.	Off-Peak:
			19	R	
		tout -			PM Peak
Profile View:	A MANUAL PROPERTY.		() K	A DATE OF	
McCormick Taylor, Inc	alm)				

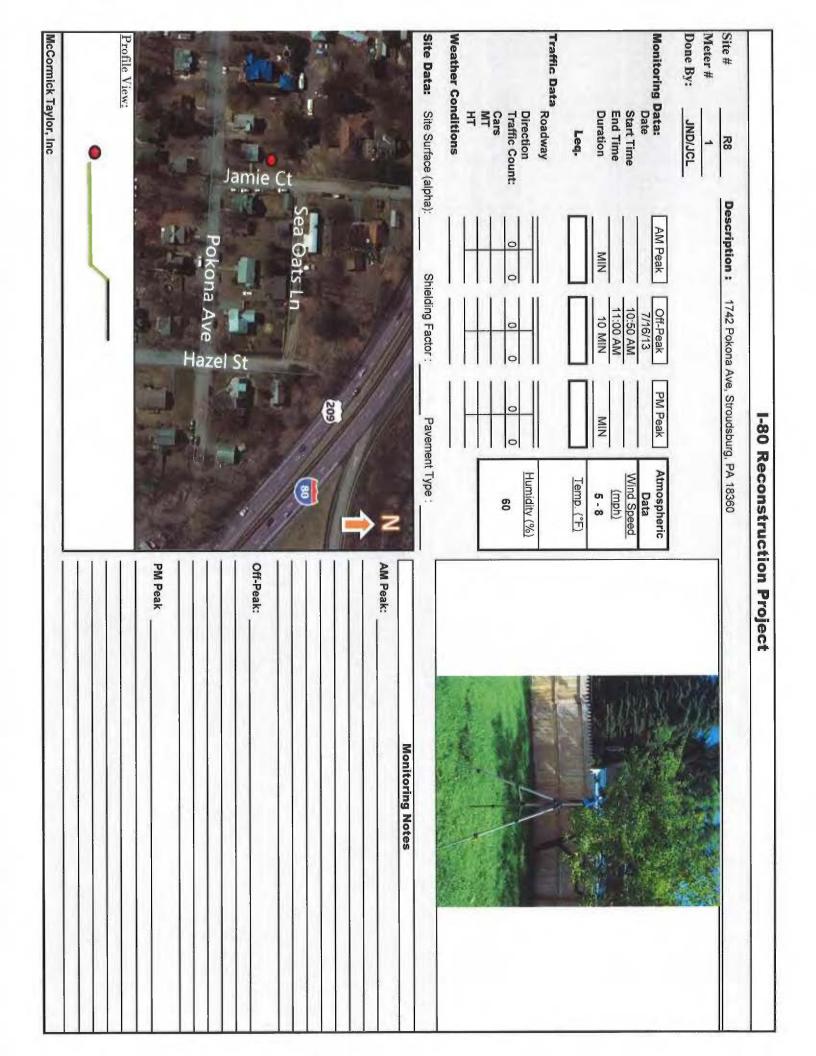
Description : 227 Tanite Rd, Stroudsburg, PA 1 AM Peak Off-Peak 7/16/13 PM Peak	ion Project
Time AM Peak Off-Peak 7/16/13 Time II:20 PM 12:20 PM 12:20 PM 12:20 PM 12:20 PM 12:20 PM 10 UN UN 10 MIN 10 MIN 10 UN 1	
Site Data: Site Surface (alpha): Shielding Factor : Pavement Type :	Monitoring Notes
	AM Peak:
A since Ro	Off-Peak:
Profile View:	PM Peak
McCormick Taylor, Inc	

I-80 Rec Site # R4 Description : 80 Bridge St, Stroudsburg, PA 18360 Meter # 1	I-80 Reconstruction Project
: JN Data: Starl End Dura	Atmospheric Data Wind Speed (mph) 5 - 8
Traffic Data Roadway Direction Traffic Count: O O Cars O MT O HT O HT <t< td=""><td>50</td></t<>	50
Site Data: Site Surface (alpha): Shielding Factor : Pavement Type :	Type :
aaaaa	AM Peak:
19	PM Peak
Profile View:	
McCormick Taylor, Inc	

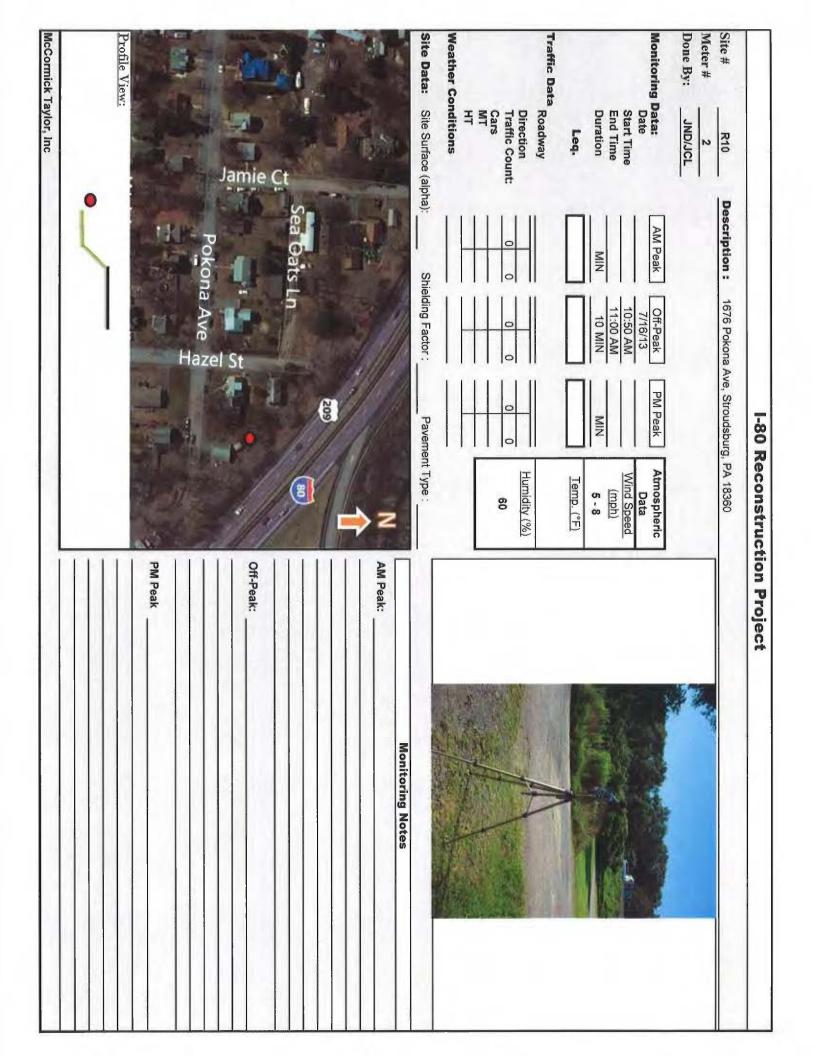
I-80 Reconstruction Pro	on Project
Site # Ko Description - */2 bitige of, onourspury, inclosed Meter # 5 Done By: JND/JCL	
Monitoring Data: AM Peak Off-Peak PM Peak Dfreek Date Start Time 7/16/13 Data Data Start Time 11:20 AM 11:30 AM Wind Speed Duration MIN 10 MIN 5 - 8 Leq. Temp. (°F)	
Traffic Data Roadway Direction Traffic Count: Cars 0 0 0 0 MT HT 0 0 0 0 0 WT HT 0 0 0 0 0 0 0 Wather Conditions HT HT	
Site Data: Site Surface (alpha): Shielding Factor : Pavement Type :	Monitoring Notes
	AM Peak:
	Off-Peak:
Fairgroup	PM Peak
Profile View:	
McCormick Taylor, Inc	

I-80 Ro Site # R6 Description : Miller St, Stroudsburg, PA 18360	I-80 Reconstruction Project
# 2 By: JND/JCL	
Monitoring Data:AM PeakOff-PeakFDate7/16/13Start Time11:20 AMEnd Time11:30 AMDurationMIN10 MIN	PM Peak Atmospheric Data Wind Speed (mph) 5-8
Leq.	Temp. (°F)
Traffic Data Roadway	
Noadway Direction Traffic Count: 0 0 0 0 Cars MT HT	0 0 60
Site Data: Site Surface (alpha): Shielding Factor :	Pavement Type :
	Monitoring Notes
	AM Peak:
Ande -	Off-Peak:
airgroun	
Profile View:	PM Peak
l	
McCormick Taylor, Inc	

Nice: F Description 1: 130 Mirrls St, Stondard Pr A tool Morei By:
--



Site # B Description: 112 Pearl SI, Straudsburg, PA 18307 Moler # B Image: Trans Minage: Trans Minage: Trans Len Minage: Trans Minage: Trans Minage: Trans Minage: Trans Len Minage: Trans Minage: Trans Minage: Trans Minage: Trans Minage: Trans Minage: Trans Mina



McCormick Taylor, Inc	Profile View:		Site Data: Site Surface (alpha): Shielding Factor : Pavement Type :	Traffic Data Roadway Image: Constrained by the second	Monitoring Data: AM Peak Off-Peak PM Peak Atmospheric Date 7/16/13 7/16/13 Data Data Start Time 9:25 AM 9:25 AM Mind Speed Mind Speed Duration MiN 10 MiN Min 5 - 8 Leq. Imp. ("F) 10 Mind Speed 10 Mind Speed	# 1 By: JND/JCL	Site # R11 Description: 119 Anna Ct, Stroudsburg, PA 18360	I-80 Reconstruction Pro
	Off-Peak:	Monitoring Notes AM Peak:						Project

	I-80 Reconstruction Project	
Site # R12 Description: 1230 Wade Ct E, S	1230 Wade Ct E, Stroudsburg, PA 18360	
# 5 By: JND/JCL		
AM Peak Off-Peak 7/16/13 9:25 AM 9:35 AM 10 MIN	PM Peak Atmospheric Data Mind Speed (mph) 5-8 Temp. (°F)	
Traffic Data Roadway		
Mathematical Conditions Image: Condition Condition Image: Condition Condition	o o o Humidity (%)	
Site Data: Site Surface (alpha): Shielding Factor :	Pavement Type :	
	AM Peak:	
	Off-Peak:	
Denny	PM Peak	
Profile View:		
McCormick Taylor, Inc		

	I-80 Reconstruction Project
Site # R13 Description : 1226 Wade Ct E, :	1226 Wade Ct E, Stroudsburg, PA 18360
# 2 By: JND/JCL	
Monitoring Data: Date Start Time End Time Duration Leq. MIN MIN MIN MIN MIN MIN MIN MIN MIN MIN	PM Peak Atmospheric Data MIN 5-8 Temp. (°E)
Traffic Data Roadway Direction Traffic Count: Cars 0 MT HT	0 0 (%)
Site Data: Site Surface (alpha): Shielding Factor :	Pavement Type :
	AM Peak:
	Off-Peak:
Profile View:	PM Peak
•	
McCormick Taylor, Inc	

McCormick Taylor, Inc	Profile View:			Site Data: Site Surface (alpha): Shielding Factor : Pavement Type :	Traffic Data Roadway Humidity (%) Direction Traffic Count: 0 <th>Monitoring Data: AM Peak Off-Peak PM Peak Atmospheric Date Start Time 7/16/13 9:25 AM Data Data End Time MIN 9:35 AM MIN MIN Seed (mph) Leq. MIN 10 MIN MIN 5 - 8 Temp. (°F)</th> <th># 4 By: JND/JCL</th> <th>I-80 Reconstruction Proj Site # R14 Description : 1222 Dreher Ave, Stroudsburg, PA 18360</th> <th></th>	Monitoring Data: AM Peak Off-Peak PM Peak Atmospheric Date Start Time 7/16/13 9:25 AM Data Data End Time MIN 9:35 AM MIN MIN Seed (mph) Leq. MIN 10 MIN MIN 5 - 8 Temp. (°F)	# 4 By: JND/JCL	I-80 Reconstruction Proj Site # R14 Description : 1222 Dreher Ave, Stroudsburg, PA 18360	
	PM Peak	Off-Peak:	Monitoring Notes AM Peak:					action Project	

I-80 Reconstruction Pro	on Project
Site # R15 Description : 796 Bryant St, Stroudsburg, PA 18360	
# 1 By: JND/JCL	
Monitoring Data: AM Peak Off-Peak PM Peak Atmospheric Date Start Time 7/16/13 Data Data End Time 8:45 AM 10 MiN MiN Start Start Leq. MiN 10 MiN 5 - 8 Temp. (°F)	
Traffic Data Roadway Humidity (%) Direction 0 <td></td>	
Site Data: Site Surface (alpha): Shielding Factor : Pavement Type :	
	montoning notes
	AM Peak:
Bryant St	Off-Peak:
	PM Peak
Profile View:	
McCormick Taylor, Inc	

I-80 Reconstruction Pro	on Project
Site # R16 Description : 765 Bryant St, Stroudsburg, PA 18360	
# 2 By: JND/JCL	
Monitoring Data: AM Peak Off-Peak PM Peak Atmospheric Date Start Time 7/16/13 Data Data Start Time 8:45 AM 10 MIN MiN Start Start Leq. MIN 10 MIN MIN 5 - 8 Image: Temp. (°F) Temp. (°F) Temp. (°F)	
Traffic Data Roadway Direction Traffic Count: 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
Site Data: Site Surface (alpha): Shielding Factor : Pavement Type :	
amant St N	AM Peak:
	Off-Peak:
Profile View:	PM Peak
McCormick Taylor, Inc	

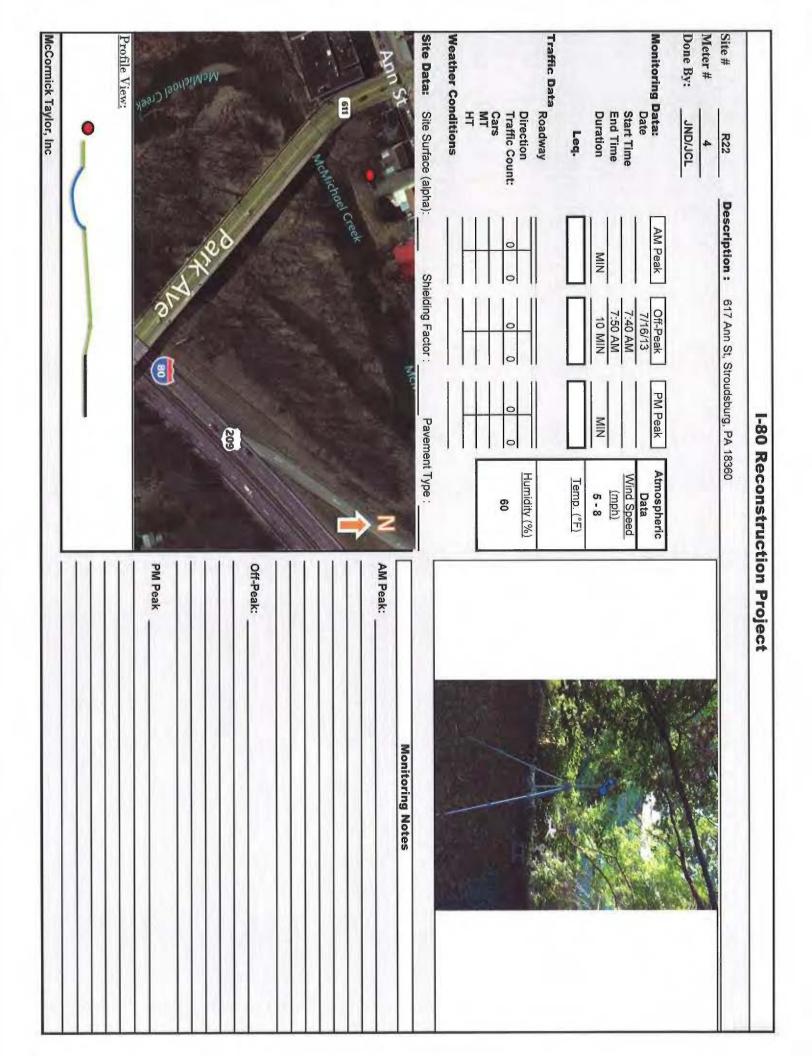
I-80 Reconstruction Pro	ction Project
Site # R17 Description : 736 Bryant St, Stroudsburg, PA 18360	
# 3 By: JND/JCL	
Monitoring Data: AM Peak Off-Peak PM Peak Atmospheric Date Start Time 7/16/13 Data Data End Time 8:45 AM Wind Speed (mph) Duration MIN 10 MIN 5 - 8 Leq. Temp. (°F) Temp. (°F)	
Traffic Data Roadway Direction Traffic Count: 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
Site Data: Site Surface (alpha): Shielding Factor : Pavement Type :	
	AM Peak:
Brya	Off-Peak:
Profile View	PM Peak
•	
McCormick Taylor, Inc	

I-80 Reconstruction Pro	on Project
Site # R18 Description : 542 Lenox St, Stroudsburg, PA 18360	
# 3 By: JND/JCL	
Monitoring Data: AM Peak Off-Peak PM Peak Atmospheric Date Start Time 7/16/13 20.4M 20.4M	
Traffic Data Roadway Direction Traffic Count: 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
Site Data: Site Surface (alpha): Shielding Factor : Pavement Type :	
	Monitoring Notes
THEd	AM Peak:
	Off-Peak:
ET LENOX 2	PM Peak
Profile View:	
McCormick Taylor Inc	

Site # R19 Description : 422 Colbert St, Stroudsburg, PA 18360 Meter # 1 Done By: JNDJ/CL Monitoring Data: AM Peak Date AM Peak Date AM Peak Date Min End Time Min Duration Min Leq. Min Traffic Data Min Cars 0 Mit 0 Mit 10 Min Mit Min Mit 10 Min Mit 0 Mit 10 Min Bielding Factor: Pavement Type :	ion Project
N THE REAL PROPERTY OF A REAL PR	
ign olbert St	Off-Peak:
	PM Peak
Profile View:	
McCormick Taylor, Inc	

McCormick Taylor, Inc	Profile View:	Colbert St. Colbert St.	But contract (album).	Site # R20 Description : 112 Lee Ave, Stroudsburg, PA 18360 Meter # 5 Done By: JND/JCL Monitoring Data: AM Peak Off-Peak Date Start Time AM Peak Off-Peak End Time MIN B:10 AM MIN Leq. MIN 10 MIN MIN Traffic Data MIN MIN MIN Direction Traffic Count: 0 0 0 0 MIT MIT MIN MIN Temp. (*F) MIT MIT MIN Ste Data Stie Surface (alpha):	
	PM Peak	Off-Peak:	AM Peak:		ction Project

	I-80 Reconstruction Project	
Site # R21 Description : 210 Colb	210 Colbert St, Stroudsburg, PA 18360	
# 2 By: JND/JCL		
Monitoring Data: AM Peak Off-Peak 7/16/13 Start Time End Time MIN 10 MIN 10 MIN	MIN PM Peak	
Leq.		
Traffic Data Roadway Direction Traffic Count: 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
Site Data: Site Surface (alpha): Shielding Factor :	tor : Pavement Type :	
the second second		Monitoring Notes
	AM Peak:	
L'IP		
	Off-Peak:	
Colbert St	PM Peak	
Profile View:		
McCormick Taylor, Inc		



I-80 Recc 2 3/JCL AM Peak Off-Peak PM Peak	ion Project
Off-Peak 7/16/13 10:10 AM 10:20 AM 10 MIN MIN	
Traffic Data Roadway Direction Traffic Count: Cars 0 <t< td=""><td></td></t<>	
Site Data: Site Surface (alpha): Shielding Factor : Pavement Type :	
	AM Peak:
	Off-Peak:
Profile View:	PM Peak
McCormick Taylor, Inc	

R24	I-80 Reconstr Description: 41-43 Garden St, Stroudsburg, PA 18360	I-80 Reconstruction Project udsburg, PA 18360
-# <u>4</u> By: <u>JND/JCL</u>		
Monitoring Data: Date Start Time End Time Duration Leq.	AM Peak Off-Peak PM Peak Atmospheric 7/16/13 10:10 AM Data 10:20 AM Wind Speed 10 MIN MIN 5 - 8 Temp. (°F)	
Traffic Data Direction Traffic Count: Cars MT HT	0 0 0 Humidity (%)	
Weather Conditions		
		Manifatina Mafa
		AM Peak:
	Japaes	
8		Off-Peak:
Profile View:	E	PM Peak
•		
McCormick Taylor, Inc		

McCormick Taylor, Inc	Profile View:	Contraction of the second seco		Site Data: Site Surface (alpha): Shielding Factor : Pavement Type :	Traffic Data Roadway Direction Image: Construction Traffic Count: 0 Cars 0 MT 0 HT 0 HT 0 Weather Conditions 0	Monitoring Data: AM Peak Off-Peak PM Peak Atmospheric Date Start Time 7/16/13 Data Data Data Start Time 10:10 AM 10:20 AM Mind Speed Mind Speed Duration MiN 10 MiN MiN 5 - 8 Leq. Temp. (°F) Temp. (°F) Temp. (°F)	# 5 By: JND/JCL	Site # R25 Description : 29 Garden St, Stroudsburg, PA 18360	I-80 Reconstruction Pro
	PM Peak	Off-Peak:	AM Peak:						ction Project

I-80 Reconstruction Project	ion Project
Site # R26 Description : 1197 W Main St, Stroudsburg, PA 18360	
# 1 By: JND/JCL	
Monitoring Data: AM Peak Off-Peak PM Peak Atmospheric Date 7/16/13 7/16/13 Data Data Start Time 10:10 AM Wind Speed Wind Speed Imph 10:20 AM (mph)	
MIN 10 MIN MIN	
Direction Humidity (%) Traffic Count: 0 0 0 0 60	
MT HT HT HT HT HT HT HT HT HT HT HT HT HT	
Site Data: Site Surface (alpha): Shielding Factor : Pavement Type :	Monitoring Notes
earde Sarde	AM Peak:
	Off-Peak:
	PM Peak
Profile View:	
McCormick Taylor, Inc	

APPENDIX C Noise Monitoring Data (2013) Metrosonics Printouts

Address	Start Time	Measurement Time	Leq	ĹĔ	LMAX	LMIN	Ly	LN1	LN2	LN3	LN4	LN5	Over	Under	Inverse Log
81	<u>I mice</u>		10.1101.000.000	t	Kalendar in der som	<u>Li di la di la di la di</u>						******			
1 1	7/16/2013	12:10:00 00d 00:10.0	66.6	76.6	68.5	65.3		68.4	68.3	66.3	65.4	65.3			4570881.9
{	· • • • • • • • • • • • • • • • • • • •				4								· •		3981071.7
2	7/16/2013	12:10:10 00d 00:10.0	66	76	68.3	63.9		68.1	68	66.3	64.1	64			3311311.2
3	7/16/2013	12:10:20 00d 00:10.0	65.2	75.2	66.3	63.7	·····	66.1	66	65.1	63.9	63,8			
4	7/16/2013	12:10:30 00d 00:10.0	6 5.3	75.3	66.2	64.1		66	66	65.6	64.3	64.2			3388441.6
5	7/16/2013	12:10:40 00d 00:10.0	65.3	75.3	66.6	63.6		66.3	66.1	65.2	63.9	63.8	•		3388441.6
6	7/16/2013	12:10:50 00d 00:10.0	63.7	73.7	67.1	61	•	66.9	66.6	63.2	61.1	61			2344228.8
7	7/16/2013	12:11:00 00d 00:10.0	61.7	71.7	62.5	60.8	÷.*	62.3	62.3	61.6	61	61	+		1479108.4
8	7/16/2013	12:11:10 00d 00:10.0	64.1	74.1	67.2	61	-7-	66.7	66.2	62.3	61.1	61.1			2570395.8
9	7/16/2013	12:11:20 00d 00:10.0	65.2	75.2	67.7	63		67.5	67.3	65.3	63.2	63.1			3311311.2
10	7/16/2013	12:11:30 00d 00:10.0	64,1	74.1	64.9	62.3		64.7	64.6	64.2	63.8	63.1			2570395.8
		******	60.1		62.4	58.7	·····	62.1	61.7	59.6	58.8	58.8	· · · · ·		1023293.0
11	7/16/2013			70.1					}	62.4	60.4	60.2			1659586.9
12	7/16/2013	12:11:50 0Dd 00:10.0	62.2	72.2	64.1	60.2		64	64		60.6	60.4			2238721.1
13	7/16/2013	12:12:00 00d 00:10.0	63.5	73.5	64.6	60.2	<u></u>	64.6	64.5	63.5		*			
14	7/16/2013	12:12:10 00d 00:10.0	70.2	80.2	74.3	63.4		74	73.4	68,6	63.5	63.5			10471285.5
15	7/16/2013	12:12:20 00d 00:10.0	61.2	71.2	70.2	60	~	68.7	67.2	60.8	60.2	60.1			1318256.7
16	7/16/2013	12:12:30 00d 00:10.0	63	73	64.2	61.2		63.8	63.7	62.7	61.5	61.3			1995262.3
17	7/16/2013	12:12:40 00d 00:10.0	67	77	68.6	64.2	·····	68.4	68.2	66.8	65.3	65.1			5011872.3
18	7/16/2013	12:12:50 00d 00:10.0	62.8	72.8	65.5	61.5	•••	64.9	64.5	62.5	61.7	61.6			1905460.7
19	7/16/2013	12:13:00 00d 00:10.0	65.4	75.4	66.3	63.9	-,-	66.1	66	6 5.7	64.4	64.2			3467368.5
20	7/16/2013	12:13:10 00d 00:10.0	66.1	76.1	68.1	63.3	-,-	67.9	67.8	65.5	63.5	63.4			4073802.8
21	7/16/2013	12:13:20 00d 00:10.0	62.2	72.2	66.4	60.5		66.1	65.4	61.7	60.7	60.6			1659586.9
22		12:13:30 00d 00:10.0	63.8	73.8	65.8	61.2		65.6	65.4	63.4	61.5	61.3			2398832.9
	7/16/2013			70.7	64	59.3	<u></u>	63.7	63.1	60.3	59.5	59.5			1174897.6
23 24	7/16/2013	12:13:40 00d 00:10.0	60.7	************			·····	61.9	61.9	61.3	60.2	60.1			1288249.6
	7/16/2013	12:13:50 00d 00:10.0	61.1	71.1	62.1	59.9		60.7	6D.4	60	59.8	59.8			1047128.5
25	7/16/2013	12:14:00 00d 00:10.0	60.2	70.2	61	59.7	×				61.3				4365158.3
26	7/16/2013	12:14:10 00d 00:10.0	66.4	76.4	68.2	61	······	68.1	67.9	66.8		61.2			
27	7/16/2013	12:14:20 00d 00:10.0	62.7	72.7	67.2	61.2		66.7	66.2	62.1	61.3	61.3			1862087.1
28	7/16/2013	12:14:30 00d 00:10.0	66.9	76.9	68.7	62.5		68.6	68.6	66.7	63.2	62.9			4897788.2
29	7/16/2013	12:14:40 00d 00:10.0	66	76	67.3	64.2		67.2	67	66.1	65.1	65			3981071.7
30	7/16/2013	12:14:50 00d 00:10.0	61.1	71.1	64.2	60.3		63.3	62.6	61.1	60.5	60.5			1288249.6
31	7/16/2013	12:15:00 00d 00:10.0	65.1	75.1	67.8	61.9		67.3	66.8	64.4	62.7	62.7			3235936.6
32	7/16/2013	12:15:10 00d 00:10.0	63.9	73.9	64.9	62.9	~~	64.7	64.5	63.7	63.3	63.2			2454708.9
33	7/16/2013	12:15:20 00d 00:10.0	66.8	76.8	69.3	62.5	-,-	69.1	68.9	66.2	62.7	62.6			4786300.9
34	7/16/2013	12:15:30 00d 00:10.0	65.4	75.4	68.8	64.4		68.3	67.5	65.7	64.8	64.8			3467368.5
1	7/16/2013	12:15:40 00d 00:10.0	64.5	74.5	65.6	63,6		65.5	65.4	64.4	63.9	63.8			2818382.9
35		12:15:50 00d 00:10.0	67.3	77.3	68.7	63.9		68.5	68.4	66.9	65.6	64.6			5370318.0
36	7/16/2013			73.5		62.5		66	65.8	63.3	62.7	62.6			2238721.1
37	7/16/2013	12:16:00 00d 00:10.0	63.5		66.2					63.9	62.5	62.4			2344228.8
38	7/16/2013	12:16:10 00d 00:10.0	63.7	73.7	64.4	62.4	····	64.4	64.2		63.4				7585775.8
39	7/16/2013	12:16:20 00d 00:10.0	68.8	78.8	72.3	63.3		71.9	71.6	67.1		63.4			4570881.9
40	7/16/2013	12:16:30 00d 00:10.0	66.6	76.6	70.8	64.1	<u></u>	70.4	69.9	66.3	64.4	64.2			
41	7/16/2013	12:16:40 00d 00:10.0	65,8	75.8	67.6	64.1	·····	67.3	67	64.9	64.4	64.2			3801894.0
42	7/16/2013	12:16:50 00d 00:10.0	65.2	75.2	67.6	63.4		67.5	67.3	64.9	63.5	63.5			3311311.2
43	7/16/2013	12:17:00 00d 00:10.0	66.9	76.9	68.5	64.9		68.3	68.1	66.8	65.2	65			4897788.2
44	7/16/2013	12:17:10 00d 00:10.0	63.1	73.1	65.1	51.8	·	65.1	64.8	63.2	61.9	61.8			2041737.5
45	7/16/2013	12:17:20 00d 00:10.0	64.3	74.3	65.4	63.4		65.2	65.1	64.1	63.5	63.5			2691534.4
46	7/16/2013	12:17:30 00d 00:10.0	63.2	73.2	64.2	62.8		63.9	63.6	63.4	62.9	62.9			2089296.
47	7/16/2013	12:17:40 00d 00:10.0	62.7	72.7	63.5	61.9		63.4	63.4	62.9	62.1	61.9			1862087.
47	7/16/2013		61.9	71.9	63.5	59.2		63.5	63.4	62.4	59.9	59.6			1548816.
			63.3	73.3	66.3	58.6		66.1	65.6	61.5	58.7	58.7			2137962.
49	7/16/2013		***********			61.6		66.5	66.5	63.5	61.8	61.7			2344228.
50	7/16/2013	12:18:10 00d 00:10.0	63.7	73.7	66.6						62.5	62.3			3548133.
51	7/16/2013	12:18:20 00d 00:10.0	65.5	75.5	66.7	62.1		66.6	66.4	65.5					2137962.
52	7/16/2013	12:18:30 00d 00:10.0	63.3	73.3	66.3	61.3	· · · · · ·	66.1	65.8	63.4	61.9	61.7			1000000.
53	7/16/2013	12:18:40 00d 00:10.0	60	70	61.3	59.2		60.9	60.7	59.9	59.3	59.3			
54	7/16/2013	12:18:50 00d 00:10.0	64.8	74.8	65.9	61.2		65.8	65.7	64.2	63.4	63.1			3019951.
55	7/16/2013	12:19:00 00d 00:10.0	66.6	76.6	67.3	64.9		67.2	67.2	66.6	65.4	65			4570881.
56	7/16/2013	12:19:10 00d 00:10.0	67.4	77.4	68.6	66.5	-,-	68.5	68.4	67.2	66.6	66.6			5495408.
57	7/16/2013	12:19:20 00d 00:10.0	66.4	76.4	68.5	62.7		68.4	68.4	67.2	63.2	62.9			4365158.
	7/16/2013	12:19:30 00d 00:10.0	61.1	71.1	62.7	59.9		62.5	62.3	61,3	60.4	60.2			1288249.
58			60.2	70.2	60.6	59.5		60.6	60.6	60.1	59.7	59.5			1047128.
59	7/16/2013	12:19:40 00d 00:10.0	1 00.2	10.4	1 00.0	57.7	· · · ·	59.5	59	58	57.8	57.8			660693.

Add	lress	Start Time	Measur	ement Time	Leq	LE	LMAX	LMIN	Ly	LN1	LN2	LN3	LN4	LN5	Over	Under	Inverse Log	Overall Leq
R	12		6				•	e	•	•			·····					60.2
: 1	1	7/16/2013	12:10:00	00d 00:10.0	61.9	71.9	64.5	55.3		64.3	63.5	61.3	56.8	56.4		***	1548817	00.Z
	2	7/16/2013	12:10:10	00d 00:10.0	60.9	70.9	64.7	58.6	-,-	54.4	64.2	61	58.9	58.9			1230269	
	····	7/16/2013	12:10:20	00d 00:10.0	61.5	71.5	63.5	58.6		63.3	63.1	60.8	58.8	58.7			1412538	
	3 4	7/16/2013	12:10:30	00d 00:10.0	62.4	72.4	63.6	61.1		63.4	63.1	62.1	61.4	61.2			1737801	
	*******	7/16/2013	12:10:40	00d 00:10.0	61.9	71.9	63.8	60.5		63.5	63.5	61.8	60.8	60,7			1548817	
	5 6	7/16/2013	12:10:50	00d 00:10.0	59.8		61.3	57.7		61.2	61.1	60.2	58.2	57.9		+	954992.6	
	7	7/16/2013	12:11:00	00d 00:10.0	58.5	69.8 68.5	60	57.3	·	59.5	59.4	57.7	57.4	57.4			707945.8	
											62.7	61.6	60.7	60.4			1621810	
	8	7/16/2013	12:11:10		62,1	72.1	63.2	60 F0 F		62,8		61		59.6			1288250	
	9	7/16/2013	12:11:20		61.1	71.1	63.3	59.5		63.1	62.8		59.7	57.4			676083	
	0	7/16/2013	12:11:30	00d 00:10.0	58.3	68.3	59.5	57.3		59.2	59.2	58.5	57.5				2041738	
	1	7/16/2013	12:11:40		63,1	73.1	66.1	58.4	·····	66	65.9	62	59.1	58.6				
	2	7/16/2013	12:11:50		59.7	69.7	61.1	58.9		60.9	60.9	59.4	59	58.9			933254.3	
	3	7/16/2013	12:12:00		60.9	70.9	62.2	59		62	61.9	61.1	60.5	60			1230269	
	4	7/16/2013	12:12:10		56.2	66.2	59	55		58.3	57.8	55.7	55.1	55.1			416869.4	
1	5	7/16/2013	12:12:20		59.3	69.3	63.3	55.2		62.4	62	58.6	55.7	55.4			851138	Į
	6	7/16/2013	12:12:30		61.6	71.6	65	56.8		64.7	64.1	60.9	56.9	56.8			1445440	
1	7	7/16/2013	12:12:40	00d 00:10.0	59	69	59.8	58.2		59.7	59.6	59	58.3	58.3			794328.2	
1	18	7/16/2013	12:12:50		64.8	74.8	69.6	58.1		67.9	66.9	62.4	58.3	58.2			3019952	Men
1	19	7/16/2013	12:13:00	00d 00:10.0	64.1	74.1	69.5	61.1		69	68.8	62.8	61.2	61.2			2570396	Workin
2	20	7/16/2013	12:13:10	00d 00:10,0	61.5	71.5	64.6	60.1		63.7	62.6	61.1	60.7	60.7			1412538	Nearby U
2	21	7/16/2013	12:13:20	00d 00:10.0	62.4	72.4	65	60.7		64.6	63.3	61.6	60.9	60.8		*****	1737801	Saw.
· · · · · · · · · · · · · · · · · · ·	22	7/16/2013	12:13:30	00d 00:10.0	64.3	74.3	65.8	52.9	•,•	65.6	65.3	64.1	63.3	63.2			2691535	J 30 44.
	23	7/16/2013	12:13:40	00d 00:10.0	59.1	69.1	64	58.3		62.7	61.5	59,3	58.4	58.4		••	812830.5	
	24	7/16/2013	12:13:50	00d 00:10,0	60.8	70.8	62.2	59.1	-,-	61.6	61.5	60.2	59.4	59.3			1202264	
	25	7/15/2013	12:14:00		61.7	71.7	63	59.5		62.9	62.8	62.3	60.3	59.9			1479108	
	26	7/16/2013	12:14:10		57.8	67.8	59.5	56.8		59.1	59	57.7	56.9	56.9			602559.6	
	27	7/16/2013	12:14:20		58.4	68.4	59.5	57.4		59,4	59.4	58.5	57.6	57.5			691831	
	28	7/16/2013	12:14:30		56.1	66.1	57.5	55.4		57.1	57	56.4	55.5	55.4			407380.3	
	29	7/16/2013	12:14:40		55.9	65.9	56.2	55.4		56.1	56.1	55.8	55,4	55.4		-+	389045.1	
		7/16/2013	12:14:50		61.2	71.2	63.1	56		63	62.9	60.2	56.7	56.2			1318257	
	10	7/16/2013	12:15:00			71.1	62.7	57.7		62.5	62.5	61.9	58.3	58			1288250	1
	31	~~~~~		* ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~	61.1			57	·····	62.2	62.2	58.1	57.4	57.2			1023293	1
	32	7/16/2013	12:15:10		60.1	70.1	62.3				62.4			61.8			1621810	
	33	7/16/2013	12:15:20		62.1	72.1	62.6	61.7	·····	62.6	***********	62.1 60.4	61.9 60				1122018	
	34	7/16/2013	12:15:30		60.5	70.5	62	59.9		61.7	61.4			59.9	·			
	35	7/16/2013	12:15:40		61.1	71.1	61.7	60.5		61.5	61.5	61.1	60.7	60.6			1288250 407380.3	
	36	7/16/2013	12:15:50		56.1	66.1	60.9	53.7		60.2	59.6	56.2	53.9	53.8				
	37	7/16/2013	12:16:00		58.6	68.6	61.2	54.2		61.1	60.4	57.8	54.7	54.5			724436	
	38	7/15/2013	12:16:10		62.5	72.5	63.9	61.2	<u> </u>	63.6	63.2	62.4	61.5	61.5			1778279	
1	39	7/16/2013	12:16:20	************************	63.2	73.2	65.6	60.7		65.5	65.2	62.8	60.9	60.8			2089296	
	40	7/16/2013	12:16:30		63.5	73.5	64.9	62.4	·····	64.8	64.6	63.Z	62.6	52.5		*****	2238721	Men
4	41	7/16/2013	12:16:40	00d 00:10.0	60.1	70.1	62,7	58.3		62.4	62.1	60.1	58.9	58.6			1023293	Workin
4	42	7/16/2013	12:16:50		4	67.6	58.6	56.6		58.5	58.3	57.4	56,8	56.7			575439.9	Nearby U
4	43	7/16/2013	12:17:00	00d 00:10.0	63.5	73.5	66.7	58.6		66.6	66.4	63	59.2	58.7			2238721	Saw.
4	44	7/16/2013	12:17:10	00d 00:10.0	64	74	66.2	61.8	ļ	66	65.8	63.9	62.4	62.2			2511886	
4	45	7/16/2013	12:17:20	00d 00:10.0	60.2	70.2	61.8	59	-,-	61.4	61.2	60.1	59.2	59.2			1047129	
4	46	7/16/2013	12:17:30	00d 00:10.0	64.7	74.7	67.9	61.1	•.•	67.8	67.4	63.1	62.5	62			2951209	
	47	7/15/2013	12:17:40	00d 00:10.0	61.6	71.6	64.2	60.3		63.2	62.8	61.8	60.5	60.4			1445440	
	48	7/16/2013	12:17:50	*******************	58.9	68.9	62.3	55.7	[62.1	61.8	59.1	55.9	55.8			776247.1	
	49	7/16/2013	12:18:00		59.7	69.7	62.1	55.9	-,-	61.9	61.7	58.4	56.2	56			933254.3	
	50	7/16/2013	12:18:10		61.1	71.1	62.2	59.7	-,-	62	62	61.3	60.3	60			1288250	i
	51	7/16/2013	12:18:20			66.9	59.7	54.4	-,-	59.3	59.1	57.5	54.6	54.5			489778.8	
	52	7/16/2013	12:18:30		54.9	64.9	56,4	53.3		56.2	55.9	54,4	53.6	53.5			309029.5	1
P	53	7/16/2013	12:18:40		+	68.3	59.7	56.4		59.4	59.3	57.7	56.7	56.7			676083	
		7/16/2013	12:18:50			69.4	61.2	57.6		61.1	61	59.8	57.7	57.7			870963.6	
	54		*************		4					60.2	60.1	58.8	57.7	57.6			812830.5	
	55	7/16/2013	12:19:00		************	69.1 70.4	60.2 61.7	57.4 58.8		61.5	61.5	60.5	59.2	59.1			1096478	
	56	7/16/2013	12:19:10	**********************************						59.1	58.9	58.2	57.5	57.3			630957.3	
	57	7/16/2013	12:19:20			68	59.3	57.2	.			58.2	57.2				933254.3	
	58	7/16/2013	12:19:30		+	69.7	61.3	56.9		61.2	61.2			57				
	59	7/16/2013	12:19:40			72.7	63.6	61		63.5	63.4	62.4	61.3	61	-+		1862087	1
	60	7/16/2013	12:19:50	00d 00:10.0	61.6	71.6	63.1	61	<u></u>	62.7	62.4	61.6	61.2	61.1			1445440	4

Address	Start Time	Measurement Time	Leq	LE	LMAX	LMIN	Ly	LN1	LN2	LN3	LN4	LN5	Over	Under	Inverse Log	Overall Leq
R3				L.,			منتخب تشمينا م	C		1		Las submitte	1	1	s.,	
1	7/16/2013	12:10:00 00d 00:10.0	63.2	73.2	65.2	62		64.6	63.9	63.4	62.2	62.1			2089296	60.9
2	7/16/2013	12:10:10 00d 00:10.0	62.2	72.2	63.7	60.9		63.6	63.5	62.6	61.1	61			1659587	
3	7/16/2013	12:10:20 00d 00:10.0	60.2	70.2	62.4	57.5	·····	62.4	62.3	59.5	57.7	57.6			1047129	
4	7/16/2013	12:10:30 00d 00:10.0	60.2	70.2	62.6	58.5		62.5	62.4	59.8	58.8	58.6			1047129	
*************	7/16/2013	12:10:40 00d 00:10.0		73	63.7	60.9		63,7	63.6	63.1	61.6	61.2	.		1995262	
5 6	7/16/2013	12:10:50 00d 00:10.0	63 64	74	67.3	61		67.2	67.1	61.9	61.3	61,1			2511886	
	7/16/2013	12:11:00 00d 00:10.0	63.2	73.2	67.1	62		66.9	66.4	62.6	62.3	62.1			2089296	
	7/16/2013	12:11:10 00d 00:10.0		72.7			·	63.6	63.5	62.3	62	61.9	+		1862087	
8	7/16/2013	12:11:10 00d 00:10.0	62.7 59.5	69.5	63.8	61.9		*************	61.4	59.7	58.6			{	891250.9	
		12:11:20 00d 00:10.0		*********	62.7	58.4		62.1	*	57.9	57.7	58,5 57,7	+		630957.3	
10	7/16/2013 7/16/2013	12:11:40 00d 00:10.0	58 57.7	68	60 58.5	57.6	·····	59.9 58.4	59.6		57.4	57.1			588843.7	
11	7/16/2013	******		67.7	+	57	·····	*******	58.2	57.6		+			1096478	
12 13	7/16/2013	12:11:50 00d 00:10.0 12:12:00 00d 00:10.0	60.4 60.5	70.4 70.5	62.2	56.9 58.2		62.1 62	61.9 62	60	58.2	57.3			1122018	
					62.2		·····		***********	59.6	58,7	58.5 57		·····		
14	7/16/2013	12:12:10 00d 00:10.0	58.2	68.2	61.6	56.9		61.5	61.1	57.7	57.1	57			660693.4	
15	7/16/2013	12:12:20 00d 00:10.0	60	70	60.8	56.8		60.8	60.6	60.1	57.1				1000000	
16	7/16/2013	12:12:30 00d 00:10.0	62	72	64.7	60.2		64.2	63	61.6	60.4	60.4			1584893	
17	7/16/2013	12:12:40 00d 00:10.0	65.2	75.2	68.2	61.4		67,7	67.6	63	61.9	61.6			3311311	
18	7/16/2013	12:12:50 00d 00:10.0	61.5	71.5	66.8	60.6		65.8	64.9	61.6	60.8	60.7			1412538	
19	7/16/2013	12:13:00 00d 00:10.0	59.7	69.7	61.8	56.8		61.5	61.4	60.4	57	56.9			933254.3	
20	7/16/2013	12:13:10 00d 00:10.0	60.9	70.9	64	56.4		63.8	63.6	58	56.6	56.5	+	·	1230269	
21	7/16/2013	12:13:20 00d 00:10.0	59,4	69,4	63.8	57.8	i:	63.2	62.9	58.9	57.9	57.9		·	870963.6	
22	7/16/2013	12:13:30 00d 00:10.0	57.7	67.7	59.2	55.4	·	59.1	59	58.4	55.6	55.5			588843.7	
23	7/16/2013	12:13:40 00d 00:10.0	59.3	69.3	62.2	55.7		61.5	60.8	58.1	56.5	56.2		·	851138	
24	7/16/2013	12:13:50 00d 00:10.0	61.2	71.2	63.6	57.9	· · · · · · · · · · · · · · · · · · ·	63.4	63.3	61.4	58.6	58.2			1318257	
25	7/16/2013	12:14:00 00d 00:10.0	57.3	67.3	58.8	56	· · · · · · · · · · · · · · · · · · ·	58.8	58.7	56.9	56.1	56.1	·		537031.8	ł
26	7/16/2013	12:14:10 00d 00:10.0	57.1	67.1	58.8	56.3		58.8	58.7	56.9	56.5	56.4			512861.4	ł
27	7/16/2013	12:14:20 00d 00:10.0	56.4	66.4	57.1	55.7		57	56.9	56.5	55.9	55.8			436515.8	
28	7/16/2013	12:14:30 00d 00:10.0	59.3	69.3	62.6	56.1		61.9	61.7	57.3	56.2	56.2	ļ	ļ	851138	
29	7/16/2013	12:14:40 00d 00:10.0	62.8	72.8	64.5	60.8		64.2	63.9	62.7	61.7	61.2	~~~		1905461	Į
30	7/16/2013	12:14:50 00d 00:10.0	60	70	62.4	57.4	·····	62.3	62.2	59.7	57.8	57.7			1000000	
31	7/16/2013	12:15:00 00d 00:10.0	62.3	72.3	64.9	56.9		64.8	64.6	59.9	57.1	57			1698244	
32	7/16/2013	12:15:10 00d 00:10.0	62.6	72.6	64.9	61.5		64.5	64	62.8	61.8	61.7			1819701	
33	7/16/2013	12:15:20 00d 00:10.0	56.8	66.8	62.4	55.5	ļ	61.6	60.7	56.7	55.7	55.6			478630.1	
34	7/16/2013	12:15:30 00d 00:10.0	63.2	73.2	66.7	55.8		66,6	66.3	62.3	57.1	56.4			2089296	
35	7/16/2013	12:15:40 00d 00:10.0	56.1	66.1	59.9	54.1		59.7	59.4	55.5	54.3	54.2	****		407380.3	
36	7/16/2013	12:15:50 00d 00:10.0	60.2	70.2	63.4	56.3		62.7	61.9	58.9	57	56.6	ļ		1047129	
37	7/16/2013	12:16:00 00d 00:10.0	63.8	73.8	65.5	63		65.2	64.7	63.4	63.2	63.1			2398833	
38	7/16/2013	12:16:10 00d 00:10.0	61.9	71.9	63.3	61.2	····	63	62.7	62	61.6	61.3			1548817	1
39	7/16/2013	12:16:20 00d 00:10.0	65.1	75.1	68.8	60.9	<u></u>	68.7	68.3	63.9	61.5	61.2			3235937	
40	7/16/2013	12:16:30 00d 00:10.0	59.7	69.7	61.3	58.1		61.1	61	59.4	58.5	58.3			933254.3	Garage D
41	7/16/2013	12:16:40 00d 00:10.0	60	70	61.4	58.6		61.2	61.2	59.3	58.7	58.6	·		1000000	and Ca
42	7/16/2013	12:16:50 00d 00:10.0	64.1	74.1	68.3	59.8	·	67.4	67.1	60.7	60	59.9			2570396	leavin
43	7/16/2013	12:17:00 00d 00:10.0	64.6	74.6	68.5	51.6		68.1	67.9	64.5	61.7	61.7			2884032	Garag
44	7/16/2013	12:17:10 00d 00:10.0	59.9	69.9	61.7	58.4		61.3	61	59.9	58.6	58.5			977237.2	
45	7/16/2013	12:17:20 00d 00:10.0	63.1	73.1	65.6	58.8		65.5	65.4	62.9	59.9	59.2			2041738	ł
46	7/16/2013	12:17:30 00d 00:10.0	65.4	75.4	69.4	58.6		69.3	69	63	58.8	58.7			3467369	ł
47	7/16/2013	12:17:40 00d 00:10.0	60.6	70.6	68.1	59.2		67	65.9	60	59.3	59.3			1148154	
48	7/16/2013	12:17:50 00d 00:10.0	59,6	69.6	61.6	56.8	<u> </u>	61.4	61.4	58.7	57.3	57.1			912010.8	
49	7/16/2013	12:18:00 00d 00:10.0	60.5	70.5	62.1	59,5		61.9	61.7	60.7	59.9	59.8			1122018	
50	7/16/2013	12:18:10 00d 00:10.0	57.4	67.4	59.5	55.3		59.4	59.2	57.2	56	55.6			549540.9	
51	7/16/2013	12:18:20 00d 00:10.0	55.6	65.6	56.3	55		56.1	55.8	55.6	55.1	55.1			363078.1	
52	7/16/2013	12:18:30 00d 00:10.0	59.7	69.7	62	56.2		61.9	61.9	58.6	57.1	56.6			933254.3	
53	7/16/2013	12:18:40 00d 00:10.0	60.8	70.8	62.3	60.1		62.2	62.1	60.8	60.2	60.1			1202264	
54	7/16/2013	12:18:50 00d 00:10.0	61.3	71.3	63.2	59.6	[62.6	62.1	60.4	59.7	5 9 .7			1348963	
55	7/16/2013	12:19:00 00d 00:10.0	63	73	63.8	62.3		63.7	63.6	63	62.6	62.6			1995262	
56	7/16/2013	12:19:10 00d 00:10.0	61.3	71.3	62.3	60.8	<u> </u>	62	61.9	61.3	60.9	60.9			1348963	
57	7/16/2013	12:19:20 00d 00:10.0	60.2	70.2	61.1	58.9		61	60.9	60.2	59.1	59			1047129	
58	7/16/2013	12:19:30 00d 00:10.0	62.6	72.6	64.3	60		64.2	64.1	62.7	60.7	60.3			1819701	
59	7/16/2013	12:19:40 00d 00:10.0	59.7	69.7	60.9	58.1	-,-	60.6	60.4	59.6	58.2	58.2			933254.3	1
+	7/16/2013	12:19:50 00d 00:10.0	62.2	72.2	63.5	59.6	-,-	63.4	63.4	62.4	60.4	59.9			1659587	1

Address	Start Time	Measurement	t Time	Leq	LE	LMAX	LMIN	Ly	LN1	LN2	LN3	LN4	LN5	Over	Under	Log
84	demanus menteres interes	********														
1 1	7/16/2013	11:20:00 00d	00:10.0	64.9	74.9	69.3	61.4	•.•	69	68.5	63.3	61.5	61.5			3090295
2	7/16/2013		00:10.0	62.8	72.8	64.5	59.6		54.3	64	63	59.9	59.7	****		1905461
***********	7/16/2013		00:10.0	50.7	70.7	62.9	59.5	·····	62.4	61.8	61	60.1	60			1174898
3	7/16/2013		00:10.0	60	70	64.7	56	·····	64	60.9	58.4	56.3	56.1			1000000
5	7/16/2013	*******************************	00:10.0	67.8	77.8	69.7	63.8		69.6	69.4	67.8	64	63.9		*	6025596
******				******			65.9	·	71.1	70.6	68.9	66.3	66			7413102
6	7/16/2013	*******************************	00:10.0	68.7	78.7	71.3			67.2	57.1	65.7	62.9	62.8			3235937
7	7/16/2013		00:10.0	65.1	75.1	68	62.6	·····	66.8	56.4	63.4	52.4	62.4			2630268
8	7/16/2013		00:10.0	64.2	74.2	66.9	62.3	·	64.9	64.2	61.2	59.5	59.3			1621810
9	7/16/2013	#*************************************	00:10.0	62.1	72.1	65	59.2	·····				***********	60.3			2041738
10	7/16/2013		00:10.0	63.1	73.1	65.3	60.1		64.9	64.8	63.2	60.5	*****			5128614
11	7/16/2013		00:10.0	67.1	77.1	68.5	64.3		68.4	68.3	67.3	65.6	65			1862087
12	7/16/2013		00:10.0	62.7	72.7	64.3	61.2		54.1	63.9	63	61.5	61.3		*******	
13	7/16/2013		00:10.0	63.4	73.4	64.8	62.4	·····	64.7	64.6	63.1	62.6	62.6			2187762
14	7/16/2013		00:10.0	66.5	76.5	59.1	61.4	<u>.</u>	69	68.8	65.9	61.6	61.5			4466836
15	7/16/2013		00:10.0	67.8	77.8	69.1	65.6	•.•	59	68.9	67.4	66.3	66.2			6025596
16	7/16/2013	***************************************	00:10.0	64.5	74.5	68	61	<u>.</u>	67.5	67.3	65	61.5	61.2		*****	2818383
17	7/16/2013		00:10.0	67.8	77.8	71.3	60.9	·····	71.1	70.6	66.8	51.3	61			6025596
18	7/16/2013	11.22:50 00d	00:10.0	64.3	74.3	68.8	60.5		68.7	68.5	63.7	60.9	60.6			2691535
19	7/16/2013	11:23:00 00d	00:10.0	66.1	76.1	70.1	60.1		69.9	69.3	64.5	60.3	60.2			4073803
20	7/16/2013	11:23:10 00d	00:10.0	64.9	74.9	68	62.1		67.6	65.9	64.4	62.2	62.2			3090295
21	7/16/2013	11:23:20 00d	00:10.0	66.6	76.6	69.1	63.4	-7	68.9	68.6	66.8	63.9	63.7			4570882
22	7/16/2013	11:23:30 00d	00:10.0	62.3	72.3	65.9	59.9		65.6	65.3	62.6	60.3	50.1		L	1698244
23	7/16/2013	11:23:40 00d	00:10.0	62.1	72.1	63.6	58.6	···	63.3	62.8	62.5	59	58.7			1621810
24	7/16/2013	11:23:50 00d	00:10.0	67.7	77.7	70.4	63.6	- <u>-</u>	70.2	70	67.1	65.5	64.5			5888437
25	7/16/2013	11 24:00 00d	00:10.0	65.1	75.1	66.7	62.3		66.6	66.6	65.4	62.5	62.4			3235937
26	7/16/2013	11.24:10 00d	00:10.0	57.6	77.6	71.2	62.5	-,-	71	70.7	66,4	64.3	63.1			5754399
27	7/16/2013	11:24:20 00d	00:10.0	62	72	64.6	60.6	-,-	64.6	54.3	62.5	60.7	60.7			1584893
28	7/16/2013	11:24:30 00d	00:10.0	64	74	65	60.5		65.9	65.6	63.4	60.8	60.6			2511886
29	7/16/2013	11:24:40 00d	00:10.0	68	78	70.5	65.4		70.3	70	66.5	65.8	65.6			6309573
30	7/16/2013		00:10.0	69.3	79.3	71	67.5	-,-	70.9	70.7	69	67.8	67.6			8511380
31	7/16/2013	**********************	00:10.0	63.7	73.7	69.3	60.9	•.•	68.6	68	63.2	61.5	61			2344229
32	7/16/2013		00:10.0	61.8	71.8	66.8	57.6	··-	65.3	63.8	59.5	57.9	57.7			1513561
33	7/16/2013		00:10.0	65.5	75.5	69	60.2	-,-	68.9	68.7	65.6	61.2	60.8			3548134
34	7/16/2013		00:10.0	57.7	67.7	50.3	55.1	•,•	59.7	59.7	57.8	55.5	55.2			588843.7
35	7/16/2013		00:10.0	63.3	73.3	65.3	57.3		65.1	64.6	62.7	51.5	58.2			2137962
36	7/16/2013		00:10.0	65.1	75.1	68.4	51.8		68.1	67.8	64.5	62.1	61.9			3235937
37			00:10.0	67	77	70.1	63.3	·····	69.8	69.6	66.6	64.4	63.8			5011872
	7/16/2013		00:10.0	62.7	72.7	63.6	61.1	·····	63.5	63.5	63.1	61,3	61.3			1862087
38				61.9	***********	63.9	59.5		63.8	63.5	61.8	60.3	59.8			1548817
39	7/16/2013		00:10.0		71.9 69.2	61	57.2		60.3	60	59	57.5	57.3			831763.8
40	7/16/2013		00:10.0	59.2	+	+			64.5	64.3	63.4	61.4	61.2			2137962
41	7/16/2013		00:10.0	63.3	73.3	64.5	61 50.4		*		66.6	59.7	59.5			4073803
42	7/16/2013	*********************	00:10.0	66.1	76.1	68.3	59.4		68.2	68 64.8	59.6	58.8	58.5			1096478
43	7/16/2013		00:10.0	60.4	70.4	66.5	58.3		65.7		63.5		59.5			5248075
44	7/16/2013		00:10.0	67.2	77.2	71.1	59.4		70.9	70.7	64.9	59.6 64.1				3090295
45	7/16/2013	*************************	00:10.0	64.9	74.9	67.7	63.3		67.2	66.8		64.1	63.8			1995262
46	7/16/2013	~	00:10.0	63	73	64.2	61.7		64.1	63.9	62.9	62	61.8			1995262
47	7/16/2013		00:10.0	63	73	64.7	61		64.6	64.4	62.7	61.2	61.1			2187762
48	7/16/2013		00:10.0	63,4	73.4	66.1	60.4	ļ	66	65.8	62.7	60.6	60.4			**************
49	7/16/2013		00:10.0	62	72	65.7	60.3		65.3	64.9	61.2	60.4	60.4			1584893
50	7/15/2013	*	00:10.0	65.7	75.7	68.3	50.4		67.8	67.2	65.5	61	60.9	****		3715352
51	7/16/2013	11:28:20 000	00:10.0	64.9	74.9	68.9	60.9		68.8	68.5	64,5	61.2	61			3090295
52	7/16/2013	11:28:30 000	00:10.0	64.1	74.1	66.2	61.4		66.1	66	65.1	61.8	61.6			2570396
53	7/16/2013	11:28:40 000	00:10.0	65.8	75.8	69.4	60.5	·	67.5	67.4	64.5	60.8	60,7			3801894
54	7/16/2013	11:28:50 000	00:10.0	64.8	74.8	69.6	62.4	<u>````</u>	69.1	68	64.9	62.9	62.8			3019952
55	7/16/2013	11.29:00 000	I 00:10.0	61.8	71.8	67	59.4		65.7	64.5	61.1	59.7	59.5			1513561
56	7/15/2013		00:10.0	67.6	77.6	70	61.5		70	69.9	67.1	62.3	61.9			5754399
57	7/16/2013		00:10.0	66.7	76.7	68.4	64.4		68.3	68.2	66.4	64.8	64.5			4677351
58	7/16/2013		00:10.0	69.7	79.7	71.2	65.4		71.1	70.9	69.6	67.7	66.8			9332543
59	7/16/2013		00:10.0	64.8	74.8	68	62.3		67.7	67.6	64.9	62.8	62.4			3019952
60	7/16/2013		00:10.0	63	73	65.2	61.8		65.1	64.8	63.1	61.9	61.9		· · · · ·	1995262

Address	Start Time	Measurement Time	Leq	LE	LMAX	LMIN	Ly	LN1	LN2	LN3	LN4	LN5	Over	Under	Inverse Log	Ove Le
R5												·		······		55
1	7/16/2013	11:20:00 00d 00:10.0	53.1	63.1	53.9	52	-,-	53.7	53.7	53.1	52.2	52.1			204173.8	
2	7/16/2013	11:20:10 00d 00:10.0	54,1	64.1	54.8	52.9		54.7	54.7	54.1	53.2	53			257039.6	
3	7/16/2013	11:20:20 00d 00:10.0	53.7	63.7	54.6	52.4		S4.6	54.5	53.7	52.5	52.5			234422.9	
4	7/16/2013	11:20:30 00d 00:10.0	54.2	64.2	55	53.1		54.9	54.8	54.4	53.7	53.4			263026.8	
5	7/16/2013	11:20:40 00d 00:10.0	51.8	61.8	53.1	51	-,-	52.9	\$2.8	51.7	51	51			151356.1	
	7/16/2013	11:20:50 00d 00:10.0	54.1	64.1	55.6	51.5	-,-	55.4	54.9	54	51.8	51.6			257039.6	
6	7/16/2013	11:21:00 00d 00:10.0	56.8	66.8	58.1	54.7	-,-	57.9	57.8	56.5	55.6	55.1			478630.1	
8	7/16/2013	11:21:10 00d 00:10.0	\$7.8	67.8	59.4	56.6		S8.3	58	57.5	56.8	56.7			602559.6	
	7/16/2013	11:21:20 00d 00:10.0	57.9	67.9	60	\$6.3		59.9	59.6	57.6	57	56.6			616595	
9	7/16/2013	11:21:30 00d 00:10.0	54.8	64.8	56.3	54.3		56,2	56	54.7	54.5	54.4			301995.2	
10	7/16/2013	11:21:40 00d 00:10.0	58.7	68.7	61.5	54.1		61.2	61	56.5	54.4	54.2			741310.2	
11	4		56.7	66.7	60.6	56.2		60	59.2	56.8	56.4	56.3			467735.1	
12	7/16/2013	11:21:50 00d 00:10.0		66.4	57.5	55.2		57.3	57	56.5	55.7	55.5			436515.8	
13	7/16/2013	11:22:00 00d 00:10.0	56.4	+	h		· · · · · ·	57.4	56.9	55.5	54.6	54.6			363078.1	
14	7/16/2013	11:22:10 00d 00:10.0	*	65.6	57.6	54.6		57.6	57.4	55.5	54.9	54,9			416869.4	
15	7/16/2013	11:22:20 00d 00:10.0	56.2	66.2	57.7	54.8		**************				56.9			588843.7	
16	7/16/2013	11:22:30 00d 00:10.0	57.7	67.7	58.7	56.8	·····	58.6	58.5	57.S 57.3	57	55.9			512861.4	
17	7/16/2013	11:22:40 00d 00:10.0		67.1	58	55.6		57.9	57.8	55.2	56.1 54.5	54.5			389045.1	
18	7/16/2013	11:22:50 00d 00:10.0	55.9	65.9	57.5	54.4	·····	57.4	57.1			56.3			524807.5	
19	7/16/2013	11:23:00 00d 00:10.0	57.2	67.2	58.4	56.2		58.1	58	57.1	56.3	55.2			363078.1	i i
20	7/16/2013	11:23:10 00d 00:10.0	\$5.6	65.6	57.7	55.1		57.3	56.8	55.7	55.2	************			446683.6	
21	7/16/2013	11:23:20 00d 00:10.0		66.5	58.2	55.1	<u>.</u>	57.9	57.9	56	55.3	55.2			301995.2	
22	7/16/2013	11:23:30 00d 00:10.0	+	64.8	56.4	53,9		56	55.5	54.5	54.1	54			380189.4	
23	7/16/2013	11:23:40 00d 00:10.0	· · · · · · · · · · · · · · · · · · ·	65.8	56.4	55.4		56.3	56.2	55,7	55.5	55.5			316227.8	
24	7/16/2013	11:23:50 00d 00:10.0		65	57.2	52.3		56.6	56.4	54.5	52.6	52.4				
25	7/16/2013	11:24:00 00d 00:10.0		67.9	59.3	56.3		59.1	59	58.1	56.7	56.4			616595	
26	7/16/2013	11:24:10 00d 00:10.0	57.2	67.2	58.1	55.8	- <u>-</u> -	58	58	\$7.3	56.4	56.2			524807.5	
27	7/16/2013	11:24:20 00d 00:10.0	55.7	65.7	56.8	55.2		56.7	56.4	\$5.6	55.3	55.3			371535.2	
28	7/16/2013	11:24:30 00d 00:10.0	55.4	65.4	57.7	53.6		57.6	57.5	54.8	53.7	53.7			346736.9	
29	7/16/2013	11:24:40 00d 00:10.0	55.7	65.7	56.8	53.6		56,7	56.3	55.4	S4.2	53.8			371535.2	
30	7/16/2013	11:24:50 00d 00:10.0	55.8	65.8	57.4	54.7	· · · · · ·	57.3	57.2	56	54.8	54.8			380189.4	
31	7/16/2013	11:25:00 00d 00:10.0	59.6	69.6	62.7	54.8	<u>.</u>	62.5	62.3	57.6	55.7	55.6			912010.8	
32	7/16/2013	11:25:10 00d 00:10.0	57.5	67.5	59.7	55.3		59.2	58.9	57.8	56.4	55.8			562341.3	
33	7/16/2013	11:25:20 00d 00:10.0	53.1	63.1	55.3	51.5		54.8	54.7	52.7	51.7	51.6			204173.8	
34	7/16/2013	11:25:30 00d 00:10.0		66.3	57.1	54.8		57.1		56.2	55	54.9			426579.5	ł
35	7/16/2013	11:25:40 00d 00:10.0	53	63	57.1	50.1		56.9	56.4	53	50.4	50.4			199526.2	
36	7/16/2013	11:25:50 00d 00:10.0		62	53	49.7		52.9	52.9	52.3	49.8	49.8			158489.3	
37	7/16/2013	11:26:00 00d 00:10.0		65.3	\$6.8	52.4		56.7	56.1	55.1	53.1	\$2.9			338844.2	
38	7/16/2013	11:26:10 00d 00:10.0	56.6	66.6	57.1	56.1		57	57	\$6.6	56.2	56.2			457088.2	
39	7/16/2013	11:26:20 00d 00:10.0	55.5	65.5	57.7	53.8		57.S	57.4	55.2	53.9	53.9			354813.4	
40	7/16/2013	11:26:30 00d 00:10.0	56.5	66.5	62.4	52.8		61.5	60.2	54.3	52.9	S2.9			446683.6	
41	7/16/2013	11:26:40 00d 00:10.0	52.8	62.8	56.6	52.1		55.9	55.3	52.7	52.4	52.2			190546.1	
42	7/16/2013	11:26:50 00d 00:10.0	53.8	63.8	54.7	52.1		54.6	54.6	53.7	52.5	52.2			239883.3	
43	7/16/2013	11:27:00 00d 00:10.0	53.9	63.9	55.4	52.5		55.3	55.3	53.4	52.7	52.6			245470.9	
44	7/16/2013	11:27:10 00d 00:10.	54.8	64.8	55.5	53.4		55.5	55.5	55.2	\$4.1	53.7			301995.2	
45	7/16/2013	11:27:20 00d 00:10.	53.1	63.1	54	52		53.7	53.6	53.2	52.3	52.2			204173.8	
46	7/16/2013	11:27:30 00d 00:10.	56.3	66.3	57.5	54		57.4	S7.3	55.8	55.4	55.4			426579.5	
47	7/16/2013	11:27:40 00d 00:10.	55	65	55.5	54.6		55.4	55.3	55	54.7	54.6			316227.8	
48	7/16/2013	11:27:50 00d 00:10.		65	\$5.9	54.4		55.8	55.7	54.9	54.6	54.5			316227.8	
49	7/16/2013	11:28:00 00d 00:10.		62.7	54.4	52.1		54.2	53.8	52,8	52.4	52.2			186208.7	
50	7/16/2013	11:28:10 00d 00:10.		62.9	54.3	51.8	•	54	53.8	52.3	52	51.9			194984.5	
51	7/16/2013	11:28:20 00d 00:10.		63.7	54.5	53.1		54.4	54.4	53.6	53.4	53.3			234422.9	2
52	7/16/2013			65.4	56.3	53.4	-,-	56.2	56.1	\$5.4	53.6	53.5			346736.9	
53	7/16/2013	11:28:40 00d 00:10.		67.6	59.2	55.7	-,-	59	58.9	57.6	56	55.9			575439.9	2
	7/16/2013	11:28:50 00d 00:10.		64	55.7	53.2		55.4	55	54	S3.3	53.3			251188.6	
54	7/16/2013	11:29:00 00d 00:10.		65	56.7	53.2			55.5	55.1	54.3	53.7			316227.8	
55 \$6	7/16/2013	11:29:10 00d 00:10.		62	53.2	50.8		53.1	53	52.1	51.1	51			158489.3	1
	7/16/2013	11:29:20 00d 00:10.		64	56.1	50.9		55.8	55.7	52.4	51.3	51.2			251188.6	5
57	7/16/2013			67.4	58.4	56.1		58.3	58.3	\$7.3	56.4	56.3			549540.9	2
58				69.7	61.2	57		61	60.6	59.2	57.7	57.5			933254.5	
59	7/16/2013	1 11.23.40 000 00.10.	~1 33.1						60.8	59.5	54.7	54.5			724436	1

Addr	ess Start Time	Measurement Time	Leq	LE	LMAX	LMIN	Ly	LN1	LN2	LN3	LN4	LNS	Over	Under	Inverse Log
Ré														·	
1		11:20:00 00d 00:10.	0 61.1	71.1	64.2	57.3	-7	64	63.7	61.2	57.6	57.4			1288250
†;	7/16/2013	11:20:10 00d 00:10		68.7	61.1	57.6	•.•	60.5	60.3	58.9	57.6	57.6			741310.2
2	7/16/2013	11:20:20 00d 00:10.		70.3	62.7	57.8		62.6	62.4	58.5	58	58			1071519
3		11:20:30 000 00:10		70.2	61.1	58.6		61.1	61	60.5	59.7	59.3			1047129
4 5		11:20:40 00d 00:10.		65.7	58,6	53.8		57.9	57.6	55.6	53.9	53.9			371535.2
6		11:20:50 00d 00:10.		68.1	60.6	53.7		60.6	60.4	58.3	54.1	53.9			645654.2
7		11:21:00 00d 00:10.		71	64.6	53.5		64,4	64.1	58.2	53.9	53.7			1258925
8	7/16/2013	11:21:10 00d 00:10.		78	70.4	63.5		70.3	70	67.4	63.9	63.6	<u> </u>		6309573
9		11:21:20 00d 00:10.		77.3	69.3	62.9	·	69	69	67.8	63.3	63.1			5370318
10		11:21:30 00d 00:10.	0 63.7	73.7	68.3	58.8	·.·	68.3	68.1	62.5	58.9	58.9			2344229
11	7/16/2013	11:21:40 00d 00:10.	0 60.6	70.6	61.9	56.8		61.7	61.5	61.2	58.4	57.6			1148154
12		11:21:50 00d 00:10.	0 60.2	70.2	61.7	55.9	<u></u>	61.6	61.S	60,8	56.1	56			1047129
13		11:22:00 00d 00:10.	0 63.6	73.6	67.8	58.2		67.6	67.2	60.1	58.4	58.3			2290868
14	7/16/2013	11:22:10 00d 00:10.	0 61.2	71.2	65.8	58.9	-,-	65.3	64.8	60.3	59.4	59.1			1318257
15		11:22:20 00d 00:10.	0 61.2	71.2	63	58.1		62.9	62.8	61.1	58.4	58.2			1318257
16		11:22:30 00d 00:10.	0 64.3	74.3	67.3	61.7		66.9	66.3	62.7	61.9	61.8			2691535
17		11:22:40 00d 00:10.		72.7	67.6	60.7		67.3	66.6	62.7	60.9	60.8	+		1862087
18		11:22:50 00d 00:10.		74.2	65.8	62		65.7	65.6	64.1	62.2	62.1			2630268
19	7/16/2013	11:23:00 00d 00:10.		78.9	71.7	63		71.5	71.3	67.8	64.4	64			7762471
20				74.7	69.4	61.6		68.7	68.1	65	62.9	62.2			2951209 933254.3
2		11:23:20 00d 00:10	***************	69.7	61.7	59	-,-	61.2	60.7	59.6	59.1 61.2	59.1 60.9	· · · · · · · · · · · · · · · · · · ·		2630268
23		11:23:30 00d 00:10.		74.2	66.3	60.3		66.1	66	62.9 63.6	61.2 62.7	62.5			2187762
2		11:23:40 00d 00:10	***********	73.4	65.7	62.3		64.5 67.6	64.5 67.3	65.6	63.6	63.6			3715352
24		11:23:50 00d 00:10	•••• • • • • • • • • • • • • • • • • •	75.7	67.7	63.2 62.8		68.4	68.3	67.6	63	62.9			5370318
2		11:24:00 00d 00:10		77.3	68.5 67.1	62.8		66.8	66.7	64.9	63.1	63			3235937
2		11:24:10 00d 00:10 11:24:20 00d 00:10		75.1 71.4	67.4	59.2		67.2	66.6	60.1	59.3	59.3		· [1380384
2				73.3	66.9	56.1		66.8	66.6	59.9	56.3	56.2			2137962
2		11:24:30 00d 00:10 11:24:40 00d 00:10	****	72.9	64.4	61.5		64.1	63.7	62.6	61.8	61.7			1949845
2		11:24:50 00d 00:10		71.5	64.9	57.7		64.8	64.8	61	57.9	57.9			1412538
3		11:24:30 00d 00:10		72	64.7	57.4		63.8	63.7	60	57.6	57.5		*****	1584893
3		11:25:10 00d 00:10		80.3	74.7	63		74.5	74.2	69.1	64.8	63.8			10715193
3		11:25:20 00d 00:10		75.1	69.6	59.2	-,-	69.3	68.7	53.6	59.5	59.4			3235937
3		11:25:30 00d 00:10		74.6	67.1	59.5		67.1	66.9	64.3	60.7	60.1			2884032
3				72.9	66.2	59.5		65.9	65.5	62.2	59.8	59.7			1949845
3			.0 58.3	68.3	60	56.4		59.9	59.8	58.4	56.5	56.4			676083
3		11:26:00 00d 00:10	0 58.2	68.2	59.9	54.3		59.8	59.8	58.7	54.7	54.5			660693.4
3		11:26:10 00d 00:10	.0 64.6	74.6	67.5	59		67.3	66.9	63.6	60.4	59.8			2884032
3				73.5	66.8	59.7	<u></u>	66.4	66.1	62.4	59.9	59.8			2238721
4	0 7/16/201	11:26:30 00d 00:10	.0 60.3	70.3	61.7	57.9		61.6	61.5	60.9	58.5	58.2			1071519
4				68.5	59.3	58.1		59	58.9	58.5	58.3	58.2			707945.8
4	******************			68.5	60.8	55.1		60.7	60.6	58.3	55.7	55.2			660693.4
4				68.2	60	54.2		60	59.9	57.6	54.6	54.3		-	1071519
4				70.3	64	57.1		63.5	62.5 64.7	59.1 63	57.2 56.6	57.2 56.2			1513561
4				71.8	65	56		64.9 58.3	58	57.1	56	55.8			562341.3
4				67.5 74.4	59.2	55.8 59.2		57.8	67.3	62.9	59.7	59.6			2754229
4				73.8	68 65.4	61		65.2	65	64.1	61.4	61.2			2398833
4				73.1	65.1	61		65	64.9	63.1	61.2	61.1			2041738
4				69.1	62.9	58.5		62.2	61.5	59	58.6	58.6			812830.5
5				70.1	63	56.3		62.8	62.5	59.5	57.6	56,8			1023293
			+******	68.1	60.5	56.2		59.4	58.8	57.2	56.4	56.3			645654.2
5				74.7	66.9	60.5		66.8	66.6	64.2	62.6	62.1			2951209
5			****	71.4	63.4	58.4		63.3	63	61.4	58.9	58.6			1380384
5	5 7/16/201			73.2	66.1	59,7		66	65.9	62.4	59.8	59.7			2089296
Ś	6 7/16/201			67.7	62.4	56.9		61.4	60.5	57.5	57.2	57.1			588843.7
	7 7/16/201			67.4	58.3	56.5		58.2	58.1	57.3	56.6	56.6			549540.9
	8 7/16/201			73.6	68.5	55.7		68.5	67.6	58.8	55.8	55.8			2290868
	9 7/16/201			75.4	68.6	63	•,-	68.4	67.7	65.8	63.3	63.1			3467369
	0 7/16/201		0.0 68.2	78.2	70.5	64.5		70.4	70.3	67.2	64.9	64.7			6606934

Address	Start	Measurement Time	Leq	LE	LMAX	LMIN	Ly 🖓	LNI	LN2	LN3	LN4	LN5	Over	Under	Inverse Log
	Time			franki († 1993)	Extensioned	Personager	l strategy a	<u>pa barabalu</u>	F elenserie	E 1997 (1977) (1	Personal Control	Constantin	Louis de la company	Ferres (Varia)	1
R7					r				1	1	1	1	1	T	Lucconcl.
1	7/16/2013	10:50:00 00d 00:10.0	66.5	76.5	69	62.8		68.9	68.5	66.2	63.1	62.9	/		4466836
2	7/16/2013	10:50:10 00d 00:10.0	70.3	80.3	72.3	67.6	<u> </u>	72.1	72.1	70.1	67.7	67,6		*****	10715193
3	7/16/2013	10:50:20 00d 00:10.0	67.4	77.4	70.6	62.3		69.6	68.8	67.2	63	62.5			5495409
4	7/16/2013	10:50:30 00d 00:10.0	72.5	82.5	77.3	64.8	-,-	77.2	76.6	71.3	65.1	64.9			17782794
5	7/16/2013	10:50:40 00d 00:10.0	62.8	72.8	65.4	61.3	-,-	65.4	65.3	62.3	61.4	61.3			1905461
6	7/16/2013	10:50:50 00d 00:10.0	65.4	75.4	68.5	60.4		68.2	67.8	63.9	60.5	60.5			3467369
7	7/16/2013	10:51:00 00d 00:10.0	69.7	79.7	71.9	66.9	-,-	71.8	71.7	69.6	67.2	67			9332543
8	7/16/2013	10:51:10 00d 00:10.0	68.7	78.7	71.9	66.4		71.6	71.3	67.1	66.6	66.5			7413102
9	7/16/2013	10:51:20 00d 00:10.0	75	85	79.7	69		79.3	78.9	73.3	69.4	69.2			31622777
10	7/16/2013	10:51:30 00d 00:10.0	71.9	81.9	73.4	70.5		73.4	73.1	71.8	71	70.7			15488166
11	7/16/2013	10:51:40 00d 00:10.0	68.7	78.7	70.6	63.1	<u></u>	70.6	70.5	69.5	64.9	63.9			7413102
12	7/16/2013	10:51:50 DOd D0:10.0	62.9	72.9	63.6	61.6		63.6	63.5	63	61.7	61.6	• · · ·		1949845
13	7/16/2013	10:52:00 00d 00:10.0	64.7	74.7	66.8	61.9	-7	66.7	66.6	64.2	62.2	62	****		2951209
14	7/16/2013	10:52:10 00d 00:10.0	72	82	73.6	63.5		73.5	73.2	71.5	67.9	65.9	·•••		15848932
15	7/16/2013	10:52:20 00d 00:10.0	70	80	73.8	66.4		73.7	73.5	68.9	66.7	66.5			10000000
16	7/16/2013	10:52:30 00d 00:10.0	68.6	78.6	69.8	67.3	-,-	69.7	69.7	68.7	67.7	67.6			7244360
17	7/16/2013	10:52:40 00d 00:10.0	69.8	79.8	72	66.1	-,-	71.9	71.8	69.7	66.3	66.2			9549926
18	7/16/2013	10:52:50 00d 00:10.0	71.2	81.2	72.9	69.1		72.8	72.7	71.3	69.3	69.2			13182567
19	7/16/2013	10:53:00 00d 00:10.0	66.5	76.5	70.4	60		70.3	70.2	66.4	60.3	60.1			4466836
20	7/16/2013	10:53:10 00d 00:10.0	68.6	78.6	70.8	60.8		70.7	70.6	68.5	62.9	61.8			7244360
21	7/16/2013	10:53:20 00d 00:10.0	70.1	80.1	74.1	64.1		73.9	73.4	66,5	64.2	64.1			10232930
22	7/16/2013	10:53:30 00d 00:10.0	71.1	81.1	74.8	64.8	-,-	74.8	74.5	71.4	65.2	65			12882496
23	7/16/2013	10:53:40 00d 00:10.0	66.5	76.5	67.8	64.5	·	67.7	67.7	66.2	64.7	64.7			4466836
24	7/16/2013	10:53:50 00d 00:10.0	67.9	77.9	69.7	65.7		69.6	69.6	67.6	66.2	65.8			6165950
25	7/16/2013	10:54:00 00d 00:10.0	66.6	76.6	69.1	61.8		69.1	69	66.2	63.1	62.5			4570882
26	7/16/2013	10:54:10 00d 00:10.0	64.1	74.1	67.1	58.5	·/	67	67	61.6	59.2	58.8			2570396
27	7/16/2013	10:54:20 00d 00:10.0	66.8	76.8	68.5	65.3		68.2	68	66.2	65.6	65.4			4786301
28	7/16/2013	10:54:30 00d 00:10.0	68.4	78.4	69.9	67		69.4	69.1	68.3	67.3	67.2			6918310
29	7/16/2013	10:54:40 00d 00:10.0	69	79	71.2	65.4		71.2	71.1	69.7	65.7	65.5			7943282
30	7/16/2013	10:54:50 00d 00:10.0	66,6	76.6	70.2	63.4		70	69.8	65.2	63.8	63.5			4570882
	7/16/2013	10:55:00 00d 00:10.0	66.4	76.4	67.5	63		67.4	67.4	66.7	63.3	63.1			4365158
31 32	7/16/2013	10:55:10 00d 00:10.0	65.7	75.7	68.1	62.6	-,-	68	67.8	66	63.1	62.7			3715352
33	7/16/2013	10:55:20 00d 00:10.0	71.1	81.1	72.7	62.7		72.6	72.5	71.1	64.9	63.8		· · · · · ·	12882496
34	7/16/2013	10:55:30 00d 00:10.0	69.6	79.6	71.8	67.3		71.7	71.5	69	67.5	67.4			9120108
35	7/16/2013	10:55:40 00d 00:10.0	67.6	77.6	71.7	63.9	 	71.2	70.6	66.5	64.2	64		·	5754399
	7/16/2013	10:55:50 00d 00:10.0	71.3	81.3	73.1	69.1		73	72.9	71.2	69.5	69.4			13489629
36	7/16/2013	10:56:00 00d 00:10.0	74.2	84.2	77.9	67.1		77.4	76.8	73.3	67.4	67.3			26302680
37 38	7/16/2013	10:56:10 00d 00:10.0	68.4	78.4	72.2	67.2		71	70.3	68.4	67.4	67.3			6918310
39	7/16/2013	10:56:20 00d 00:10.0	68.4	78.4	72.3	63.9		72.3	72.1	67.3	65	64.4			6918310
40	7/16/2013		66.5	76.5	68	63.5		67.9	67.8	66.6	63.6	63.6		·	4466836
			67.3	77.3	68.5	66.1		68.2	67.6	67	66.4	66.3			5370318
41	7/16/2013	{		+	72.4	66.5		71.7	70.2	67	66.6	66.6			7413102
42	7/16/2013	***************************************	68.7 73.4	78.7	76.1	66.2		76	75.9	73.9	68	67.2			21877616
43	7/16/2013		73.4 61.1	83.4 71.1	66.2	59.7	<u>-</u>	65.3	64.3	61.1	59.9	59.8			1288250
44	7/16/2013	***************************************		************				70.7	70.6	67.4	61.2	61.1			7244360
45	7/16/2013	10:57:20 00d 00:10.0	68.6 71.0	78.6	71.5	61 70.4		73.6	73.4	71.8	70.7	70.6			15488166
46	7/16/2013	10:57:30 00d 00:10.0	71.9 67	81.9	73.7	63.6		69.7	69.1	67.8	64.3	63.8			5011872
47	7/16/2013	10:57:40 00d 00:10.0	67	77				70.5	70.4	69.5	64.4	64.1			7762471
48	7/16/2013	10:57:50 00d 00:10.0	68.9	78.9	70.6	63.7 67.2		70.3	70.4	68.3	67.4	67.3			7762471
49	7/16/2013	10:58:00 00d 00:10.0 10:58:10 00d 00:10.0	68.9	78.9	71			72.1	72.1	68.7	63.1	62.1	+		7585776
50	7/16/2013		68.8	78.8	72.2	61.5	· · · · · · · · · · · · · · · · · · ·	70.5	70.3	66.8	61.2	61.1	+		5623413
51	7/16/2013	10:58:20 00d 00:10.0	67.5	77.5	70.6	61			64.8	63	61	60.8			1905461
52	7/16/2013	10:58:30 00d 00:10.0	62.8	72.8	65.1	60,7		64.9						·	4168694
53	7/16/2013	10:58:40 00d 00:10.0	66.2	76.2	68.7	62.5	l	68.5	68.3	64.4	63.2	62.7		********	5370318
54	7/16/2013	10:58:50 00d 00:10.0	67.3	77.3	68.7	63.9	·	68.7	68.6	67.8	64.8	64.3			
55	7/16/2013	10:59:00 00d 00:10.0	69	79	73.4	63.4		73.3	72.8	64.6	63.6	63.5			7943282
56	7/16/2013	10:59:10 00d 00:10.0	67.7	77.7	73.3	62.6		73.2	72.9	66.7	62.8	62.6			5888437
57	7/16/2013	10:59:20 00d 00:10.0	65.2	75.2	67.4	60.4		67.3	67.3	65.3	60.8	60.5			3311311
58	7/16/2013	10:59:30 00d 00:10.0	70.3	80.3	73.5	64.2		73.3	72.8	69.7	67.1	65.5			10715193
59	7/16/2013	10:59:40 00d 00:10.0	68	78	71.3	62.4		71.2	71	67.3	62.7	62.5			6309573
60	7/16/2013	10:59:50 00d 00:10.0	70.8	80.8	72.4	63.1		72.1	71.4	70	67.7	65.3			12022644

	Address	Start Time	Measur	ement Time	Leq	LE	LMAX	LMIN	Ly	LN1	LN2	LN3	LN4	LN5	Over	Under	Inverse Log	Ove Le
	R8																	<i>c.</i>
****	1	7/16/2013	10:50:00	00d 00:10.0	63.8	73.8	66.1	57.6		65.9	65.8	64.7	59.3	58.5			2398833	59
,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	2	7/16/2013	10:50:10	00d 00:10.0	56	66	58.5	54.5		57.9	57.6	55.3	54.6	54.6			398107.2	
		7/16/2013	10:50:20		59.8	69.8	60.7	58.4		60.5	60.5	59.6	59.1	58.9			954992.6	
		7/16/2013	10:50:30	00d 00:10.0	+	59	60	58.4	·····	59.6	59.5	59.1	58.6	58.5	a		794328.2	
	4 5	7/16/2013	10:50:40	00d 00:10.0	64.2	74.2	68.1	59.2	<u></u>	67.9	67.6	63.2	\$9.5	59.4			2630268	
	6	7/16/2013	10:50:50		61.7	71.7	63	61.2	·····	62.9	62.7	61.8	61.3	61.2			1479108	
	7	7/16/2013	10:50:50		60.5	70.5	62	59.2		61.7	61.7	60.5	59.6	59.3			1122018	
	h	7/16/2013	10:51:10	00d 00:10.0	57.7	67.7	60.2	55.3	······································	59.9	59.3	58.6	\$5.6	55.5			588843.7	
	8		10:51:20		55.5	65,5	56.1	54.8		56	56	55.3	55. 1	55			354813.4	
		7/16/2013	10:51:30		58.6	68.6	60,1	56	-,- 	60	59.9	57.8	56.1	56.1			724436	
	10 11	7/16/2013	10:51:30	00d 00:10.0	61.5	71.5	62.2	59.9	····	62.1	62	61.4	60,2	60.1			1412538	
		7/16/2013	10:51:50	00d 00:10.0	60.8	70.8	62.1	60		62	61.6	60.9	60.1	60.1			1202264	
	12		10:51:50		+	68.6	61		<u></u>	60.9	60.7	58.2	57.1	57	+		724436	
	13	7/16/2013			58.6	*****	61.9	56.9 57.5	·····	61.7	61.5	60	57.7	57.6			1047129	
		7/16/2013	10:52:10	00d 00:10.0		70.2		57.9	<u></u>	61.8	61.7		58.6	58.2			1122018	
	15	7/16/2013	10:52:20	00d 00:10.0	60.5	70.5 66.1	61.9 57.9			57.6	57.5	61.1 56	54.8	54.7			407380.3	
	16	7/16/2013	10:52:30			66.1	************	54.6		57.6	57.5	57.7	57.5	57.5			602559.6	
	17	7/16/2013	10:52:40	00d 00:10.0	57.8	67.8 71.1	58.4	57.4		58.5 63	63	59.5	57.5	57.5			1288250	
	18	7/16/2013 7/16/2013	10:52:50	00d 00:10.0 00d 00:10.0		71.1 70.3	63.1 62.3	57.6 58		62.2	62.2	60.5	58.2	58.1			1071519	
	19		10:53:00			**********	*******	******	<u>``</u>	59.8	59.6	57.4	56.6	55.6			616595	
	20	7/16/2013	10:53:10	00d 00:10.0		67.9	60 50 6	56.5	·	59.2	58.9	57.6	56.4	55.9			537031.8	
	21	7/16/2013	10:53:20			67.3	59.6	55.8				54.5	53.4	*			281838.3	
	22	7/16/2013	10:53:30			64.5	55,8	53.2	····	55.8	55.7	57.2	55	53.3 54.6	+		575439.9	
	23	7/16/2013	10:53:40			67.6	58.8	54	····	58.8	58.6	57.9	57.6	\$7.6			645654.2	
	24	7/16/2013	10:53:50			68.1	59	57.5		58.9	58.8		*				831763.8	
	25	7/16/2013	10:54:00			69.2	59.8	58.6		59.7	59.6	59.4	58.7	58.6	+		602559.6	
	26	7/16/2013	10:54:10		57.8	67.8	59.1	56.3		59	58.9	58.2	56.5	56.4			354813.4	
	27	7/16/2013	10:54:20		************	65.5	57.5	53.5	·····	57.5	57,4	55	53.8	53.6			630957.3	
	28	7/16/2013	10:54:30	******		68	59	57.2		58.9	58.9	57.7	57.4	57.3 55.9			812830.5	
	29	7/16/2013	10:54:40			<u>69.1</u>	61.5	55.8	·	61.4	61	57.3	55.9 60.7				1445440	
	30	7/16/2013	10:54:50		*****	71.6	62.9	60.1		62.9	62.8	61.4	57.7	60.5 57,6			741310.2	
	31	7/16/2013	10:55:00			68.7	60.1	57.4	·	59.9	59.8	59.4	57.3	57.2			1023293	
	32	7/16/2013	10:55:10		+	70.1	61.6	57.1	·	61.5	61.2	60		+			1288250	
	33	7/16/2013	10:55:20		******	71.1	63.2	59.2	· · · · · · · · · · · · · · · · · · ·	62.8	62.3	60.9	59.5	59.3			1737801	[
	34	7/16/2013	10:55:30	***************************************		72.4	63.6	60		63.5	63.3	63	60.9 57.7	60.4 57.6			645654.2	ł
	35	7/16/2013	10:55:40			68.1	60	57.5		59.4	59	58.3	*********				537031.8	
	36	7/16/2013	10:55:50			67.3	58.5	56		58.5	58.3	57,4	56.2	56.1			831763.8	
	37	7/16/2013	10:56:00		+	69.2	60.4	57.5		60.2	60.1	59.5	57.7	57.7			676083	
	38	7/16/2013	10:56:10			68.3	59.5	\$7.8	ļ	59,3	59.2	58.3	57.9	57.9			1659587	
	39	7/16/2013	10:56:20			72.2	63.9	58		63.7	63.7	62.4	58.1	58.1	+		1071519	
	40	7/15/2013	10:56:30			70.3	63.9	53.7		63.7	63.4	60.7	54.8	54.2			245470.9	
	41	7/16/2013	10:55:40			63.9	57.2	51.8		56.3	55.4	52.5	51.9	51.8			1318257	1
	42	7/16/2013	10:56:50			71.2	62.7	57.2		62.5	62.4	61.5	58.2	58 58.6			1230269	
	43	7/16/2013	10:57:00			70.9	63.1	58.1		62.7	62.6	61.1	58,9	58.6			457088.2	
	44	7/16/2013	10:57:10			66.6	58.1	55.7		58	57.8	56.1	55.8	55.8				
	45	7/16/2013	10:57:20	******************		68.9	59.4	57.9		59.2	59.2	58.9	58.1	58	·		776247.1	
	46	7/16/2013	10:57:30		**************	68.1	58.9	57.4		58.8	58.8	58.3	57.5 56	57.4			478630.1	
	47	7/16/2013	10:57:40		*****	66.8	58.3	55.8		58.1	57.8	56.8		+			389045.1	1
	48	7/16/2013	10:57:50			65.9	57.6	\$4.3		57.4	57	55.8	54.5	54.4	• • • • • • • • • • • • • • • • • • • •		501187.2	1
	49	7/16/2013	10:58:00		*********	67	59.2	55.3		59.1	58.8	56.3	55.5	55.4 57.7			676083	1
	50	7/16/2013	10:58:10			68.3	59	56.9	<u>-</u>	58.9	58.7	58.1	57.7	4	· /		346736.9	•
	51	7/16/2013	10:58:20			65,4	58	54		57.9	57.8	55.1	54.1	54.1				1
	52	7/16/2013		00d 00:10.0		70.5	61.9	54.5	·	61.7	61.5	60.5	55.8	55.1			1122018	
	53	7/16/2013		00d 00:10.0		66.4	60.4	55.4		59.9	59.4	56,1	55.7	55.5	.+		436515.8	
	54	7/16/2013		00d 00:10.0		69	61	55.2		61	60.9	58	55.5	55.4			794328.2	
	55	7/16/2013		00d 00:10.0		69.1	61.4	57	ļ	61.2	60.9	58.6	58	57.6			812830.5	-
	56	7/16/2013		00d 00:10.0		68.9	60	56.6	ļ	59.9	59.9	58.3	56.8	56.7			776247.1	1
	57	7/16/2013	10:59:20			70.6	61.2	59.5		60.9	60.9	60.5	59.8	59.7			1148154	- 1
	58	7/16/2013	10:59:30			68.6	61.5	55.4		61.3	61.2	58,9	56.3	55.9			724435	2
	59	7/16/2013	10:59:40	00d 00:10.0	55	65	55.7	54.6		55.6	55.6	54.9	54.7	54.7			316227.8	-
	60	7/16/2013	10:59:50	00d 00:10.0	57.1	67.1	59.8	53.3	-,-	59.7	59.6	54.8	53.5	\$3.4			512861.4	1

Addre	ss Start Time	Measurement Time	Leq	LE	LMAX	LMIN	Ly	LN1	LN2	LN3	LN4	LN5	Over	Under	Inverse Log
R9		<u></u>													
1	7/16/2013	10:50:00 00d 00:10.0	61.6	71.6	69	57.5		68.2	67.4	60.6	57.7	57.6			1445440
	7/16/2013	10:50:10 00d 00:10.0	75.2	85.2	79.6	61		79.5	79	73.6	65.2	63.8			33113112
2			63.7	73.7	70.8	61.6		69.7	68.8	63,3	61.7	61.6			2344229
3	7/16/2013	***************************************	*************		·{·····	62		66	66	64.9	63.1	62.5			3090295
4	7/16/2013	10:50:30 00d 00:10.0		74.9	66.2			*************					h		3981072
5	7/16/2013	10:50:40 00d 00:10.0		76	68.3	63.4		68.1	68	65.4	63.5	63.5			3630781
6	7/16/2013	10:50:50 00d 00:10.0		75.6	67.3	64.1		66.6	66.3	65.5	64.2	64.2			
7	7/16/2013	10:51:00 00d 00:10.0	69.9	79.9	71.8	67.2		71.7	71.5	69.3	68.6	68.5			9772372
8	7/16/2013	10:51:10 00d 00:10.0		78.8	71.1	66.8	·	70.B	70,6	68.3	67.2	67			7585776
9	7/16/2013	10:51:20 00d 00:10.0	67.3	77.3	68.2	66.3		68.1	68,1	67.4	67	66,9			5370318
10	7/16/2013	10:51:30 00d 00:10.0	60.9	70.9	66.3	59.7		65.2	64.1	61.3	59.9	59.8			1230269
11	7/16/2013	10:51:40 00d 00:10.0	62.6	72.6	63.9	60.1	<u></u>	63.8	63.8	62.5	60.2	60.2	*		1819701
12	7/16/2013	10:51:50 00d 00:10.0	67.6	77.6	70.1	62.5		70	70	67.1	62.7	62.6			5754399
13	7/15/2013	10:52:00 00d 00:10.0	69.3	79.3	71.1	66.4		71.1	71	69.2	66.8	66.5	-*-*		8511380
14	7/16/2013	10:52:10 00d 00:10.0	66.6	76.6	68.7	62.2		68.7	68.5	67.5	63	62.6			4570882
15	7/16/2013	10:52:20 00d 00:10.0	64.1	74.1	67.8	58,9		67.6	67.4	61.6	59	58.9			2570396
16	7/16/2013	10:52:30 00d 00:10.0		79.6	70.9	67		70.8	70,6	69.8	67.4	67.2			9120108
17	7/16/2013	10:52:40 00d 00:10.0	62.7	72.7	69.3	59.1		68	66.7	64.1	59.9	59.4			1862087
18	7/16/2013	10:52:50 00d 00:10.0		75.2	67.5	58.6		67.4	67.4	63.6	58,8	58.7			3311311
19	7/16/2013	10:53:00 00d 00:10.0		74	67.1	61.9		66.6	65	64.1	62.1	61.9		[2511886
20	7/16/2013	10:53:10 00d 00:10.0		80.3	72.7	65.7	·.•	72,6	72.6	70	67.2	66.7			10715193
21	7/16/2013	10:53:20 00d 00:10.0	+	73.2	66.1	58.1	-,-	65.5	65.2	64.6	59.2	58.5			2089296
22	7/16/2013	10:53:30 00d 00:10.0		74	66.3	57.7	-,-	66.2	66	63.5	58	57.8	•		2511886
23	7/16/2013	10:53:40 00d 00:10.0		74.1	66.2	62.7	-7	66.1	65.9	64	62.9	62.8			2570396
24	7/16/2013	10:53:50 00d 00:10.0		73	66.5	60.5		66	64.9	61.8	60.7	60.5			1995262
25	7/16/2013	10:54:00 00d 00:10.0		74.2	67.3	59.3	-,-	67.2	67.1	64.7	59.6	59,4			2630268
26	7/16/2013	10:54:10 00d 00:10.0		75.8	67	59.8		65.9	66.8	66	61.7	60.7	1		3801894
		10:54:20 00d 00:10.0	+	76.7	68.5	64.7		68.4	68.3	66.9	64.9	64.8			4677351
27		10:54:30 00d 00:10.0	+	73.3	66.4	59.5		66.3	66.2	63.3	59.9	59.6			2137962
28	*****			75	66	61.1		65.9	65.8	64.8	62.6	61.8			3162278
29	7/16/2013	10:54:40 00d 00:10.0 10:54:50 00d 00:10.0		72.1	65.3	60		64,9	64.5	62.1	60.2	60			1621810
30	7/16/2013			78.2	70.4	63.1	·····	70.2	69.9	67.6	63.9	63.5			6606934
31	7/16/2013	10:55:00 00d 00:10.0			70.4	63.4		70.4	70	64.4	63.6	63.5			4168694
32	7/16/2013	10:55:10 00d 00:10.0		76.2		62.9		68.1	68.1	64.8	63.1	63			3801894
33	7/16/2013	10:55:20 00d 00:10.0		75.8	68.2 70.6	64.8		70.5	70.3	68.8	65.9	65.2			7585776
34	7/16/2013	10:55:30 00d 00:10.0		+				75.8	75.4	67.2	65	64.9		·	14125375
35	7/16/2013	10:55:40 00d 00:10.0		81.5	76	64.8		74.2	73.6	65.5	63.8	63.5			5623413
36		10:55:50 00d 00:10.0		77.5	74.6	63.4		68.4		65.1	63.5	63.4			3801894
37	7/16/2013	10:56:00 00d 00:10.0		75.8	68.5	63.1		67.1	68.1 66.7	64.9	62.3	62.1	• • • • • • • • • • • • • • • • • • • •		3311311
38		10:56:10 00d 00:10.0		75.2	67.2	61.9						63.5			3388442
39	7/16/2013	10:56:20 00d 00:10.0		75.3	67.4	63.1	ļ	67.2	67.1	65 62.7	63.9 61.9	61.8	- 1		2570396
40		10:56:30 00d 00:10.0		74.1	66.7	61.8		66.6 73.4	66.3 73.3	70.2	66.7	66.6			12302688
41		10:56:40 00d 00:10.0		80.9	73.8	66.5			· • • • • • • • • • • • • • • • • • •						812830.5
42	7/16/2013	10:56:50 00d 00:10.0		69.1	66.8	55.3		65.7	64.9	58,6	55.4	55.3	.+		2754229
43		10:57:00 00d 00:10.0		74.4	68.9	55.2		68.7	68.2	59.6	55.3	55.3	• • • • • • • • • • • • • • • • • • • •		10232930
44		10:57:10 00d 00:10.0		80,1	72.2	68.1		72.1	72	69.5	68.4	68.2			3162278
45	7/16/2013	10:57:20 00d 00:10.0		75	69.9	62.7	ļ	69.5	69.3	63.9	63.1	63.1			
46	7/16/2013	10:57:30 00d 00:10.0		75.1	68	60.8		67.9	67.8	63.7	61	60.9			3235937 3890451
47	7/16/2013	10:57:40 00d 00:10.0		75.9	67.7	64		67.4	67.3	66	64.4	64.1			
48		10:57:50 00d 00:10.0	******	76.5	68.8	63.6		68.6	68.5	66.1	64	63.8			4466836
49		10:58:00 00d 00:10.0		73.3	67	59		66.6	66.5	61.6	59.5	59.2			2137962
50	7/16/2013	10:58:10 00d 00:10.0		75.2	68.7	61.6		68.3	67.7	63.9	62.1	61.8			3311311
51	7/16/2013	10:58:20 00d 00:10.0		74.1	69.1	61.9		68.9	68.2	64.1	62.2	62.1			2570396
52	7/16/2013	10:58:30 00d 00:10.0	63,5	73.5	65.3	61.6		65.2	65.1	63.3	62.2	61.9			2238721
5.	7/16/2013	10:58:40 00d 00:10.0	62.8	72.8	67	59.9		65.5	63.7	61.2	60	60			1905461
54		10:58:50 00d 00:10.0	68.9	78.9	72.7	60.9		72.6	72.3	68.2	62.2	61.5			7762471
55		10:59:00 00d 00:10.0	63.1	73.1	64.1	60.2		64	63.9	63,4	60.5	60.3			2041738
56	*****	10:59:10 00d 00:10.0		77.6	70.7	62.9		70.5	70.4	66.5	63.1	63			5754399
5				75.8	68.7	62.6		68.6	68.4	64.3	62.7	62.6			3801894
58				77.2	68.9	65.3		68.7	68.6	67.1	65.6	65.5			5248075
	*****			77.4	68.6	65.3		68.5	68.4	67.1	65.5	65.4			5495409
60	7/16/2013	***************************************		73.2	68.8	59.3		68.7	68.4	62.4	59.5	59.4			2089296

Addr	ess Start Time	Measurement Tim	e Leq	LE	LMAX	LMIN	Ly	LN1	LN2	LN3	LN4	LN5	Over	Under	Inverse Log
R1			*****			,									
1		3 10:50:00 00d 00:1	0.0 68.5	78.5	71	62.3		70.8	70.5	68.2	63.7	63.2			7079458
				77,7	74.8	58.6		72.5	68.8	62.1	58.7	58.7			5888437
3	7/16/201	********		92.3	87.3	66.3		87.1	86.7	79.6	68.9	67.4			1.7E+08
F				74.8	66.3			65.7	65.5	65.3	64.3	64			3019952
4	7/16/201	~. { ~ ~ ** *** ~ *** *********		******	****	63.7		63.3	63.1	62.1	61.1	61			1621810
5				72.1	63.7	61		69.1		65.3		63.3			4073803
6	7/16/201	······································		76.1	69.2	63.1	×	•	68.9 cc o	64.9	63.3	63.1			3715352
7	7/16/201	~~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~		75.7	68.7	63		67.7	66.2		63.5 cc				8511380
B				79.3	72.1	65.6	·····	72.1	71.9	69	66	65.8			8709636
9	7/16/201			79.4	71.3	66.2	·····	71.2	71	69.1	67.3	67.1			
10				76.8	68.4	60.7		68.3	68.3	68	62.6	61.6			4786301
11				70.7	63.1	57.6		62.7	62.1	60.8	57.9	57.8			1174898
12				71.8	63.3	59.5		63.2	63.1	62.7	59.7	59.6		*****	1513561
1	7/16/201	3 10:52:00 00d 00:1	0.0 69.8	79.8	71.6	60.3	·	71.2	71.1	69.6	63	61.7			9549926
14	7/16/201	3 10:52:10 00d 00:1	0.0 68	78	72	64		71.8	71.7	67	64.1	64		*****	6309573
15	7/16/201	3 10:52:20 00d 00:	66 66	76	70	61.2	*,*	70	69.7	65.2	62.3	61.7			3981072
16	5 7/16/201	3 10:52:30 00d 00:	0.0 67	77	69.3	61		69.1	69	66.9	61.4	61.1			5011872
17		3 10:52:40 00d 00:	0.0 68.9	78.9	71.4	65.8	-,-	71.3	71.1	68.7	67.4	66.6			7762471
18	3 7/16/201	3 10:52:50 00d 00:	10.0 61.6	71.6	65.8	59		6S.3	65	61.1	59.3	59.1			1445440
19		3 10:55:00 00d 00::	10.0 66.9	76.9	69.2	60.2		69.1	69	66.6	61.8	61			4897788
20			10.0 67.1	77.1	72.5	60.6		71.8	69.8	63.1	60.8	60.7			5128614
2			68.8	78.8	72.6	63.5		72.6	72.4	69	63.7	63.7			7585776
23			0.0 61.6	71.6	64.3	55.7		64.3	64.2	60,8	56.1	55.9			1445440
2				75.2	66.6	62.9	-,-	66.6	66.4	65.3	63,9	63.4			3311311
24				75.4	67.9	62		67.8	67.6	64.9	62.3	62.2			3467369
2!				74.7	65.9	63.6		65.8	65.5	64.7	63.9	63.8			2951209
2				72.5	64.3	61.1		63.9	63.6	62.5	61.4	61.2			1778279
				75.2	66.7	62.9		66.7	66.6	65.2	63.3	63.1			3311311
2			*****************	77	68.8	63.1		68.7	68.5	67.5	63.8	63.7		· / · · · · · · · · · ·	5011872
2				75.5	68.3	63.1		68.2	68	64.3	63.3	63.2			3548134
2				73.8	· · · · · · · · · · · · · · · · · · ·	62.1		64.9	64.7	64	62.3	62.2		h	2398833
				74.7	65 67.3	62.6		67.2	66.8	64.4	62.9	62.6			2951209
					*************	63.4		70.6	70.2	68.1	65.6	64.5			6760830
3		***************************************	******	78.3	70.7			66.8	66.2	64.3	62.1	61.9			3019952
3				74.8	67.4	61.8	·····*		69.4	64.9	63.4	63.3			4265795
				76.3	69.7	63.3		69.6		***	67.6				7943282
3					70.4	65	· · · · · · · · · · · · · · · · · · ·	70.4	70.3	68.9		66.1 65.3		-	13489629
3				81.3	74.5	65.2	· · · · · · · · · · · · · · · · · · ·	74,4	74.1	69.8	65.5				2884032
3				74.6	71.1	63.6		69.7	68.3	64.9	63.9	63.7			
3				77.5	70.4	64.1		70.4	70.1	66.7	64.3	64.2	·		5623413
3				75.7	66.5	64		66.4	66.4	65.8	64.8	64.5			3715352
4				72.8	64.5	61		64.3	64	63.1	62.2	61.7			1905461
4	1 7/16/20			74.5	69.1	58.9		68.1	66.5	60.8	59.2	59			2818383
4	2 7/16/20	3 10:56:50 00d 00:	10.0 70.2	80.2	73.1	62		73.1	72.9	70.4	63.7	62.9			10471285
4	3 7/16/20	3 10:57:00 00d 00:	10.0 54.4	64.4	62	52.5		61	59.7	53.9	52.6	52.6			275422.9
4		3 10:57 10 00d 00:	10.0 66.3	76.3	68.3	55.1	:	68.3	68.3	65.4	57.7	56.4			4265795
4			10.0 69.5	79.5	70.8	67.8		70,7	70.6	69.3	68	68			8912509
4			10.0 64.6	74.6	68.3	62.5		67.5	66.7	65	63.8	63.1			2884032
4				76.6	68.5	62.1		68.3	68.3	64.9	62.3	62.2			4570882
4				76.4	68.8	64.2		68.7	68,6	66.3	64.3	64.3			4365158
4				77.1	71.1	61.1		71	70.5	66.6	63.6	62.2			5128614
				77.2	70.8	59.3		70.7	70.7	62.8	59.4	59.3			5248075
5				74.1	70.1	62.6	-,-	69.1	68	64.5	62.8	62.7	*		2570396
5				67.9	62.8	54.5		62.1	61.4	57.7	54.6	54.5			616595
F				73.3	64.9	60.4	· [·····	64.8	64.7	63.3	61.3	61.3			2137962
P	3 7/16/20				71.6	61.3		71	70.2	64.3	61.7	61.6		······	5370318
	4 7/16/20			77.3				71.8	71.6		63.2	63.2			4168694
	5 7/16/20			76.2	71.8	63.1				64 63.9	60,8	60.6			2398833
	6 7/16/20			73.8	65.5	60.5	······	65.4	65.3						5495409
	7 7/16/20			77.4	69.7	64.8		69.6	69.5	66.9	65.2	64.9			4897788
	8 7/16/20			76.9	70	63.9		69.9	69.6	65.8	64.1	64		••	4265795
5	9 7/16/20			76.3	68.8	64		68.6	68.3	65.7	64.2	64.1			
	0 7/16/20	3 10:59:50 00d 00:	10.0 69.1	79.1	71.1	66.5		71	70.6	68.9	67	66.8			8128305

Addre	ss Start Time	Measur	ement Time	Leq	LE	LMAX	LMIN	Ly	LN1	LN2	LN3	LN4	LN5	Over	Under	Log	0
R11																 1	5
1	7/16/2013	9:25:00	00d 00:10.0	59	69	61.4	56.5	•,-	61.3	61.1	59.7	56.9	56.7			794328.2	
2	7/16/2013	9:25:10	00d 00:10.0	56	66	57.3	55.4	·.•	57	56.4	55.8	55.5	55.4			398107.2	
3	7/16/2013	9:25:20	00d 00:10.0	58.4	68.4	60	57.2		59.7	59.3	58.3	57.6	57.5			691831	
4	7/16/2013	9:25:30	00d 00:10.0	59.8	69.8	60.5	57.4		60.4	60.4	59.9	57.6	57.5			954992.6	
5	7/16/2013	9:25:40	00d 00:10.0	58.8	68.8	60.3	57.1		60.2	60.2	58.9	57.5	57.3			758577.6	
6	7/16/2013	9:25:50	00d 00:10.0	55.9	65.9	57.1	54.7		56.9	56.8	56.4	54.8	54.7		[389045.1	
7	7/16/2013	9:26:00	00d 00:10.0	57	67	57,9	54.9		57.6	57.2	57	55.4	55		[501187.2	
8	7/16/2013	9:26:10	00d 00:10.0	59.4	69.4	60.2	57.8		60.1	60.1	59.3	58.1	57.9			870963.6	
9	7/16/2013	9:26:20	00d 00:10.0	58,1	68.1	\$9.7	56.8		59.7	59.7	58	56.9	56.8			645654.2	
10	7/16/2013	9:26:30	00d 00:10.0	58	68	59.4	56.2		59.3	59.2	58.3	56.4	56,2			630957.3	
11	7/16/2013	9:26:40	00d 00:10.0	56.3	66.3	57.1	\$5.5	-,*	57	57	56.1	55.6	55.6			426579.5	
12	7/16/2013	9:26:50	00d 00:10.0	56.6	66.6	57.4	55.5		57.3	57.2	56.9	55.9	55.7			457088.2	
13	7/16/2013	9:27:00	00d 00:10.0	57	67	57.8	55.3	-,-	57.7	57.7	56.9	55.5	55.4			501187.2	
14	7/16/2013	9:27:10	00d 00:10.0	60	70	60.9	57.7	<u></u>	60.9	60.8	59.9	58.5	58.1			1000000	
15	7/16/2013	9:27:20	0.01:00 b00	59.3	69.3	60.5	57.9	-,-	60.4	60.4	59.3	58.5	58.1			851138	
15	7/16/2013	9:27:30	00d 00:10.0	56.5	66.5	57.9	55.9		57,6	57.2	56.6	56.1	56			446683.6	
17	7/16/2013	9:27:40	00d 00:10.0	55.9	65.9	56,6	55.1	-,-	56.5	56.5	56	55.3	55.2			389045.1	
18	7/16/2013	9:27:50	00d 00:10.0	56.3	66.3	56.9	55.4	-,-	56.9	56.8	56.2	55.5	55.5			426579.5	
19	7/16/2013	9:28:00	00d 00:10.0	54.4	64.4	56.8	53.5		56.5	56.2	54.2	53.6	53.6		ļ	275422.9	
20	7/16/2013	9:28:10	00d 00:10.0	56.3	66.3	56.9	54.1		5 6 .9	56.8	56.2	54.6	54.2	* * * *		426579.5	
21	7/16/2013	9:28:20	00d 00:10.0	58.1	68.1	58.9	56.8	-,-	58.9	58.8	58	56.9	56.9			645654.2	
22	7/16/2013	9:28:30	00d 00:10.0	56.4	66.4	57.1	55.5	-,-	57	56.9	56.5	55.7	55.6			436515.8	
23	7/16/2013	9:28:40	00d 00:10.0	59.2	69.2	60.7	56.6	-,-	60.6	60.5	59.2	57.1	56.9			831763.8	
24	7/16/2013	9:28:50	00d 00:10.0	59.1	69.1	59.6	58.7		59.5	59.4	59.2	58.9	58.8			812830.5	
25	7/16/2013	9:29:00	00d 00:10.0	\$7.7	67.7	59.4	56.2		59.3	59.2	57.9	56.5	56.4			588843.7	
26	7/16/2013	9:29:10	00d 00:10.0	\$5.2	65.2	56.2	55		56	55.6	55.2	55	55			331131.1	
27	7/16/2013	9:29:20	00d 00:10.0	54.5	64.5	55.7	53.5		55.6	55.6	54.6	53.6	53.6			281838.3	
28	7/16/2013	9:29:30	00d 00:10.0	54.7	64.7	55.2	54		55.2	55.2	54.6	54.1	54.1			295120.9	
29	7/16/2013	9:29:40	00d 00:10.0	55.1	65.1	56.2	54.3		56	55.9	55	54.6	54.5			323593.7	
30	7/16/2013	9:29:50	00d 00:10.0	58.7	68.7	60.6	54.3		60.5	60.4	58	54.5	54.4			741310.2	
31	7/16/2013	9:30:00	00d 00:10.0	56	66	59.7	54.6	-7	59.2	58.8	55.6	54.7	54.7			398107.2	
32	7/16/2013	9:30:10	00d 00:10.0	54	64	\$5,8	52.8		55.7	55.5	54.2	52.9	52.9			251188.6	
33	7/16/2013	9:30:20	00d 00:10.0		66.7	58.9	53.1		58.2	57.2	56.3	53.7	53.3			467735.1	
34	7/16/2013	9.30:30	00d 00:10.0	58.6	68.6	60.3	57	-,-	60.2	60	58.5	57.1	57.1			724436	
35	7/16/2013	9:30:40	00d 00:10.0	59.5	69.5	61	58		61	60.8	59.5	58.2	58.1			891250.9	i .
36	7/16/2013	9:30:50	00d 00:10.0	59.5	69.5	60.2	58.2		60.2	60.2	59.3	58.3	58.3			891250.9	
37	7/16/2013	9:31:00	00d 00:10.0	58.1	68.1	59.7	57.1	<u>.</u>	59.4	59.1	58.1	57.4	57.2			645654.2	
38	7/16/2013	9:31:10	00d 00:10.0	56.9	66.9	58.7	56		58.5	58.2	56.7	56.1	56.1			489778.8	
39	7/16/2013	9:31:20	00d 00:10.0	56	66	56.7	55.3		56.5	56.4	56	55.4	55.3			398107.2	
40	7/16/2013	9:31:30	00d 00:10.0	58.3	68.3	59.3	56.2	- <u></u>	59.2	58.8	58	57.5	56.9			676083	
41	7/16/2013	9:31:40	00d 00:10.0	59.3	69.3	60.4	58	-,-	60.2	60.2	59.5	58.1	58			851138	
42	7/16/2013	9:31:50	00d 00:10.0	60	70	61.7	57.7		61.5	61.4	59.8	58.4	58.1			1000000	
43	7/16/2013	9:32:00	00d 00:10.0	59.3	69.3	60.4	57.2		60.3	60.3	59.4	57.5	57.3			851138	
44		9:32:10	00d 00:10.0	58.9	68.9	59.9	58.1		59.7	59.6	58.9	58.2	58.2			776247.1	I
45	7/16/2013	9:32:20	00d 00:10.0	57.9	67.9	58.5	57.2		58.4	58.3	57.9	57.3	57.3			616595	
46	7/16/2013	9:32:30	000 00:10.0	57.9	67.9	58.9	56.8		58.6	58.5	57.8	56.9	56.8			616595	1
47	7/16/2013	9:32:40	00d 00:10.0	57.3	67.3	\$9.7	55.3		59.6	59.4	57.6	55.3	55.3			537031.8	l
48	7/15/2013	9:32:50	00d 00:10.0	56.5	66.5	56.9	56		56.7	56.7	\$6.5	56.2	56.1			446683.6	ł
49	7/16/2013	9:33:00	00d 00:10.0	56.1	66.1	57.5	55.2	<u>.</u>	57.2	56,9	56		55.4			407380.3	1
50	7/16/2013	9:33:10	00d 00:10.0	57.3	67.3	61.4	55.3		60.9	60	56.3	55.7	55.6			537031.8	1
51			00d 00:10.0	57.7	67.7	61.2	54		60.7	60.4	56.5	54.2	54.1			588843.7	
52	7/16/2013	9:33:30	00d 00:10.0	59.6	69.6	61.7	56.8		61.6	61.2	59.8	57.2	56.8			912010.8	1
53					64.2	56.8	53.5		56.5	56.2	53.8	53.6	53.6			263026.8	
54			00d 00:10.0	54.2	64.2	55	53.4		55	54.9	53.7	53.6	53.5			263026.8	1
55		9:34:00			65.9	56.4	55		56.3	56.3	56	55.1	55.1			389045.1	1
56) 00d 00:10.0	57.1	67.1	58.5	55.8		58.2	58	56.6	55.9	55.8			512861.4	1
57	7/16/2013	9:54:20	00d 00:10.0	59	69	60.6	57.8		60.5	60.4	58.1	57.8	57.8			794328.2	
58				58.2	68.2	60.8	56.6		60.6	60.4	57.9	56.7	56.7			660693.4	- 1
59			00d 00:10.0	58.7	68.7	59.7	57.7		59.6	59.5	58.4	57.9	57.8			741310.2	-
60			00d 00:10.0	57	67	59.3	55.3		59.3	59.3	56.6	55.4	55.4			501187.2	-

Addr	ess	Start Time	Measur	ement Time	Leq	LE	LMAX	LMIN	Lγ	LN1	LN2	LN3	LN4	LN5	Over	Under	Log	Ove Le
R1	2																	57
1	7	/16/2013	9:25:00	00d 00:10	0 55.5	65.5	57.4	55	-,-	56.8	56.3	55.4	55.2	55.1			354813.4	
2	7	/16/2013	9:25:10	00d 00:10	0 57.7	67.7	59.3	\$5.7		59.3	58.5	57.2	55.9	55.8			588843.7	
3		/16/2013	9:25:20	00d 00:10	•••	68.7	60.2	56,4	···	60.1	60	59,4	56.7	56.5			741310.2	
4		/16/2013	9:25:30	00d 00:10	••••	65.8	57.5	54.6	-,-	57.2	56.8	55.4	54.7	54.6			380189.4	
5		/16/2013	9:25:40	00d 00:10	• • • • • • • • • • • • • • • • • • •	68.9	60.1	57.4		60	59.8	58.9	57.8	57.6			776247.1	
6		/16/2013	9:25:50	00d 00:10	0 56.7	66.7	57.5	55.8		57.4	57.4	56.8	55.9	55.9			467735.1	
7	7	/16/2013	9:26:00	00d 00:10		67	57.6	56.3	-,-	57.6	57.5	57	56.5	56.4			501187.2	
8		/16/2013	9:26:10	00d 00:10		66.1	56.8	55.2		56.7	56.7	56.2	55.7	55.4			407380.3	
9		/16/2013	9:26:20	00d 00:10.		64.9	55.2	54.4		55.1	55.1	55	54.6	54.5			309029.5	
10		/16/2013	9:26:30	00d 00:10	0 58.2	68.2	59	55		58.9	58.8	58.3	56.2	55.8			660693.4	
11		/16/2013	9:26:40	00d 00:10	0 58.1	58.1	59.9	56.1	·.·	59.8	59.6	58.4	56.2	56.2			645654.2	
12		/16/2013	9:26:50	00d 00:10	0 57.1	67.1	57.9	55.9		57.8	57.8	57.2	56.1	56.1			512861.4	
13		/16/2013	9:27:00	00d 00:10		64	55.9	53.1	•,•	55.5	55.3	54	53.2	53.1			251188.6	
14		/16/2013	9:27:10	00d 00:10	0 55.6	65.6	56.4	54.3		56.4	56.4	55.5	54.7	54.5			363078.1	
15		/16/2013	9:27:20	00d 00:10		64.7	55.4	53.6		55.4	55.3	54.6	53.7	53.7			295120.9	
10		/16/2013	9:27:30	00d 00:10	0 58.3	68.3	59.3	55.2	-,-	59.2	59.2	58.8	55.4	55.3			676083	
17		/15/2013	9:27:40	00d 00:10		68.8	50.1	57,5		60	59.9	58.8	57.8	57.6			758577.6	
18		/16/2013	9:27:50	00d 00:10		67.4	58	56.8		58	57.9	\$7.3	56.9	56.9			549540.9	
19		/16/2013	9:28:00	00d 00:10	.0 57.3	67.3	57.9	56.4		57.8	57.7	57.6	56.9	56.7			537031.8	
20		/15/2013	9:28:10	00d 00;10		66.1	57	55.4		57	56.8	55.8	55.5	55.5			407380.3	
21		/16/2013	9:28:20	00d 00:10	.0 56.3	66.3	57.4	55		57.3	57.2	56.7	55.2	55.1			426579.5	
22	2 7	/16/2013	9:28:30	00d 00:10	.0 55.1	65.1	55,9	54	·	55.8	55.7	55.3	54.1	54.1			323593.7	
2.	3 7	/16/2013	9:28:40	00d 00:10	.0 56.7	66.7	57.7	54 57		57.6	57.6	56.7	54.1	54			467735.1	
24	1 7	/16/2013	9:28:50	00d 00:10	.0 57.4	67.4	57.7	57		57.6	57.6	57.3	57.1	57			549540.9	
23	5 7	/16/2013	9:29:00	00d 00:10	0 57.6	67.6	58.1	57.1		58	57.9	57.7	57.3	57.3			575439.9	
20	5 7	/16/2013	9:29:10	00d 00:10	0 58.6	68.6	60	57.1	·····	59.9	59.8	57.8	57.4	57.2			724436	
27	7 7	/16/2013	9:29:20	00d 00:10	.0 59.4	69.4	60.6	58		60.5	60.4	59.6	58.5	58.3			870963.6	ł
28	3 7	/16/2013	9:29:30	00d 00:10	.0 55.7	65.7	58	54.7		57.8	57.4	55.5	54.9	54.8			371535.2	
29	7	/16/2013	9:29:40	00d 00:10		65.1	57.1	52.6		57.1	57	55.4	52.9	52.8			323593.7	
30) 7	/16/2013	9:29:50	00d 00:10	.0 52.4	62.4	53.9	51.5		53.6	53.4	52	51.6	51.6			173780.1	
31		/16/2013	9:30:00	00d 00:10		66.4	57.3	53.9		57.3	57.2	56.5	54.8	54.4			436515.8	
32	2 7	/16/2013	9:30:10	00d 00:10		66.1	57.6	54.5	·	57.5	57.5	55.4	54.6	54.5			407380.3	
3	3 7	/16/2013	9:30:20	00d 00:10		65.3	57.5	54		57.4	57.2	55.4	54.1	54.1			338844.2	
34		/16/2013	9:30:30	00d 00:10		63.7	54.6	52.9		54.5	54.4	53.9	53	53			234422.9	
3		/16/2013	9:30:40	00d 00:10		65.7	56.4	53,3		56.3	56.3	55.9	53.8	53.6			371535.2	
30		/16/2013	9:30:50	00d 00:10		68.9	59.4	56.3		59.3	59.3	58.9	57.3	56.9			776247.1	1
3		/16/2013	9:31:00	00d 00:10		59.9	60.3	59	····	60.2	60,2	59.8	59.5	59.4	+		977237.2	
30		/16/2013	9:31:10			67.8	59.5	57.2		59.3	59	57.7	57.3	57.2	·		602559.6	
	*******	/16/2013	9:31:20	00d 00:10		68.3	59.4	56.4		59.3	59.2	58.5	57.1	56.8	······		676083 251188.6	
4		/16/2013	9:31:30	00d 00:10		64	56.4	53.1		55.9	55.6	54	53.2	53.2				
4		/16/2013	9:31:40	00d 00:10		62.8	53.6	52.1		53.5	53.5	52.8	52.2	52.2			190546.1 446683.6	
4		/16/2013	9:51:50	00d 00:10		66.5	57.4	52.6		57.2	57.2	56,9	53.3	52. 9 57.4			560693.4	
4		/16/2013	9:32:00			68.2	58.5	57.1		58.5	58.4	58.1	57.5	58.4			891250.9	
4		/16/2013	9:32:10			69.5	60.4	58.3		60.3	60.3 58.8	59.5 58.3	58.6 58.1	58			676083	1
4		/16/2013	9:32:20			68.3	59.1 59.2	57.8 57.7		58.9 58.5	58.5	58.2	57.8	57.8			660693.4	t
4		/16/2013	9:32:30			68.2	58.6			58.1	57.9	57	56.3	56.2	+		489778.8	1
4		/16/2013	9:32:40			66.9 67.2	58.2 57.6	56.2 56.6		57.5	57.4	57.1	56.9	56.8			524807.5	1
4		7/16/2013 7/16/2013	9:32:50 9:33:00			67.5	58.1	56.4		58	58	57.7	56.9	56.6			562341.3	1
+		7/16/2013	9:33:00			65.2	56.4	54.5		56.3	56.1	55.2	55	54.8			331131.1	1
5		/16/2013	9:33:20			63.1	54.5	52.8		54.3	53.9	53.1	52.9	52.9			204173.8	
			9:33:30			65.1	55.5	53.3		55.4	55.3	55.2	54	53.7			323593.7	
		7/16/2013 7/16/2013	9:33:40			66.6	56.9	55.5		56.8	56.8	56.5	56.2	56			457088.2	
5	*********	7/16/2013	9:33:50			68.4	59.7	56.5		59.6	59.5	58.3	56.8	56.6			691831	1
		7/16/2013	9:33:50			65.1	56.8	54.3		56.7	56.6	54.9	54.5	54.4	****		323593.7	1
5		7/16/2013	9:34:10			64.9	55.6	54.5		55.3	55.1	54.8	54.5	54.5			309029.5	1
		7/16/2013	9:34:20			68	58.9	55.6		58.8	58.7	57.8	56.4	56			630957.3	
5	****	7/16/2013	9:34:30			66.6	58.2	55.4		57.8	57.5	57	55.8	55.6			457088.2	1
5		7/16/2013	9:34:40			65.7	57	55.1		56.7	56.3	55.4	55.2	55.2			371535.2	
		7/16/2013	9:34:50			68.2	60.1	56.6	-,-	59.9	59.7	57.4	56.8	56.7	-+		660693.4	1

Address	Start Time	Measureme	ent Time	Leq	LE	LMAX	LMIN	Ly	LN1	LN2	LN3	LN4	LN5	Over	Under	Inverse Log
R13																
1	7/16/2013	9:25:00 00	0d 00:10.0	62.6	72.6	65.9	59	-	65.8	65.7	62.7	59.1	59.1			1819701
2	7/16/2013	9:25:10 00	od 00:10.0	61.8	71.8	62.7	59.2	····	62.6	62.6	61.6	59.8	59.5		** * * *	1513561
3	7/16/2013		0d 00:10.0	65.6	75.6	67.1	62.6		67	67	64.9	62.6	62.6			3630781
4	7/16/2013		Od 00:10.0	63	73	66.7	61.1		66.4	66	62.5	61.3	61.3			1995262
5	7/16/2013	9:25:40 00	0d 00:10.0	64	74	65.3	61.7	··· ··	65.2	65.1	63.3	62.3	62.1			2511886
6	7/16/2013	9:25:50 00	Od 00:10.0	62.8	72.8	65.2	60.9		65.2	65.1	62.7	61.1	61			1905461
7	7/16/2013		0d 00:10.0	63.4	73.4	63.9	61.9	·.•	63.7	63.6	63.5	62.5	62.2			2187762
8	7/16/2013	9:26:10 00	od 00:10.0	63.5	73.5	64.1	63.1		64	64	63.4	63.2	63.2]	2238721
9	7/16/2013		0d 00:10.0	61.2	71.2	63,4	60	·	63.2	63.1	61.1	60.1	60.1			1318257
10	7/16/2013	9:26:30 00	0d 00:10.0	63.3	73.3	65.7	61		65.6	65.2	61.9	61.2	61.1			2137962
11	7/16/2013	9:26:40 00	0d 00:10.0	65.4	75.4	67	63.9		66.9	66.7	65.5	64.1	64			3467369
12	7/16/2013	9:26:50 00	0d 00:10.0	63.2	73.2	65.9	62.2	n,n	65.2	64.4	63.2	62.3	62.3			2089296
13	7/16/2013	9:27:00 00	od 00:10.0	61.6	71.6	64.6	58.3	•.•	64.5	64.4	61.9	58.6	58.6			1445440
14	7/16/2013	9:27:10 00	0.01:00 b0	61.3	71.3	62.5	58.3	•,-	62.4	62.4	61.3	58.5	58.4			1348963
15	7/16/2013	9:27:20 00	0d 00:10.0	60.3	70.3	61.8	59.6	·	61.4	61.1	60.5	59,9	59.8			1071519
16	7/16/2013	9:27:30 00	0d 00:10.0	61.6	71.6	64.2	59.6		63.2	62.7	60.4	59.8	59.7			1445440
17	7/16/2013	9:27:40 00	0d 00:10.0	66	76	66.9	64.2	-,-	66.9	66.7	65.7	65	65			3981072
18	7/16/2013	9:27:50 00	0d 00:10.0	64.8	74.8	66.3	63.5		66.2	66.1	64.8	63.7	63.6			301.9952
19	7/16/2013	9:28:00 00	0d 00:10.0	63.8	73,8	64.7	63		64.5	64.4	63.7	63.1	63			2398833
20	7/16/2013		od 00:10.0	62.6	72.6	64.7	61.4		64.5	64.4	62.4	61.4	61.4			1819701
21	7/16/2013	9:28:20 00	0d 00:10.0	63.1	73.1	63.6	61.5		63.5	63.5	63.2	62	61.8	****		2041738
22	7/16/2013	9:28:30 00	0d 00:10.0	61	71	62.6	59.5		62.4	62.1	61.4	60	59,7			1258925
23	7/16/2013	9:28:40 00	od 00:10.0	60.4	70.4	63.2	58.3	· · ·	62.7	62.2	59.2	58.5	58.4			1096478
24	7/16/2013	9:28:50 0	0d 00:10.0	64.3	74.3	64.9	63.2	····	64.8	64,8	64.3	63.5	63.5			2691535
25	7/16/2013		0d 00:10.0	63.5	73.5	63.9	63		63.9	63.8	63.5	63	63			2238721
26	7/16/2013		0d 00:10.0	63, 9	73.9	65	62,4	·····	64.9	64.8	63.7	62.6	62.5			2454709
27	7/16/2013		0d 00:10.0	67.3	77.3	69.1	64.3	·····	69	68.7	66.5	64.5	64.4			5370318
28	7/16/2013		0d 00:10.0	64.1	74.1	68.2	61.6	·····	67.5	67.4	63.9	61.9	61.8			2570396
29	7/16/2013	******	0d 00:10.0	61.6	71.6	62.5	60.3		62.4	62.3	61.7	60.6	60.5		•	1445440
30	7/16/2013		0d 00:10.0	57.6	67.6	60.3	\$6.5		59.8	59.5	57.3	56.7	56.6 57.8			1230269
31	7/16/2013		10d 00:10.0	60.9	70.9	61.8	57.2	¥	61.7	61.7	61.1	58.1 59.9				1202264
32	7/16/2013	*****************	00d 00:10.0	60.8	70.8	61.9	59.6		61.9	61.8	60.8 62.7	60.9	59.7 60.3			1905461
33	7/16/2013		od 00:10.0	62.8	72.8	64.1	59.6	· ›:	64	63.9	60.4	59.3	59.3			1023293
34	7/16/2013	*******	0d 00:10.0	60.1	70.1	61.9	59.2		61.6	61.2 60.9	59.7	59.1	59.1			1000000
35	7/16/2013		0d 00:10.0	60	70	61.4	59	·····	61.2 65.7	65.4	61.8	61.4	61.3			2238721
36	7/16/2013	*********************	0d 00:10.0	63.5 65.9	73.5 75.9	65.8 66.3	61.2 65.2		66.2	66.1	65.8	65.5	65.4			3890451
37	7/16/2013		00d 00:10.0			66.2	63.6		66	65.9	63.9	63.7	63.7		·	2630268
38	7/16/2013		00d 00:10.0	64.2 63.9	74.2 73.9	64.3	63.3	····	64.2	64.2	63.8	63.5	63.4			2454709
39	7/16/2013			61.4	71.4	63.8	60.1		63.4	63.2	61.8	60.5	60.2			1380384
40	7/16/2013		0d 00:10.0	58.6	68.6	60.3	57.5		60.2	60	58.8	58	57.8			724436
41 42	7/16/2013 7/16/2013		00d 00:10.0	58.9	68.9	62	56.4		61.6	60.9	57.1	56.6	56.5			776247.1
42	7/16/2013		od 00:10.0	64	74	64.9	62		64.8	64.7	63.5	63	62.5			2511886
45	7/16/2013	{	00d 00:10.0	65.2	75.2	65.7	64.8		65.6	65,6	65.2	64.9	64.9			3311311
45	7/16/2013	*******************	od 00:10.0	64.8	74.8	66.1	63.2		66	65.9	65.2	63.8	63.6			3019952
45	7/16/2013		00d 00:10.0	64.7	74.7	65.3	63.1		65.3	65.3	64.7	63.5	63.3			2951209
47	7/16/2013		00d 00:10.0	62.8	72.8	64.7	61.7		64.5	64.3	62.8	61.8	61.7	****		1905461
48	7/16/2013		00d 00:10.0	63.7	73.7	64.5	62.9		64.4	64.4	63.4	63.1	63			2344229
49	7/16/2013		00d 00:10.0	63.8	73.8	65.1	62.7	2.7	65.1	64.9	63.5	62.8	62.8			2398833
50	7/16/2013	*****	00d 00:10.0	62.5	72.5	65	61		64.7	64.7	62.3	61.2	61.2			1778279
51	7/16/2013		00d 00:10.0	59.4	69.4	61.2	57.4	-,-	61.2	61.1	59.5	57.6	57.5			870963.6
52	7/16/2013		00d 00:10.0	59.6	69.6	61.3	57.9		61.1	60.7	59	58	57.9			912010.8
53	7/16/2013		00d 00:10.0	61.4	71.4	61.9	60.2		61.9	61.9	61.5	60.7	60.5			1380384
54	7/16/2013		00d 00:10.0	63.6	73.6	66.1	59.8	-,-	66	65.9	62	60.1	59.9			2290868
55	7/16/2013		00d 00:10.0	64	74	66.4	60.9	<u>.</u>	66.3	66.1	64,7	61.6	61.4			2511886
56	7/16/2013		00d 00:10.0	59.9	69.9	61	59.2		60.7	60.6	60	59.3	59.2			977237.2
57	7/16/2013		00d 00:10.0	62.9	72.9	63.8	60.7		63.6	63.5	63.1	60.9	60.9			1949845
58	7/16/2013	**********************	00d 00:10.0	63.5	73.5	64.4	62.3		64.4	64.3	63.5	62.8	62.5			2238721
59	7/16/2013	9:34:40 C	00d 00:10.0	60.5	70.5	62.3	59.6		62.1	62	60.6	59.7	59.7			1122018
60	7/16/2013		00d 00:10.0	63.2	73.2	65.3	59.5	-,-	65.1	65	62.9	59.7	59.7			2089296

Add	iress	Start Time	Measur	ement Time	Leq	LE	LMAX	LMIN	Ly	LN1	LN2	LN3	LN4	LN5	Over	Under	Inverse Log	Ove Le
	14			······			1					70.5	60.6	CO 5	T	1	101077616	71
	1	7/16/2013	9:25:00	00d 00:10.0	73.4	83.4	77.6	69.4	<u> </u>	76.9	76.3	72.6	69.6	69.5	+		21877616	
	2	7/16/2013	9:25:10	00d 00:10.0	71.3	81.3	72.9	69.9	· · · · · · · · ·	72.8	72.7	70.7	70.1	70.1			13489629	
	3	7/16/2013	9:25:20	00d 00:10.0	73	83	75.4	69.3	· · · ·	75	74.8	73.3	70.3	69.6			19952623	
J	4	7/16/2013	9:25:30	00d 00:10.0	68.7	78.7	69.5	68		69.3	69	68.6	68.2	68,1			7413102	
ļ	5	7/16/2013	9 :25:40	00d 00:10.0	72.6	82.6	76.6	69.5		75.9	74.3	70.3	69.9	69.8			18197009	
	6	7/16/2013	9:25:50	00d 00:10.0	74.8	84.8	77.4	71.7	······	77.1	77	75,5	71.9	71.7			30199517	
ļ	?	7/16/2013	9:26:00	00d 00:10.0	68.3	78.3	72.6	65.7		72.2	72.1	67.4	66	65.9			6760830 12589254	
	8	7/16/2013	9:26:10	00d 00:10.0	71	81	74	67.1	·····	73.9	73.7	70.4	67.7	67.2			12589254	
	9	7/16/2013	9:26:20	00d 00:10.0	71	81	73.5	67.2	· · · · · · · · · · · · · · · · · · ·	73.4	73.2	70.4	67.7 70.8	67.6 70.5			16595869	
	.0	7/16/2013	9:26:30	00d 00:10.0	72.2	82.2	73.9	70.5		73.8	73.5	70.5	68.1	68			9549926	
	1	7/16/2013	9:26:40	00d 00:10.0	69.8	79.8	71.2	67.8 66.6		71.1 71.6	71.4	69.8	67	66.7			9120108	
	2	7/16/2013	9:26:50	00d 00:10.0	69.6 72.6	79.6	71.6			74.7	74.3	71.8	70	68,6			18197009	
· · · · · ·	.3	7/16/2013	9:27:00	*****	72.6 70.9	82.6 80.9	74.8	67.1 68.3		74.2	73.8	69.8	68.5	68.4			12302688	
	.4	7/16/2013 7/16/2013	9:27:10 9:27:20	00d 00:10.0 00d 00:10.0	70.9	80.9	72.8	68.6		72.7	72.4	70.6	69.3	69.3			12302688	
	5	7/16/2013	9:27:30	00d 00:10.0	67.2	77.2	68.6	65.9	·····	68.4	68.4	66.8	66.2	66.1			5248075	
******	.6	7/16/2013	9:27:40	00d 00:10.0	68.2	78.2	68.9	67.5		68.9	68.8	58.3	67.7	67.6			6606934	
	17 18	7/16/2013	9:27:50	00d 00:10.0	67.3	77.3	68.8	65.4	····	68.4	68.2	67.2	65.6	65.5			5370318	
F	19	7/16/2013	9:28:00	00d 00:10.0	73.7	83.7	76.1	68.8		76	75.9	72.9	69.4	69.3			23442288	
	20	7/16/2013	9:28:10	00d 00:10.0	74.1	84.1	76.8	72.8		76.7	76.5	73.5	73.1	73			25703958	1
	21	7/16/2013	9:28:20	00d 00:10.0	71.6	81.6	73.4	69.9	•	73.3	73	71	70.1	70			14454398	
	22	7/16/2013	9:28:30	00d 00:10.0	72.7	82.7	73.3	71.9	-,-	73.2	73.2	72.9	72.1	72			18620871	
	23	7/16/2013	9:28:40	00d 00:10.0	70.9	80.9	72	70		71.9	71.8	70.9	70.2	70.1			12302688	1
	24	7/16/2013	9:28:50	00d 00:10.0	67.5	77.5	70.9	65.5	~	70.4	70	67.6	65.8	65.7			5623413	
	25	7/16/2013	9:29:00	00d 00:10.0	68.1	78.1	69.7	65.4		69.5	69.2	68.3	65.8	65.6			6456542	
	26	7/16/2013	9:29:10	00d 00:10.0	71.6	81.6	73.6	68.4		73.4	73,4	71.2	68.7	68.7			14454398	
	27	7/16/2013	9:29:20	00d 00:10.0	67.5	77.5	72.2	65.6	~~	71.6	70.8	66.9	65.8	65.7			5623413	
	28	7/16/2013	9:29:30	00d 00:10.0	71.5	81.5	73.3	69.2		72.7	72.5	70.6	70	70			14125375	Į –
	29	7/16/2013	9:29:40	00d 00:10.0	73.4	83.4	75.5	70.9		75.2	74.8	72.8	71	71			21877616	
	30	7/16/2013	9:29:50	00d 00:10.0	75.4	85.4	79.4	69.9		79.1	78.5	75.3	71	70.3			34673685	
	31	7/16/2013	9:30:00	00d 00:10.0	67.5	77.5	69.9	66.3		69.8	69.4	67.5	66.6	66.4			5623413 9332543	
+	32	7/16/2013	9:30:10	00d 00:10.0	69.7	79.7	70.8	67.8	·	70.7	70.5	69.7	68.8	68.2 61.3			2290868	
******	33	7/16/2013	9:30:20	00d 00:10.0	63.6	73.6	69.4	61.2	·····	68.5 70.2	67.6 70.2	63.2 68.2	61.4 64	63,9			6606934	
} · · · · ·	34	7/16/2013	9:30:30	00d 00:10.0	68.2	78.2 79.9	70.3	63.5 cc c	·····	72,8	72.6	67.7	66.1	65.8			9772372	1
	35	7/16/2013	9:30:40	00d 00:10.0	69.9	79.9	72.9	65.6 67.8	·····	70.8	70.6	69.2	67.9	67.9			7585776	1
	36	7/16/2013	9:30:50 9:31:00	00d 00:10.0 00d 00:10.0	68.8 66.7	76.7	68.6	64.6		68.5	68.3	66.8	64.9	64.8			4677351	
	37	7/16/2013	9:31:10	00d 00:10.0	71.3	81.3	73.1	64.9		72.9	72.6	71.2	65.7	65.2			13489629	
	38 39	7/16/2013	9:31:20	00d 00:10.0	74.7	84.7	76.4	71.9		76.1	76	75.1	72.6	72.2			29512092	
	40	7/16/2013	9:31:30	00d 00:10.0	72.1	82.1	73.2	70.9		73.2	73.1	71.6	71	71			16218101	
	41	7/16/2013	9:31:40	00d 00:10.0	71	81	73.3	68.6		73.2	73.2	71.1	68.7	68.7			12589254]
	42	7/16/2013	9:31:50	00d 00:10.0	71	81	71.9	69.3	-,-	71.7	71.6	70.8	70.2	70.1			12589254	
	43	7/16/2013	9:32:00	00d 00:10.0	65.3	75.3	71.1	63.2		70.4	69.7	64.9	63.5	63.4			3388442	
h	44	7/16/2013	9:32:10	00d 00:10.0	64.1	74.1	66	61.5		65.9	65.8	64.1	61.8	61.6			2570396	
	45	7/16/2013	9:32:20	00d 00:10.0	72.9	82.9	76.1	65		76	75.7	73.1	66,1	65.5			19498446	
	46	7/16/2013	9:32:30	00d 00:10.0	73.8	83.8	74.6	72.6		74.4	74.3	74	72.8	72.7			23988329	4
******	47	7/16/2013	9:32:40	00d 00:10.0	73.8	83.8	76.5	71.2		76.3	76	73.5	71.5	71.3			23988329	4
	48	7/16/2013	9:32:50	00d 00:10.0	72.1	82.1	73.3	71.2		72.9	72.9	72.2	71.5	71.4			16218101	
	49	7/16/2013	9:33:00	00d 00:10.0	70	80	72.6	68.5		72.5	72.1	69.8	68.8	68.6		*****	10000000	1
h	50	7/16/2013	9:33:10	00d 00:10.0	71.8	81.8	73.1	70.1		73	72.9	71.3	70.6	70.6			15135612	
	51	7/16/2013	9 33:20	00d 00:10.0	71.6	81.6	73.3	70.1	·····	73.2	73.1	71.5	70,3	70.2			14454398	
	52	7/16/2013	9:33:30		70.9	80,9	73.6	67.6		73.5	73.3	70,9	67.8	67.7			6918310	
	53	7/16/2013	9:33:40		68.4	78.4	69.3	66.5		69.1	69,1	68.7	67.4	67.1			3090295	1
	54	7/16/2013	9:33:50		64.9	74.9	66.5	63,7		65.9	65.7	65 68 /	63.9	63.8			7079458	1
	55	7/16/2013	9:34:00		68,5	78.5	69,4	65.2		69.3	69.2 71	68.4 68.4	65.9 67.7	65.4 67.7			8511380	•
	56	7/16/2013	9:34:10		69,3	79,3	71.9	67.6		71.4	76	73.8	72.2	72.1			26302680	
	57	7/16/2013	9.34:20		74,2	84.2	76.5	71.8 68.9		71.6	71.4	70.3	69.7	69.4			10471285	-
	58	7/16/2013	9:34:30		70.2	80.2	71.8	68.7	·	71.1	71	70.2	68.8	68.8			10964782	-
1	59	7/16/2013	9:34:40	00d 00:10.0 00d 00:10.0	70.4	80.4	71.6	68.5		71.5	71.3	69.8	68.7	68.6			10000000	-

Address	Start Time	Measure	ement Time	Leq	LE	LMAX	LMIN	Ly	LN1	LN2	LN3	LN4	LNS	Over	Under	Inverse Log
R15																
1	7/16/2013	8:45:00	00d 00:10.0	71.4	81.4	72	70.7		71.9	71.8	71.4	70.8	70.8			13803843
2	7/16/2013	8:45:10	00d 00:10.0	75.2	85.2	76.2	71.5		76.1	76	75.3	72.1	71.7			33113112
	7/16/2013	8:45:20	00d 00:10.0	74.8	84.8	76.5	72.4		76.4	76.2	75	73.4	73			30199517
3	7/16/2013	8:45:30	00d 00:10.0	72.8	82.8	74.9	70.5		74.7	74.6	72	70.5	70.5			19054607
4	7/16/2013	8:45:40	00d 00:10.0	74.3	84.3	74.9	73.3		74.8	74.8	74.5	73.5	73,4			26915348
5			00d 00:10.0		82.1	74.1	71.4		73,9	73.6	72.3	71.5	71.4			15218101
6	7/16/2013	8:45:50		72.1		74.1		·····	74	73.9	72.9	71.2	70.8			18620871
7	7/16/2013	8:46:00	00d 00:10.0	72,7	82.7	72.1	70.5 70.1		72	71.9	71.6	70.5	70.3			13803843
8	7/16/2013	8:46:10	00d 00:10.0	71,4	81.4	***********	68.9		70.2		69.8	69.1	69			9332543
9	7/16/2013	8:46:20	00d 00:10.0	69.7	79.7	70.5		·····	72.7	70 72.4	71.6	70.7	70.7			15135612
10	7/16/2013	8:46:30	00d 00:10.0	71.8	81.8	73	70.5	·····				71.9	71.7			23988329
11	7/16/2013	8:46:40	00d 00:10.0	73.8	83.8	75.3	71.5		75.3	75.1	73.4	70.3	69.9			21379621
12	7/16/2013	8:46:50	00d 00:10.0	73.3	83.3	75.9	69.2	<u>-</u>	75.8	75.7	73.9	+				8912509
13	7/16/2013	8:47:00	00d 00:10.0	69.5	79.5	71.4	66.2		71.4	71.3	68.8	66.3	66.3			13803843
14	7/16/2013	8:47:10	00d 00:10.0	71.4	81.4	72.9	70.1		72.7	72.4	71.3	70.2	70.2			
15	7/16/2013	8:47:20	00d 00:10.0	76.1	86.1	77.3	72.1		77.2	77.1	76.1	74,2	73.7			40738028
16	7/16/2013	8:47:30	00d 00:10.0	74.8	84,8	76.6	73.7		76.5	76.3	74.2	73.9	73.8			30199517
17	7/16/2013	8:47:40	00d 00:10.0	72	82	74.2	69.6		73.7	73.6	72.4	69.8	69.8			15848932
18	7/16/2013	8:47:50	00d 00:10.0	71.6	81.6	74.2	68.8		74.1	73.9	70.8	68.9	68.9			14454398
19	7/16/2013	8:48:00	00d 00:10.0	69.9	79.9	73.9	67.5	·.	73.5	73.1	70	67.8	67.6			9772372
20	7/16/2013	8;48:10	00d 00:10.0	71.8	81.8	73	70.7	.	73	72.9	71.5	70.9	70.8			15135612
21	7/16/2013	8:48:20	00d 00:10.0	73.4	83.4	74.4	71.1		74.3	74.3	73,5	71.8	71.5			21877616
22	7/16/2013	8:48:30	00d 00:10.0	72.2	82.2	74.1	70.9	·····	74	73.6	71.9	71	71			16595869
23	7/16/2013	8:48:40	00d 00:10.0	68.4	78.4	71.4	66.1		71.2	70.9	68.3	66.2	66.1		*****	6918310
24	7/16/2013	8:48:50	00d 00:10.0	68.2	78.2	69.4	67.1		69.3	69.2	68.2	67.3	67.2			6606934
25	7/16/2013	8:49:00	00d 00:10.0	72.7	82.7	74.6	68.3		74.5	74.5	72.2	68.6	68.4		ļ	18620871
26	7/16/2013	8:49:10	00d 00:10.0	75.7	85.7	76.1	72.5		75.9	75.8	75.7	74.7	73.6			37153523
27	7/16/2013	8:49:20	00d 00:10.0	72.6	82.6	75.6	70.3		75,3	74.9	72.7	70.6	70.5			18197009
28	7/16/2013	8:49:30	00d 00:10.0	73	83	75.6	69.8		75.5	75	72.9	70.1	69.9			19952623
29	7/16/2013	8:49:40	00d 00:10.0	73.4	83.4	76.1	70.6		76	76	73	70.8	70.7			21877616
30	7/16/2013	8:49:50	00d 00:10.0	74.5	84.5	77.2	68.2		77.1	76.9	74.8	69.9	69			28183829
31	7/16/2013	8:50:00	00d 00:10.0	71.3	81.3	74.4	66		74.2	74	68.6	66.1	66			13489629
32	7/16/2013	8:50:10	00d 00:10.0	74.1	84.1	75.6	72.3	·	75.4	75	74.2	73.4	72.9			25703958
33	7/16/2013	8:50:20	00d 00:10.0	74.1	84.1	76.2	70.7		76.1	76	73.8	70.8	70.8			25703958
34	7/16/2013	8:50:30	00d 00:10.0	75.1	85.1	77.4	71.5	-,-	77.3	77.2	74.8	71.9	71.7			32359366
35	7/16/2013	8:50:4D	00d 00:10.0	71.1	81.1	74.2	67	-,-	73,5	73	72.5	67,5	67.2			12882496
36	7/16/2013	8:50:50	00d 00:10.0	71.9	81.9	75.3	67.1		74.9	74.3	69.9	67.7	67.2			15488166
37	7/16/2013	8:51:00	00d 00:10.0	74	84	77.7	70.3		77.4	77.2	72.7	70.5	70.4			25118864
38	7/16/2013	8:51:10	00d 00:10.0	71	81	73.6	58.1		73.6	73.3	70.9	68.2	68.1			12589254
39	7/16/2013	8:51:20	00d 00:10.0	71.4	81.4	73.1	68.1		72.9	72.8	70.7	68.5	68.2			13803843
40	7/16/2013	8:51:30	00d 00:10.0	69.9	79.9	72.7	69		72.6	72.1	69.5	69.2	69.1			9772372
41	7/16/2013	8:51:40	00d 00:10.0	71.2	81.2	72.6	68.8		72.6	72.5	71.1	68.9	68.8			13182567
42	7/16/2013	8:51:50	00d 00:10.0	71.6	81.6	73	69.2	-,-	72.9	72.5	71.6	69.4	69.3			14454398
43	7/16/2013	8:52:00	00d 00:10.0	72.2	82.2	73.2	71.1		73.1	73	72.5	71.2	71.1			16595869
44	7/16/2013	8:52:10	00d 00:10.0	70.1	80.1	71.9	68.9		71,8	71.7	69.9	69.1	69			10232930
45	7/16/2013	8:52:20	00d 00:10.0	75.1	85.1	76.8	69.1		76.8	76.B	74.9	69.4	69.2			32359366
45	7/16/2013	8:52:30	00d 00:10.0	73,6	83.6	75.9	72.6		75.5	75.1	73.7	72.9	72.8			22908677
47	7/16/2013	8:52:40	00d 00:10.0	70.6	80.6	73.7	69.9		73.1	72.6	70.4	70.1	70			11481536
48	7/16/2013	8:52:50	00d 00:10.0	67.8	77.8	70.2	63.8		69.8	69.8	68.9	64.8	64.2			6025596
40	7/16/2013	8:53:00	00d 00:10.0	70.7	80.7	73.3	63.7		73.2	73.1	70.8	64.5	64			11748976
50	7/16/2013	8:53:10	00d 00:10.0	71.8	81.8	72.8	70.7		72.7	72.7	71.9	70.9	70.8			15135612
50	7/16/2013	8:53:20	00d 00:10.0	70.2	80.2	72.3	69.2		71.7	70.9	69.7	69.2	69.2			10471285
		8:53:30	00d 00:10.0	72.5	82.5	73,3	71.6		73.2	73.1	72.6	71.8	71.7			17782794
52	7/16/2013		00d 00:10.0	74.7	84.7	76	72.2		75.9	75.9	74.4	72.6	72.5			29512092
53	7/16/2013	8:53:40		***********			71		74.2	73.6	72.1	71.1	71.1			15488166
54	7/16/2013	8:53:50	00d 00:10.0	71.9	81.9	74.5			76	76	74.1	70.9	70.8			26302680
55	7/16/2013	8:54:00	00d 00:10.0	***********	84.2	76.1	70.7 67.4		74.7	74.1	70.3	67.6	67.5			10964782
56	7/16/2013	8:54:10	00d 00:10.0	70.4	80.4	75.3	67.4			74.1	72.1	70.2	69.8			18197009
57	7/16/2013	8:54:20	00d 00:10.0	72.6	82.6	74.4	69.2		74.3		69.9	67.3	67.2			11481536
58	7/16/2013	8:54:30	00d 00:10.0	***********	80.6	73.7	67.1	· · · · · · · · · · · · · · · · · · ·	73.5	72.8		71.4	71.2	•••		16982437
59	7/16/2013	8:54:40	00d 00:10.0	72.3	82.3	73.8	71.1	· · ·	73.6	73.4	72.4	1				16218101

Address	Start Time	Measurement Time	Leq	LE	LMAX	LMIN	Ly	LN1	LN2	LN3	LN4	LNS	Over	Under	Inverse Log
R16															
1	7/16/2013	8:45:00 00d 00:10.0	56,4	66.4	57.1	54.4		57	56.7	56.4	54.8	54.5			436515.8
.	7/16/2013	8:45:10 00d 00:10.0		65.8	57	55.4		56.7	56.3	55.9	55.5	55.5			380189.4
2			+	+	***** *******************************				55,4	54.6	54.3	54.2			295120.9
3	7/16/2013	8:45:20 00d 00:10.0	54.7	64.7	55.8	54.1		55.5	56.6	56.1	55.3	55.3	t		416869.4
4	7/16/2013	8:45:30 00d 00:10.0	56.2	66.2	57.1	55.2	·····	57			+	57.4			707945.8
5	7/16/2013	8:45:40 00d 00:10.0	58.5	68.5	59.1	57.1	····· ···	59	59	58.3	57.5			- {	
6	7/16/2013	8:45:50 00d 00:10.0	57.8	67.8	59.4	55.9		59.2	59.1	57.8	56.3	56.1			602559.6
7	7/16/2013	8:46:00 00d 00:10.0	57.1	67.1	58.4	55.7		58.4	58.2	56.8	56,1	56.1			512861.4
8	7/16/2013	8:46:10 00d 00:10.0	56.6	66.6	57.2	56.2		\$7	57	56.6	56.3	56.3			457088.2
9	7/16/2013	8:45:20 00d 00:10.0	54.1	64.1	56.4	53.1		56	55.9	54.1	53.2	53.1			257039.6
10	7/16/2013	8:46:30 00d 00:10.0	54.4	64.4	55.4	52.8		55.3	55,3	54.6	53.1	52.9			275422.9
11	7/16/2013	8:46:40 00d 00:10.0	52	62	52.9	51.3		52.8	52.8	52	51.4	51.4			158489.3
12	7/16/2013	8:46:50 00d 00:10.0	53.2	63.2	53.6	52.3	····	53.6	53.5	53.2	52.5	52.5	<u> </u>		208929.6
13	7/16/2013	8:47:00 00d 00:10.0	55.6	65.6	56.5	53.3		56.5	56.4	55.6	53.7	53.4			363078.1
14	7/16/2013	8:47:10 00d 00:10.0	56.5	66.5	57	54.9	~2	56.9	56.9	56.6	55.5	55.5			446683.6
15	7/16/2013	8:47:20 00d 00:10.0		65.1	56.3	54.3		56.2	56.2	55.1	54.5	54.5			323593.7
16	7/16/2013	8:47:30 00d 00:10.0	*****	66.3	57	54.6	-,-	56,9	56.9	56.3	55,2	54.9			426579.5
17	7/16/2013	8:47:40 00d 00:10.0		65.9	56.4	\$5.7		56.3	56,3	55.9	55.8	55.8	[389045.1
18	7/16/2013	8:47:50 00d 00:10.0	************	71.2	65.1	55.8		65,1	64.9	56.6	56	55.9	[1318257
19	7/16/2013	8:48:00 00d 00:10.0	56.2	66.2	63.5	55.2		62.1	60.8	56.1	55.4	55.3	<u> </u>]	416869.4
20	7/16/2013	8:48:10 00d 00:10.0	57.9	67.9	59.7	56.2		59.1	58.9	57.3	56.4	56.3		<u>]</u>	616595
21	7/16/2013	8:48:20 00d 00:10.0	67.9	77.9	71	59.7	·	70.9	70.8	67.1	62.1	60.9			6165950
22	7/16/2013	8:48:30 00d 00:10.0	56.8	66.8	63	56.2	-,-	61.5	60.2	57.1	56.7	56.5			478630.1
23	7/16/2013	8:48:40 00d 00:10.0		64.7	56.2	54	••	56.1	55.9	54.8	54.2	54.2			295120.9
24	7/16/2013	8:48:50 00d 00:10.0	• • • • • • • • • • • • • • • • • • • •	63.8	54.8	53.3	-,-	54.7	54.5	53.7	53.4	53.3			239883.3
25	7/16/2013	8:49:00 00d 00:10.0	*****	63.9	54.4	53		54.4	54.4	53.8	53.6	53.4			245470.9
26	7/16/2013	8:49:10 00d 00:10.0		63	53.8	52.3		53.5	53.4	52.8	52.4	52.3			199526.2
27	7/16/2013	8:49:20 00d 00:10.0	*******	65.8	56.9	53.8		56.8	56.8	55.4	53.9	53.9		· · · · · ·	380189.4
	7/16/2013	8:49:30 00d 00:10.0	**********	67	57.5	56.6		57.5	57.4	57	56.7	56.6	*		501187.2
28	7/16/2013	8:49:40 00d 00:10.0		67.4	57.8	56.5		57.7	57.7	57.5	56.8	56.6			549540.9
30	7/16/2013	8:49:50 00d 00:10.0		66.1	57.5	55.3		57.4	57.4	56	55.5	55.4			407380.3
31	7/16/2013	8:50:00 00d 00:10.0		66.4	57	55.5		56.9	56.8	56.4	55.6	55.6			436515.8
32	7/16/2013	8:50:10 00d 00:10.0		67.1	58	56		58	57,9	56.8	56.1	56.1			512861.4
				66.8	57.9	56.1		57.8	57.7	56.9	56.2	56.2			478630.1
33	7/16/2013			66.8	57.2	56.3		57.1	57	56.8	56.4	56.4			478630.1
34	7/16/2013	8:50:30 00d 00:10.0		+	***********	56.5		57.2	57.1	57	56.7	56.7			489778.8
35	7/16/2013	8:50:40 00d 00:10.0	************	66.9	57.2			56.8	56.8	55.8	55.6	55.5			389045.1
36	7/16/2013	8:50:50 00d 00:10.0	+	65.9	56.9	55.5		57.3		56.7	56.2	56.1			467735.1
37	7/16/2013	8:51:00 00d 00:10.0	**********	66.7	57.4	55.7			57.2	54.2	53.8	53.8			269153.5
38	7/16/2013	8:51:10 00d 00:10.0	+	64.3	56.1	53.7		55.7	55.4 rc	55.7	54,2	54.1			354813.4
39	7/16/2013	8:51:20 00d 00:10.0		65.5	56.1	54		56	56				. .		288403.2
40	7/16/2013	8:51:30 00d 00:10.0		64.6	55.8	53.9		55.6	55.5	54.5	54.1	54			323593.7
41	7/16/2013	8:51:40 00d 00:10.0		65.1	58.7	53	······	58.2	57.6	53.9	53.3	53.2			549540.9
42	7/16/2013	8:51:50 00d 00:10.0	*****	67.4	59	54.6	· · · · · ·	58.8	58.7	57.2	54.9	54.8	• • • • • • • • • • • • • • • • • • • •	{	537031.8
43	7/16/2013	8:52:00 00d 00:10.0		67.3	59.5	55.2		59.2	59	56.8	55.5	55.3			
44	7/16/2013	8:52:10 00d 00:10.0		65.3	59	54.3	·	58.5	58	54.9	54.5	54.4			338844.2
45	7/16/2013	8:52:20 00d 00:10.0		65.3	56.1	54.3		56	55.6	55.3	54,4	54.4	· • • · • • • • • • • • • • • • • • • •		
46	7/16/2013	8:52:30 00d 00:10.0		67.3	58.1	55.9		57.9	57.9	57.2	56	56			537031.8
47	7/16/2013	8:52:40 00d 00:10.0		67.1	57.9	55.9		57.8	57.7	57.4	56.3	56.1			512861.4
48	7/16/2013	8:52:50 00d 00:10.0		66	56.5	55.6		56.4	56.3	56	55.7	55.6			398107.2
49	7/16/2013	8:53:00 00d 00:10.0		67.1	58.6	55.4		58.4	58.3	57	55.6	55.5			512861.4
50	7/16/2013	8:53:10 00d 00:10.0	+	69	62.3	54,9		61.9	61.5	57.3	55.1	55	· · · · · · · · · · · · · · · · · · ·		794328.2
51	7/16/2013	8:53:20 00d 00:10.0		68.4	62.6	54.7		62.2	61.7	58.1	55.5	55.1			691831
52	7/16/2013	8:53:30 00d 00:10.0		67.9	60.6	54.7	· · ·	60.2	60	57	55.1	54.8			616595
53	7/16/2013	8:53:40 00d 00:10.0		68	61.2	55.4		60.9	60.4	56.9	55.4	55.4			630957.3
54	7/16/2013	8:53:50 00d 00:10.0	59.8	69.8	62.6	56.9		62.4	61.8	59.6	57.8	57.3			954992.6
55	7/16/2013	8:54:00 00d 00:10.0	58	68	60.8	54.9		60.5	60.2	57.1	55.3	55.1			630957.3
56	7/16/2013	8:54:10 00d 00:10.0	57.8	67.8	60.8	55.1]	60.5	60	57.2	55.4	55.2			602559.6
57	7/16/2013	8:54:20 00d 00:10.0		69.1	61.1	56.2		60.9	60.7	59	56.4	56.3			812830.5
58	7/16/2013	8:54:30 00d 00:10.0		71.6	64.8	56.3		64.8	64.2	61	58	57.1			1445440
59	7/16/2013	8:54:40 00d 00:10.0	58.2	68.2	60.6	55.6		60.3	60	57.8	55.7	55.6			660693.4
60	7/16/2013	8:54:50 00d 00:10.0		68.1	61.4	54.2		61.2	60.7	58.3	54.6	54.3			645654.2

Addre	is Start Time	Measure	ement Time	Leq	LE	LMAX	LMIN	Ly	LN1	LN2	LN3	LN4	LN5	Over	Under	Inverse Log
R17																
1	7/16/2013	8:45:00	00d 00:10.0	59.7	69.7	62.4	55.4	-,-	61.9	61.8	58.4	55.9	55.6			933254.3
2	7/16/2013	8:45:10	00d 00:10.0	58.6	68.6	63	55.9		62.8	62.4	58.4	56	56		····	724436
3	7/16/2013	8:45:20	00d 00:10.0	57.1	67.1	58.2	55.7	-,-	58	57.9	56.6	55.9	55.9			512861.4
4	7/16/2013	8:45:30	00d 00:10.0	58.3	68.3	59	57.7		59	58.9	58	57.8	57.8			676083
5	7/16/2013	8:45:40	00d 00:10.0	63	73	64.2	59		64.1	64.1	62.6	60.2	59,5			1995262
6	7/16/2013	8:45:50	00d 00:10.0	61	71	63.6	58.4		63.3	63.1	61.5	59.3	58.9			1258925
7	7/16/2013	8:46:00	00d 00:10.0	56,4	66.4	58.4	55.2		58	57.8	56.3	55,3	55.2			436515.8
8	7/16/2013	8:46:10	00d 00:10.0	61	71	62.3	58.1		62.2	62.1	60.8	58.8	58.5]	1258925
9	7/16/2013	8:46:20	0.01:00 b00	56.9	66.9	60.3	55.3		60	59.6	57	55.4	55.3			489778.8
10	7/16/2013	8:46:30	00d 00:10.0	55.6	65.6	56.2	55.1		56.1	56	55.4	55.2	55.1]	363078.1
11	7/16/2013	8:46:40	00d 00:10.0	55	65	56.7	53.3	-,-	56.6	56.6	55.1	53.3	53.3			316227.8
12	7/16/2013	8:46:50	00d 00:10.0	55.5	65.5	56.4	53.6	~	56.3	56.2	55.3	54.2	53.9	+		354813.4
13	7/16/2013	8:47:00	00d 00:10.0	58.8	68.8	60.5	56		60.5	60.4	58	56.3	56.1		*	758577.6
14	7/16/2013	8:47:10	00d 00;10.0	59.9	69.9	61.2	58.8	-7	61	60.8	59.3	59	58.9			977237.2
15	7/16/2013	8:47:20	00d 00:10.0	59.9	69.9	61.7	58.3	••	61.7	61.5	60	58.5	58.4			977237.2
16	7/16/2013	8:47:30	00d 00:10.0	60.7	70.7	62	58,2	··· ··	61.8	61.7	60.8	58,9	58.7			1174898
17	7/16/2013	8:47:40	00d 00:10.0	57	67	58.7	55.7	·	58.4	58.1	56.6	55.8	55.7			501187.2
18	7/16/2013	8:47:50	00d 00:10.0	60.2	70.2	61.4	58.7	<u>,,</u>	61.3	61.2	60	59,3	59			1047129
19	7/16/2013	8:48:00	00d 00:10.0	60.5	70.5	62	58.5	· · ·	61.8	61.6	60.4	58.8	58.6			1122018
20	7/16/2013	8:48:10	00d 00:10.0	60	70	61	59.1		60.9	60.8	60	59.2	59.2			1000000
21	7/16/2013	8:48:20	00d 00:10.0	58.5	68.5	59.6	57.7		59.5	59.4	58.4	57.8	57.8	****		707945.8
22	7/16/2013	8:48:30	00d 00:10.0	58.3	68.3	59.9	57.3		59.8	59.6	58.3	57.6	57.4			676083
23	7/16/2013	8:48:40	00d 00:10.0	58	68	58.4	57.3	- ~	58.3	58.3	58	57.6	57.4			630957.3
24	7/16/2013	8 48:50	00d 00:10.0	57.1	67.1	58.5	\$5.8		58.3	58.2	57.2	56.3	56			512861.4
25	7/16/2013	8:49:00	00d 00:10.0	57.5	67.5	58.5	55.6	····	58.4	58.3	57.6	55.9	55.7			562341.3
26	7/16/2013	8:49:10	00d 00:10.0	55,3	65.3	56.6	54		56.4	56.3	55.3	54.2	54.1			338844.2
27	7/16/2013	8:49:20	00d 00:10.0	57.5	67.5	58.3	56.3	·	58.2	58.1	57.4	56.5	56.4			562341.3
28	7/16/2013	8:49:30	00d 00:10.0	59,9	69.9	60.5	58.2		60.5	60.4	59.9	58.5	58.4			977237.2
29	7/16/2013	8:49:40	00d 00:10.0	61.5	71.5	62.4	60.3		62.3	62.1	61.1	60.5	60.5			1412538
30	7/16/2013	8:49:50	00d 00:10.0	60.3	70.3	62.5	59.3		62.4	62.2	60.1	59.4	59.3			1071519
31	7/16/2013	8:50:00	00d 00:10.0	58.8	68.8	59.9	57.8	ļ	59.8	59.8	58.6	58	57.9			758577.6
32	7/16/2013	8:50:10	00d 00:10.0	60	70	61.3	58.9		61.2	61.1	59.7	59	59			1380384
33	7/16/2013	8:50:20	00d 00:10.0	61.4	71.4	62.9	58.4	<u>-</u>	62.8	62.8	61.7	59.4	58.7 57.7	+		812830.5
34	7/16/2013	8:50:30	00d 00:10.0	59.1	69.1	60.6	57.7		60.5	60.4	58.8	57.8	59			1230269
35	7/16/2013	8:50:40	00d 00:10.0	60.9	70.9	61.8	58.9		61.7 59.7	61.6 59.5	61.3 58.2	59.4 57.6	57.5		·	707945.8
36	7/16/2013	8:50:50	00d 00:10.0	58,5	68.5	59.7	57.4		61.9	61.8	59.8	59,4	59.4			1122018
37	7/16/2013	8:51:00	00d 00:10.0	60.5	70.5	62	59.3		60.3	59.9	57.8	56.6	56.6			575439.9
38	7/16/2013	8:51:10	00d 00:10.0		67.6	60.8	56.5		58.7	58.2	56.9	56.4	56.4			575439.9
39	7/16/2013	8:51:20	00d 00:10.0		67.6 68.5	59.3 59.7	56.3		59.6	59.6	58.4	57.8	57.7			707945.8
40	7/16/2013	8:51:30 8:51:40	00d 00:10.0 00d 00:10.0		64.9	57.7	57.5 53.3		57.2	56.8	54.7	53,6	53.4			309029.5
41	7/16/2013	8:51:50	00d 00:10.0	+	66.7	57.4	54.4		57.3	57.3	56.9	54.8	54.6			467735.1
42	7/16/2013	8:52:00	00d 00:10.0	+	67.4	58.1	56.5		58	57.8	57.4	56.6	56.6			549540.9
43	7/16/2013	8:52:00	00d 00:10.0		67	58.2	56.2		58.1	57.7	57.1	56.4	56.4			501187.2
44 45	7/16/2013	8:52:20	00d 00:10.0	+	68.3	59.6	56		59.5	59.5	58.5	56.1	56			676083
*******	7/16/2013	8:52:30	00d 00:10.0	***********	71.6	62.7	59.6		62.6	62.5	61.7	60.1	59.9			1445440
46	7/16/2013	8:52:40	00d 00:10.0		69	61.2	57.5		60.8	60.5	59.2	58.4	58			794328.2
47	7/16/2013	8:52:50	00d 00:10.0		67.1	58.8	56.1		58.5	58	56.6	56.2	56.1			512861.4
49	7/16/2013	8:53:00	00d 00;10.0	·•	68.2	59.8	55.7		59.8	59.6	58.9	55.8	55.8			660693.4
50	7/16/2013	8:53:10	00d 00:10.0		67.9	58,4	55.8		58.3	58.3	58.1	56.3	56			616595
51	7/16/2013	8:53:20	00d 00:10.0		66.2	57.5	55.7		57.2	56.9	56.2	55.8	55.8			416869.4
52	7/16/2013	8:53:30		*******	70	62	55.8		62	61.9	59.6	55.9	55.9			1000000
53	7/16/2013	8:53:40		+	69.6	61.1	58.2	···	60.9	60.8	60.1	58,6	58.3			912010.8
54		8:53:50			67.8	59.1	56.6		59	58.6	57.6	56.7	56.7			602559.6
55					68.4	59.6	57.5		59.5	59.4	58.5	57.7	57.6			691831
56	7/16/2013	8:54:10			68.1	58.5	57.6		58.4	58.4	58.2	57.8	57.8			645654.2
57					68	58.5	57.2		58.3	58.3	58	57.3	57.3			630957.3
58	7/16/2013			***********	69.9	61.1	58.5		61	60.9	59.7	58.7	58.7			977237.2
59	7/16/2013				67.5	59.9	56.6		59.6	59.2	57.2	56.7	56.7			562341.3
60	7/16/2013				69.2	61	57.1		60.9	60.6	58.6	57.6	57.5			831763.8

Addre	ss Start Time	Measurement Time	Leq	LE	LMAX	LMIN	Ly	LN1	LN2	LN3	LN4	LN5	Over	Under	Inverse Log	Overa Leq
R18																70.0
1	7/16/2013	8:10:00 00d 00:10	.0 68.1	78.1	70	67.3	-,-	69	68.8	68.2	67.6	67.4			6456542	
2	7/16/2013	8:10:10 00d 00:10	0.0 70.7	80.7	73.8	67.7	·	73.7	73.2	69.6	67.9	67. 7			11748976	
3	7/16/2013	8:10:20 00d 00:10	0.0 73.9	83.9	76.9	70.4		76.8	76.8	71.4	70.6	70.5			24547089	
4	7/16/2013	8:10:30 00d 00:10	0.0 72.9	82.9	76.9	69.8	-,-	76.6	75.8	73	70	69.9			19498446	
5	7/16/2013	8:10:40 00d 00:10	.0 68.9	78.9	74.6	67.1	-,-	74.1	73.4	68.4	67.3	67.2			7762471	
6	7/16/2013	8:10:50 00d 00:1	0.0 70.4	80.4	72.1	67.3		72.1	72	69.9	67.7	67.5			10964782	
7	7/16/2013	8:11:00 00d 00:1	0.0 68.2	78.2	71.9	65.1		71.6	71.1	68.4	66.4	66.2			6606934	
8	7/16/2013	8:11:10 00d 00:1		78.8	72.5	63.4	· · · ·	72.3	72	68.6	63.7	63.5	~~		7585776	
9	7/16/2013	8:11:20 00d 00:1	0.0 70.9	80.9	73	66.2		73	72.9	70.9	66.7	66.6			12302688	
10	7/16/2013	8:11:30 00d 00:1	0.0 72	82	74.5	70.3	·	74.3	74	71	70.6	70.5			15848932	
11	7/16/2013	8:11:40 00d 00:1		76.3	72.7	64		71.7	70.6	66.4	64.3	64.2			4265795	
12	7/16/2015	8:11:50 00d 00:1	0.0 65.7	75.7	69.1	62.4		68.5	67.2	65	62.6	62.6			3715352	
13	7/16/2013	8:12:00 00d 00:1	0.0 73	83	75.7	69.1	-,-	75.3	75	72.4	70.3	69.7	····		19952623	
14	7/16/2013	8:12:10 00d 00:1		81.5	73.7	67	~~	73.6	73.5	70.4	67.5	67.2			14125375	
15	7/16/2013	8:12:20 00d 00:1		80.7	73.9	65.4	×	73.9	73.6	69.8	65.7	65.5			11748976	
16	7/15/2013	8:12:30 00d 00:1	0.0 68.8	78.8	73.1	65.4	····	72.8	72.6	67	65.7	65.5			7585776	
17	7/16/2013	8:12:40 00d 00:1		81.4	73.5	65.9		73.4	73.2	70.9	67.8	67			13803843	
18	7/16/2013	8:12:50 00d 00:1		78.3	71.8	65.9		71.1	70.7	67.6	66.2	66			6760830	
19	7/16/2013	8:13:00 00d 00:1	0.0 71.8	81.8	74.7	69.2		74.6	74.2	71.4	70	69.4			15135612	
20	7/16/201	8:13:10 00d 00:1	0.0 72.9	82.9	75.8	69	· · · · · · · · · · · · · · · · · · ·	75.6	75.4	72.4	69.3	69.1			19498446	
21	7/16/2013	8:13:20 00d 00:1	0.0 72.1	82.1	75	66.8	·.•	74.9	74.8	71.4	67.1	67			16218101	
22	7/16/201	8:13:30 00d 00:1	0.0 69.1	79.1	71.8	66.4	•.•	71.6	71.5	68.7	66.8	66.6			8128305	
23	7/16/2013	8:13:40 00d 00:1	0.0 71	81	72.4	68.9		72.4	72.3	71.1	69.3	68.9			12589254	
24	7/16/201	8:13:50 00d 00:1		81.1	72.1	69.5	<u></u>	72	71.9	70.7	70.1	69.7			12882496	
25	7/16/2013	8:14:00 00d 00:1	0.0 70	80	72.6	65.9		72	71.5	70	66.6	66.1		·	10000000	
26	7/16/201	8:14:10 00d 00:1	0.0 69.4	79.4	73.6	63.1	-,-	73.5	73.3	68.7	64.1	63.5			8709636	
27	7/16/2013	8:14:20 00d 00:1	0.0 66.7	76.7	69.1	61.9		69.1	68,8	65.7	62.3	62			4677351	
28	7/16/2013	8:14:30 00d 00:1	0.0 71.2	81.2	73.8	68.3	-,-	73.7	73.5	69.9	68.5	68.4			13182567	
29	7/16/201	8:14:40 00d 00:1	0.0 71	81	73.8	68.7	·	73.4	73	71.2	68.9	68.8			12589254	
30	7/16/2013	8:14:50 00d 00:1	0.0 67.3	77.3	71.4	62.4		71.3	71.1	65.9	62.7	62.6			5370318	
31	7/16/201	8:15:00 00d 00:1	0.0 72.1	82.1	73.8	68.6		73.6	73.5	71.7	70.6	70.3			16218101	
32	7/16/201	8:15:10 00d 00:1	0.0 68.5	78.5	70.7	66.6		70.6	70.5	68.3	66.9	66.7			7079458	
33	7/16/201	8:15:20 00d 00:1	0.0 69.5	79.5	71.8	66.3	<u>~</u>	71.7	71.5	69.1	66.4	66.4			8912509	
34	7/15/201	8:15:30 00d 00:1	0.0 71.6	81.6	73.5	67	<u></u>	73.3	73	71.8	67.3	67.2			14454398	
35	7/16/201	8:15:40 00d 00:1	0.0 69.4	79.4	73.2	66.3		72.3	70.6	68.9	66.6	66.5			8709636	1
36	7/16/201	8:15:50 00d 00:1	0.0 71.6	81.6	74	69.8		73.8	73.4	71,5	70.2	70			14454398	
37	7/16/201	8:16:00 00d 00:1	0.0 70.7	80.7	73.1	66.2		73	72.9	70.9	67.3	66.7			11748976	
38	7/16/201			81.3	73.5	65.1	·	73.3	73.2	71.4	66.4	66.1			13489629	1
39	7/16/201	8:16:20 00d 00:1	0.0 70.5	80.5	73.2	68.3		73.1	72.8	70	68.6	68.4			11220185	1
40	7/16/201	8:16:30 00d 00:1	0.0 66.8	76.8	69.6	63.2	· · · · · ·	68.7	68.5	67.3	63.7	63.3			4786301	
41	7/16/201			81.7	73.5	68.6		73.4	73.3	71.2	68.9	68.7			14791084	ł
42	7/16/201			78.3	72.3	66		72.2	71.6	68	66.4	66.2			6760830	
43	7/16/201			83.7	74.7	66.3		74.6	74.5		69.2	67.5			23442288	
44	7/16/201			80.9	73.3	69.5	·	73.2	73.1	71	69.6	69.6			4073803	1
45	7/16/201	*********	******	76.1	70.6	63.6		69.8	69.6	65.7	63.9	63.7				
46	7/16/201	***************************************		79	72.8	62.8	· · · · · · · · · · · · · · · · · · ·	72.7	72.4	68.1	63,9	63.4			7943282	1
47	7/16/201			79.5	72.4	61.8		72.3	72.1	69.2	62.1	61.9			8912509 5754399	
48	7/16/201		*****************	77.6	69.8	64.2		69.7	69.6	66.7	64.4	64.3 70			17378008	
49	7/16/201			82.4	74.2	69.7	· · · · · · · · · · · · · · · · · · ·	74.1	73.9	72	70.2			•• {-•••	11481536	
50	7/16/201			80.6		65.7	·	73.9	73.7	70.1	66.5	66.1			5248075	1
51	7/16/201			77.2		65.7		67.9	67.8	67.4	66.2	65 3				1
52	7/16/201			77.9	69	65.2		68.8	68.7	67.9	65.4	65.3			16982437	
53	7/16/201			82.3	74	68.5		74	74	71.9	68.8	68.7			9772372	-
54	7/16/201			79.9	73.3	67.4		72.8	72.7	69.2	67.6	67.5			17378008	
55				82.4	. 74	69.6		73.9	73.9	72.3	70,1	69.8			1380384	-
56				81.4	73.1	69.1		73.1	73.1	71.3	69.9	69.8			8709636	••
57	7/16/201			79.4	71.3	67.7		71.2	71.1	68.8	68	67.8			8709536	-6
58			****	79.5	73.6	63.4		73.5	73.2	66.1	63.9	63.6				-
59	7/16/201			83.1	75.5	70.2		75.4	75.2	72.4	70.5	70.3			20417379	-
60	7/16/201	3 8:19:50 00d 00:	0.0 71.7	81.7	74.5	68.7		74.4	74.1	71.9	69.2	68.9			14791084	*

Address	Start Time	Measur	ement Time	Leq	LE	LMAX	LMIN	Ly	LN1	LN2	LN3	LN4	LN5	Over	Under	Inverse Log
R19															.	
1	7/16/2013	8:10:00	00d 00:10.0	73.4	83.4	75.9	71.4	-,-	75.7	75.6	72.6	71.6	71.5			21877616
2	7/16/2013	8:10:10	00d 00:10.0	68.8	78.8	72.4	67	·	72.3	72.1	68.3	67.1	67.1			7585776
3	7/16/2013	8:10:20	00d 00:10.0	69.2	79.2	71.1	65.7		71	70.8	69	66	65,8			8317638
4	7/16/2013	8:10:30	00d 00:10.0	70.3	80.3	72.8	66.8		72.7	72.5	70.7	67.1	66.9]	10715193
5	7/16/2013	8:10:40	00d 00:10.0	70.7	80.7	72.9	68		72.8	72.7	70.6	68.4	68.3	I		11748976
6	7/16/2013	8:10:50	00d 00:10.0	68.8	78.8	71.5	65.4	-,-	71.4	71.2	66.9	65.9	65.6	1		7585776
7	7/16/2013	8:11:00	00d 00:10.0	66.7	76.7	70.7	65.4		69.8	68.9	67	65.5	65.4	[4677351
8	7/16/2013	8:11:10	00d 00:10.0	67.6	77.6	68.5	66.8		68.2	67.9	67.6	67.1	67			5754399
9	7/16/2013	8:11:20	00d 00:10.0	66.8	76.8	68.1	65.7		68	67.8	66.9	66.1	66			4786301
10	7/16/2013	8:11:30	00d 00:10.0	68	78	70	64.8		69.9	69.8	67.8	65.1	64.9			6309573
11	7/16/2013	8:11:40	00d 00:10.0	65.9	75.9	69.7	61.9	-,-	68.8	67.9	64.5	62.2	62			3890451
12	7/16/2013	8:11:50	00d 00:10.0	71.3	81.3	73.9	66.5	-,*	73.7	73.6	72	67.1	66.6			13489629
13	7/16/2013	8:12:00	00d 00:10.0	69.2	79.2	72.1	66.2	<u></u>	71.9	71.9	67.9	66.6	66.5	****		8317638
14	7/16/2013	8:12:10	00d 00:10.0	66.9	76.9	68.9	64.8	<u>.</u>	68.7	68.2	66.6	65	54.9			4897788
15	7/16/2013	8:12:20	00d 00:10.0	64	74	68.7	61.9		68.1	67.3	64.3	62.1	62	ļ		2511886
16	7/16/2013	8:12:30	00d 00:10.0	68.3	78,3	69.5	65.1		69,4	69.2	68.2	86.7	65.5			6760830
17	7/16/2013	8:12:40	00d 00:10.0	69.5	79.5	73.9	63.2		73.7	73.5	65.3	63.6	63.3	<u> </u>		8912509
18	7/16/2013	8:12:50	00d 00:10.0	69,9	79.9	73.4	68.2		72.9	71.9	69.8	68.5	68.3			9772372
19	7/16/2013	8:13:00	00d 00:10.0	68.6	78.6	72.9	63.1		72.6	72.1	68.9	63.4	63.1			7244360
20	7/16/2013	8:13:10	00d 00:10.0	68.8	78.8	70.8	63		70.8	70.7	68.9	63.8	63.6			7585776
21	7/16/2013	8:13:20	00d 00:10.0	66.6	76.6	68.9	64.1		68.8	68.8	66	64.3	64.1			4570882
22	7/16/2013	8:13:30	00d 00:10.0	68.6	78.6	71.6	65.4		71.3	71	68.6	65.7	65.5			7244360
23	7/16/2013	8:13:40	00d 00:10.0	70	80	72.8	65.9		72.7	72.5	69.6	66.1	66			10000000
24	7/16/2013	8:13:50	00d 00:10.0	64	74	65.6	63.1		66.5	66.5	63.8	63.2	63.2			2511886
25	7/16/2013	8:14:00	00d 00:10.0	67.2	77.2	70.4	62.7		70.3	70.1	66.4	63	62.9	·····		5248075
26	7/16/2013	8:14:10		68.5	78.5	71.6	63.5	·····	71.5	71.4	67.6	64.2	63.9			7079458
27	7/16/2013	8:14:20	00d 00:10.0	65.5	75.5	66.6	63.9	·····	66.5	66.4	65.5	64.4	64.3	· · · · · · · · · · · · · · · · · · ·		3548134
28	7/16/2013	8:14:30	00d 00:10.0	67.6	77.6	68.7	64.2	·	68.5	58.2	67.1	65.6	64.7			5754399
29	7/16/2013	8:14:40		68.6	78.6	70.3	67.4	<u>1</u>	70.2	70	68.3	67.6	67.5			7244360
30	7/16/2013	8:14:50		67.3	77.3	70.1	63.1		70	69.8	67.6	64.3	63.8			5370318 9772372
31	7/16/2013	8:15:00	00d 00:10.0	69.9	79.9	74.3	60.6	····· ···	73.4	72.4	65.4	60.9	60.7			6165950
32	7/16/2013	8:15:10		67.9	77.9	74	64.7	<u></u>	73.2	72.8	68.3	65.4	65.1	· · · · · · · · · · · · · · · · · · ·		11481536
33	7/16/2013	8:15:20		70.6	80.6	72.6	64.7	·····	72.4	72.3	70.4 69.7	66.2	65 64.1		• • • • • • • • • • • • • • • • • • • •	6165950
34	7/16/2013	8:15:30	00d 00:10.0	67.9	77.9	70.9	64		70.8	70.7	68.7 63	64.4 60.7	60.4			2630268
35	7/16/2013	8:15:40		64.2	74.2	67.7	60.3		67.2 69.9	66.3 69.8	67.9	64.5	64.5			5888437
36	7/16/2013	8:15:50	00d 00:10.0	67.7	77.7	69.9	64.4		69.5	69.3	66.4	65.2	65.2			5248075
37	7/16/2013	8:16:00		67.2	77.2	69.6	64.8		70.1	69.9	67.1	65.6	65.5			6025596
38	7/16/2013	8:16:10	************************	67.8	77.8	70,2 70,7	65.4 67.1		70.5	70.3	69.2	68	67.7			8511380
39	7/16/2013	8:16:20	00d 00:10.0	69.3 71 5	· · · · · · · · · · · · · · · · · · ·	73.5	68.9	·····	73,4	73.3	71	69.1	69			14125375
40	7/16/2013	8:16:30		71.5	81.5	+	66	~~~~	70.5	70.4	67.6	66.4	66.4			6760830
41	7/16/2013	8:16:40 8:16:50		68.3 69.1	78.3 79.1	71 71.4	66.8		71.2	71.1	68.6	67.1	67.1			8128305
42	7/16/2013	8:17:00		67.8	77.8	69.2	66.1		69.2	69.1	67.9	66.3	66,3			6025596
43		8:17:10		67.9	77.9	72.1	61.4	 	71.8	71.2	65.5	61.8	61.5			6165950
44	7/16/2013	8:17:10		66.5	76.5	72.4	63,6		72.3	71.8	65.1	63.9	63.7			4466836
45	7/16/2013	8:17:20		68.5	78.5	72	63.3		71.7	71.3	67.4	63.8	63.5			7079458
46	7/16/2013	8:17:40		64.4	74.4	67.1	60.7		67	66.9	63.7	60.9	60.8			2754229
47	7/16/2013	8:17:50		69.1	79.1	72.8	65.8		71.9	71	68.7	66.2	66			8128305
48	7/16/2013	8:18:00		68.6	78.6	69.8	66.7	•	69.7	69.6	69	67.1	66.9			7244360
50	7/15/2013	8:18:10		69.1	79.1	70.2	67		70.1	70	68.9	67.2	67.2			8128305
51	7/16/2013	8:18:20			79.3	74.1	65.4		73.8	73.2	67.1	65.8	65.7			8511380
52	7/16/2013	8:18:30		+	80.1	73	65.4		72.3	72	69	65.9	65.8			10232930
53	7/16/2013	- {			80.6	73.6	68.2		73.4	73.1	70.9	68.6	68.5			11481536
54	7/16/2013	8:18:50		***********	79	72.2	66.7	· · ·	70.7	70.6	67.8	67	66.8			7943282
55	7/16/2013				78.2	73.6	63.1		73.2	72.6	68	63.6	63,2			6606934
56	7/16/2013				80.3	72	64.5		71.5	71.3	69.5	67.6	65.9			10715193
57	7/16/2013				79.9	73.9	64.9		73.7	73.6	68.4	65.1	65			9772372
58	7/16/2013				80	71.8	67.2		71.8	71.7	69.9	67.3	67.3			10000000
59	7/16/2013		*** ********************************		77.5	70.1	65.5		69.5	69.1	67.7	65.8	65.7	****		5623413
60	7/16/2013			****	75.4	69.6	63.2	*.*	69.5	69.4	64.4	63.4	63,4			3467369

Addres	s Start Time	Measurement Time	Leq	LE	LMAX	LMIN	Ly	LN1	LN2	LN3	LN4	LN5	Over	Under	Inverse Log	Overall Leq
R20																50.9
1 1	7/16/2013	8:10:00 00d 00:10.0	52.9	62.9	54.5	51.5	~-	53.8	53.4	52.8	51.9	51.8			194984.5	50.5
2	7/16/2013	8:10:10 00d 00:10.0	53.3	63.3	54.8	52.3	~~	54.4	54.1	53.4	52.5	52.4		*****	213796.2	
3	7/16/2013	8:10:20 00d 00:10.0		62.6	53.5	52	-,-	53.2	53.1	52.5	52.2	52.1			181970.1]
	7/16/2013	8:10:30 00d 00:10.0		51.8	53	50.8		52.6	52.3	\$1.9	51	50.9			151356,1	
4	7/16/2013	8:10:40 00d 00:10.0		65.4	59.5	51,4		58.8	57.6	53.1	51.5	51.5			346736.9	Land Car Datab
6	7/16/2013	8:10:50 00d 00:10.0	56.9	66.9	61.4	50.5	•.•	61.3	61.1	\$5.2	51.3	50.9			489778.8	Local Car Passb
7	7/16/2013	8:11:00 00d 00:10.0	50.3	60.3	51.8	49.1		51.8	51.7	50.1	49.2	49.2			107151.9	
8	7/16/2013	8:11:10 00d 00:10.0	54.8	64.8	59.9	50.5		58.6	56.5	51.9	50.8	50.7		1	301995.2	1
	7/16/2013	8:11:20 00d 00:10.0	61.8	71.8	64	54.7		63.9	63.9	61.9	57.2	55.9	t			Local Car Passby
9		8:11:30 00d 00:10.0	50.2	60.2	54.7	49.5		53.6	52.7	50,3	49.7	49.5			104712.9	
	7/16/2013		*****	60.2	50.9	49.4		50.8	50.7	50.3	49.6	49.5	 		104712.9	
11	7/16/2013	8:11:40 00d 00:10.0 8:11:50 00d 00:10.0	50.2 48.8	58.8	50.3	47.8		49.7	49.5	48.5	48.1	48			75857.76	
12	7/16/2013		************			49.9		51	50.9	50.4	50.1	50			112201.8	1
13	7/16/2013	8:12:00 00d 00:10.0	50.5	60.5	51.1			52.5	52.3	51,9	49.4	49.2			138038.4	
14	7/16/2013	8:12:10 00d 00:10.0		61.4	52.6	49.1			50	49.2	48.9	48.8	+		87096.36	
15	7/16/2013	8:12:20 00d 00:10.0		59.4	50.2	48.8		50.1 49.6	49.5	49.3	49.1	49.1			85113.8	
16	7/16/2013	8:12:30 00d 00:10.0		59.3	49.6	49					48.7	48.6			79432.87	
17	7/16/2013	8:12:40 00d 00:10.0		59	49.6	48.5	ļ	49.5	49.4	49.1	48.7	48.0			107151.9	
18	7/16/2013	8:12:50 00d 00:10.0	+	60.3	51.2	48.6		51.1	51.1	50.2	50.8				128825	1
19	7/16/2013	8:13:00 00d 00:10.0	51.1	61.1	51.4	50.7		51.3	51.2	51	\$	50.7			162183	·
20	7/16/2013	8:13:10 00d 00:10.0	52.1	62.1	52.5	51.3	·	52.4	52.4	52.1	51.6	51.4			112201.0	
21	7/16/2013	8:13:20 00d 00:10.0		60.5	51,4	50	·····	51.2	51.1	50,6	50.2	50,1			109647.	
22	7/16/2013	8:13:30 00d 00:10.0		60.4	50.9	49.7		50.9	50.8	50.4	49.9	49.8			117489.8	
23	7/16/2013	8:13:40 00d 00:10.0		60.7	51.2	50	·	51.1	51.1	50.8	50.1	50.1	·			
24	7/16/2013	8:13:50 00d 00:10.0		60.7	51.2	49.7	·	51.1	51	5D.9	50.1	49.9	ļ <u></u>		117489.8	
25	7/16/2013	8:14:00 00d 00:10.0		58.6	50.2	48		49.9	49.8	48.4	48.1	48.1			72443.6	4
26	7/16/2013	8:14:10 00d 00:10.0		59.2	49.4	48.5		49.3	49.3	49.2	49	48.9			83176.3	4
27	7/16/2013	8:14:20 00d 00:10.0		59.4	50.2	47.7	· · · · · · · · · · · · · · · · · · ·	50.1	50	49.8	48.3	48.1			87096.3	
28	7/15/2013	8:14:30 00d 00:10.0		57.8	48.3	47.2	· · · · · · · · · · · · · · · · · · ·	48.2	48.1	47.7	47.3	47,3			60255.9	2
29	7/16/2013	8:14:40 00d 00:10.0		59.8	50.6	48.3		50.6	50.5	49.4	48.8	48.4			95499.2	2
30	7/16/2013	8:14:50 D0d 00:10.0	50.3	60.3	50.6	49.8		50.5	50.4	50.3	50	49.9			107151.	
31 32	7/16/2013	8:15:00 00d 00:10.0	49.5	59.5	50.1	48.9		50	50	49.5	49	48.9			89125.0	-
32	7/16/2013	8:15:10 00d 00:10.0	50.8	60.8	51.8	49.7	· · · · · ·	51.6	51.4	50.8	49.7	49.7			120226.	1
33	7/16/2013	8:15:20 00d 00:10.0	51	51	52.7	49.9		52.3	51.9	51	50	49.9			125892	
34	7/16/2013	8:15:30 00d 00:10.0	51.2	61.2	52.4	50.3	<u> </u>	52.3	52.1	51	50.5	50.4			131825.	2
35	7/16/2013	8:15:40 00d 00:10.0	50.2	60.2	51.9	49	<u> </u>	51.7	51.3	50.3	49.8	49.6			104712.	9
36	7/16/2013	8:15:50 00d 00:10.0	49	59	52.9	46.7		52.4	51	47.6	46.9	46.8			79432.8	2
37	7/16/2013	8:16:00 00d 00:10.0	49.5	\$9.5	52.2	48.2	· · ·	51.7	51.6	48,9	48.3	48.3			89125.0	2
38	7/16/2013		50.6	60.6	52.2	49.4		52.1	51.5	50.6	49.6	49.5			114815.	4
39	7/16/2013		51.3	61.3	52.8	49.6		52.6	52.3	51.4	49.7	49.7			134896	3
40	7/16/2013		51.7	61.7	52.5	50.5	-,-	52.3	52.2	51.7	51	50.7			147910.	3
41	7/16/2013		52.5	62.5	54.2	50.5		54.1	53.9	52	50.6	50.6			177827.	<u>,</u>
42	7/16/2013	8:16:50 00d 00:10.0	51.2	61.2	53.9	49.9		53.6	53.2	51.1	50.3	50.1			131825.	2
43	7/16/2013	8:17:00 00d 00:10.0	50	60	52.2	48.7	·	52.1	51.6	49.9	48.9	48.7			10000	2
44	7/16/2013	8:17:10 00d 00:10.0		60.3	50.9	49.4	-,-	50.9	50.8	\$0.3	49.7	49.6			107151.	**
45	7/16/2013	8:17:20 00d 00:10.0		59.2	50.3	48.4		50.1	49.9	49.2	48.5	48.4			83176.3	B
46	7/16/2013			67.2	63,3	49.5	-,-	62.3	60.4	50.5	49.6	49.6			524807.	5 Resident Noi:
47	7/16/2013			67.2	63.5	49.9		63.4	63.1	55.9	50.5	50.2			524807.	5
48	7/16/2013	8:17:50 00d 00:10.0		58.5	50.4	47.1	-,-	50.2	49.8	48.8	47.5	47.3			70794.5	8
49	7/16/2013			60.7	52.2	46.9		52.2	52	50.4	47.2	47.1			117489.	8
50	7/16/2013			61.8	53.9	49.9		53.7	53.6	51.2	50.1	50			151356.	il i
51	7/16/2013			61.1	52.8	50		52.3	52.1	50.8	50.1	50			12882	5
	7/16/2013			60.5	53.4	48.8		53.1	52.9	5D.5	49.2	48.9			112201	8
52				60	50.9	48.9		50.8	50.6	49.8	49	49			10000	
53	7/16/2013			62.4	53.6	50.8		53.4	53.4	51.7	51	50.9			173780	1
54	7/16/2013				63	53.6		62.9	62.8	59	54.7	54.3				6 Resident Nois
	7/16/2013			69.8 60.8	54.2				53.3	50.4	49.3	49.2			120225	
56	7/16/2013	8:19:10 00d 00:10.0				49.1		53.5	53.6	52.7	51.2	50.4			190546	*-
57	7/16/201	8:19:20 00d 00:1D.0		62.8	54.1	49.9		53.8 53.4			51.8	51.7			177827	
58	7/16/2013			62.5	53.6	51.6			53.3	52.6 50.9	50.3	50.2			120226	
59	7/16/2013			60.8	52.6	50.1		52.3	51.9						134896	
60	7/16/2013	8:19:50 00d 00:10.0	0 51.3	61.3	52.1	49.7		52	51.9	51.3	49.9	49.8			1 134030	1

É	Address	Start Time	Measure	ement Time	Leq	LE	LMAX	LMIN	Ly	LN1	LN2	LN3	LN4	LN5	Over	Under	Inverse Log
	R21												.	····		T · · · · · ·	
	1	7/16/2013	8:10:00	00d 00:10.0	69.6	79.6	71.3	64.8		71.1	71	69.7	66.4	65.2			9120108
	2	7/16/2013	8:10:10	aod 00:10.0	68.8	78.8	70	67.5		69.9	69.9	68.8	67.9	67.6			7585776
	3	7/16/2013	8:10:20	0.01;DD bD0	67.3	77.3	68.6	66.3	-,-	68.4	68.2	67.4	66.6	66.5			5370318
	4	7/16/2013	8:10:30	00d 00:10.0	69	79	70.6	67.2		70.2	70	68.3	67.3	67.3			7943282
	5	7/16/2013	8:10:40	00d 00:10.0	68.6	78.6	71.9	65.6		71.5	71.1	67.8	65.8	65.7			7244360
	6	7/16/2013	8:10:50	00d 00:10.0	67.4	77.4	69.9	66		69.7	69.5	66.9	66.2	66,1			5495409
1	7	7/16/2013	8:11:00	00d 00:10.0	67.9	77.9	69.1	66.1	-,-	69	69	67.9	66.5	66.5			6165950
1	8	7/16/2013	8:11:10	00d 00:10.0	65.3	75.3	66.2	64.8	-,-	66.1	66	65.3	64,9	64.9			3388442
1	9	7/16/2013	8:11:20	00d 00:10.0	62.9	72.9	65	61.7		64.7	64.6	62.8	61.9	61.8			1949845
1	10	7/16/2013	8:11:30	00d 00:10.0	63.1	73.1	65	61.2		63.9	63.6	62.7	61.6	61.4			2041738
1	11	7/16/2013	8:11:40	00d 00:10.0	65.2	75.2	67.7	63.6		67.4	66.8	64.7	63.7	63.6			3311311
	12	7/16/2013	8:11:50	00d 00:10.0	68.1	78.1	69.7	64.6		69.5	69.5	68.1	65.1	64.8			6456542
	13	7/16/2013	8:12:00	00d 00:10.0	65.6	75.6	68.3	63.6	<u></u>	67.9	67.6	66	63.8	63.8			3630781
	14	7/16/2013	8:12:10	00d 00:10.0	63	73	65.8	61.2	·	65.4	64.9	63.4	61.3	61.2			1995262
I	15	7/16/2013	8:12:20	00d 00:10.0	66.3	76.3	67.1	63.8	*.*	67	66.9	66.2	64.8	64.1			4265795
ļ	16	7/16/2013	8:12:30	00d 00:10.0	65.7	75.7	66.2	65.4	·	66.1	66	65.7	65,6	65.5			3715352
ļ	17	7/16/2013	8:12:40	00d 00:10.0	64.9	74.9	67.6	63		66.1	66	64.2	63.3	63			3090295
1	18	7/16/2013	8:12:50	00d 00:10.0	68	78	69.6	66.3		69.4	69.2	68	66.4	66.3			6309573
	19	7/16/2013	8:13:00	00d 00:10.0	66.5	76.5	67.3	65.4		67.2	67.1	66.7	65.6	65.4	[]	4466836
	20	7/16/2013	8:13:10	00d 00:10.0	65,3	75.3	66.4	64.7		66.2	66	65.1	64.8	64.7		[3388442
	21	7/16/2013	8:13:20	00d 00:10.0	68.7	78.7	69.4	66.4		69.2	69.1	68.6	67.2	67			7413102
	22	7/16/2013	8:13:30	00d 00:10.0	68.3	78.3	69.8	67.1	-,-	69.5	69.3	68.2	67.6	67.6			6760830
	23	7/16/2013	8:13:40	00d 00:10.0	68.6	78.6	71	65.8	-,-	70.9	70.8	67	65.9	65.9			7244360
	24	7/16/2013	8:13:50	ood 00:10.0	65.5	75.5	70.5	63.6		69.9	69	65.5	63.8	63.7		<u> </u>	3548134
	25	7/16/2013	8:14:00	00d 00:10.0	66.5	76.5	68.1	65	·	67.9	67.7	65.8	65.1	65.1			4466836
	26	7/16/2013	8:14:10	00d 00:10.0	67	77	69.1	64.8	···	69	68.8	66.2	65.1	64.9			5011872
	27	7/16/2013	8:14:20	00d 00:10.0	65.1	75.1	69	62.9	·····	68.8	68.4	64.9	63.1	63.1	•		3235937
	28	7/16/2013	8:14:30	00d 00:10.0	60.8	70.8	63.2	60		63.1	62.9	60.5	60.2	60.1			1202264
	29	7/16/2013	8:14:40	00d 00:10.0	65.2	75.2	66.8	60.5	····	66.6	65.7	65	61.7	61			3311311
	30	7/16/2013	8:14:50	00d 00:10.0	65.4	75.4	67.1	64.7		67	66.9	65.1	64.9	64.8			3467369
	31	7/16/2013	8:15:00	00d 00:10.0	64.9	74.9	65.9	64.1	·	65.8	65.8	64.9	64.3	64.3			3090295
	32	7/16/2013	8:15:10	00d 00:10.0	68.6	78.6	70.9	64.2		70.8	70.6	68.4	65.3	64.5			7244360
	33	7/16/2013	8:15:20	00d 00:10.0	68	78	69.S	65.5		69.4	69.3	67.4	65.8	65.7			6309573
	34	7/16/2013	8:15:30	00d 00:10.0	67.2	77.2	69	65.6	-,-	68.9	68.8	67.4	65.9	65.7			5248075
	35	7/16/2013	8:15:40	00d 00:10.0	64.2	74.2	66	63.4		65.3	65.1	64.6	63.6	63.5			2630268
	36	7/16/2013	8:15:50	00d 00:10.0	64.5	74.5	66	62.7		65.9	65.8	64.4	63	62.8			2818383
	37	7/16/2013	8:16:00	00d 00:10.0	62	72	63.8	59.6	L	63.8	63.7	62.5	60.5	60			1584893
	38	7/16/2013	8:16:10	00d 00:10.0	62.4	72.4	64.1	59.5		63.3	63.2	61.7	60	59.6			1737801
	39	7/16/2013	8:16:20	00d 00:10.0	67	77	68.3	64.1		68.2	68.1	66.3	65.3	65			5011872
	40	7/16/2013	8:16:30	00d 00:10.0	68.4	78.4	70.2	67.1		70	69.5	68	67.3	67.2			6918310
	41	7/16/2013	8:16:40	00d 00:10.0	69.3	79.3	71	67.3		70.8	70.7	69.5	68.3	67.8			8511380
	42	7/16/2013	8:16:50	00d 00:10.0	67.6	77.6	69.8	65.4		69.6	69.1	67.2	65.6	65.5			5754399
	43	7/16/2013	8:17:00	aod 00:10.0	66.4	76.4	67.7	65.3		67.5	67.4	66.6	65.5	65.4			4365158
	44	7/16/2013	8:17:10		+	74	66.1	62.5		65.8	65.7	64	62.8	62.7			2511886
	45	7/16/2013	8:17:20	00d 00:10.0		77.4	68.6	62.7		68.5	68.4	67.6	64.2	63.3		·	5495409
	46	7/16/2013	8:17:30	00d 00:10.0	65.4	75.4	66.5	64.5		66.4	66.3	65.6	64.6	64.6			3467369
	47	7/16/2013	8:17:40		65.9	75.9	69	62.1		68.9	68.5	65.7	62.5	62.3			3890451
	48	7/16/2013	8:17:50		61.4	71.4	63.7	59	.	63.6	63.4	61.8	59.2	59.1			1380384
	49	7/16/2013	8:18:00	00d 00:10.0		72.6	63.1	59.1		63	63	62.6	61.4	59.9			2884032
	50	7/16/2013	8:18:10	00d 00:10.0	64.6	74.6	66.4	62.1		66.3	66.2	64	62.3	62.2	-+		6165950
	51	7/16/2013	8:18:20		4	77.9	70	66.1	· · · · · · · · · · · · · · · · · · ·	69.6	69.4	67.5	66.2	66.1			
	52	7/16/2013	8:18:30		+	76.1	67.6	65.2		67.2	66.5	65.8	65.6 66.4	65.4			4073803 5370318
	53	7/16/2013	8:18:40			77.3	68.4	66.2		68.1	68.1	67.7	66.4	66.3			4265795
	54	7/16/2013	8:18:50			76.3	67.7	64.8	<u>.</u>	67.6	67.5	66.4	65	65			3715352
	55	7/16/2013	8:19:00		************	75.7	67.4	63.8		67.3	67.2	65.4	64.3	64.2			5011872
	56	7/16/2013	8:19:10			77	69.9	63.2		69.7	69.5	64.4	63.3	63.2	· + ····	{	8317638
	57	7/16/2013	8:19:20			79.2	71.4	67	·	71.3	71.2	68.6	67.3	67.2			6456542
	58	7/16/2013	8:19:30			78.1	69.9	65.9		69.8	69.8	67.6	66	65.9			2290868
	59	7/16/2013	8:19:40	00d 00:10.0	63.6	73.6	66.8	62.6		66.3	65.8	63.8	62.8	62.7			2511886

Addre	s Start Time	Measure	ment Time	Leq	LE	LMAX	LMIN	Lÿ	LN1	LN2	LN3	LN4	LNS	Over	Under	Log	Over Lec
R22	* London frienden anderstad 1999 1999 1999 1999 1999 1999 1999 19																59.
1 1	7/16/2013	7:40:00	00d 00:10.0	57	67	57.9	56.4		57.9	57.8	57.1	56.5	56.4	····		501187.2	
2	7/16/2013	7:40:10	00d 00:10.0	56.8	66.8	57.7	56.1		57.6	57.6	56.8	56.2	56.2			478630.1	
3	7/16/2013	7:40:20	00d 00:10.0	60.8	70.8	63.7	55.3		63.3	63	58.6	55.4	\$5.4			1202264	
4	7/16/2013	7:40:30	00d 00:10.0	60.2	70.2	64.4	57.8		64.2	63.5	59.8	58	57.9	****		1047129	
5	7/16/2013	7:40:40	00d 00:10.0	60.5	70.5	61.5	59.8		61.5	61.3	60.3	59.9	59.9			1122018	
6	7/16/2013	7:40:50	00d 00:10.0	58.3	68.3	61.4	55.9		61.2	61	57.7	56.3	56.1			676083	
7	7/16/2013	7:41:00	000 00:10.0	57.8	67.8	59.1	55.8	•,•	59	58.9	57.4	56	55.9	~~**		602559.6	
}	7/16/2013	7:41:10	00d 00:10.0	57.9	67,9	58.8	57.1		58.7	58.6	58	57.2	57.2			616595	
8	7/16/2013	7:41:20	00d 00:10.0	60.3	70,3	62	57.4		61.9	61.8	60.2	57.8	57.7			1071519	
10	7/16/2013	7:41:30	00d 00:10.0	58.9	68.9	60.1	57.8		60	59.7	59.1	58.4	58.1			776247.1	
h	7/16/2013	7:41:40	00d 00:10.0	58.4	68.4	59.7	57		59.6	59.6	57.6	57.2	57.1		1	691831	
11	7/16/2013	7:41:50	00d 00:10.0	60.1	70.1	61.1	58.9		61	60.9	60.3	59.3	59.2			1023293	
	7/16/2013	7:42:00	00d 00:10.0	57.8	67.8	58.9	57.3		58.4	58.3	57.9	57.5	57.4			602559.6	
13	7/16/2013	7:42:10	00d 00:10.0	58.4	68.4	59.6	57.3	·	59.5	59.3	58.4	57.5	57.4			691831	
14	7/16/2013	7:42:20	00d 00:10.0	63.7	73.7	65.6	58.9		64.8	64.3	63.2	61.1	60.7			2344229	
15	7/16/2013	7:42:30	00d 00:10.0	61.4	71.4	65.6	59.9	<u></u>	65.1	64.6	61.1	60	60			1380384	
	7/16/2013	7:42:40	00d 00:10.0	61.9	71.9	63	60.9		62.9	62.7	62.2	61	61			1548817	
17	7/16/2013	7:42:50	00d 00:10.0	59.2	69.2	60.9	57,9		60.7	60.3	59.6	58.3	58.1			831763.8	
h	7/16/2013	7:42:00	00d 00:10.0	57.9	67.9	59.1	57.1	·····	58.9	58.8	57.6	57.3	57.2			616595	
19	7/16/2013	7:43:10	00d 00:10.0	57.7	67.7	59.3	56.7		59.2	58.9	57.3	57	56.8		·/	588843.7	
20	7/16/2013	7:43:20	00d 00:10.0	60.3	70.3	61.4	59.3		61.4	61.1	60.1	59.6	59.5			1071519	
21		7:43:30	00d 00:10.0	61.2	71.2	62.1	50.3	·	62	51.8	61.1	60.5	60.5			1318257	
	7/16/2013 7/16/2013	7:43:40	00d 00:10.0	+	68	60.3	56.6		59,9	59.8	58.1	56.8	56.8			630957.3	
23		7:43:50	00d 00:10.0	58 57.1	67.1	57.6	56.5	<u></u>	57.5	57.4	57.1	56.7	56.6			512861.4	
24	7/16/2013 7/16/2013	7:43:50	00d 00:10.0	56.6	66.6	57.3	56.2	·····	57	56.9	56.6	56.3	56.2			457088.2	
25	7/16/2013	7:44:10	00d 00:10.0	59.2	69.2	60	56.7		59.9	59.9	59.4	57	56.8			831763.8	
26		7:44:10	00d 00:10.0	58.9	68.9	60	58.1	·····	59.9	59.9	58.6	58.2	58.2			776247.1	
27	7/16/2013	7:44:30	00d 00:10.0	58.8	68.8	59.7	57,9		59.6	59.5	58.6	58.3	58.1			758577.6	
	7/16/2013	~~~~*********		*************	+	61.6	57.9		61.4	61.4	59.8	58.1	58			1071519	
29	7/16/2013	7:44:40 7:44:50	00d 00:10.0 00d 00:10.0	60.3 61.1	70.3 71.1	63.7	57.7		63.5	63.4	61.8	57.9	57.8			1288250	
30	7/16/2013		00d 00:10.0	61.1 60.9	70.9	62.4	57.8		62.3	62.3	60.3	58	58			1230269	
31	7/16/2013	7:45:00	00d 00:10.0	58.8	68.8	62.2	57.6		61.7	61.1	58.8	57.8	57.7			758577.6	
32	7/16/2013				68	58.7	57.4		58.6	58.5	57.8	57.5	57.5			630957.3	
33	7/16/2013	7:45:20	00d 00:10.0	58		61.4	58.2		61.4	61.2	59.9	59.1	58.8			1047129	
34	7/16/2013	7:45:30	00d 00:10.0	60.2	70.2		58.9		60	59.9	59,3	59	59			870963.5	
35	7/16/2013	7:45:40	00d 00:10.0	59.4	69.4	<u>60.1</u>	57.5		59.9	59.9	58.2	57.6	57.6			724436	
36	7/16/2013	7:45:50	000 00:10.0	58.6	68.6	60 50 5	57.4	<u>1</u>	58.4	58.3	58.2	57.9	57.5	+		660693.4	
37	7/16/2013	7:46:00	00d 00:10.0	58.2	68.2	58.5	58		58.5	58.5	58.3	58.1	58.1	+		676083	
38	7/16/2013	7:46:10	00d 00:10.0	58.3	68.3	58.7 60.9			60.7	60.6	59.9	58.6	58.5		+	977237.2	
39	7/16/2013	7:46:20	00d 00:10.0	59.9	69.9		58.5		61.9	61.7	60.5	60.3	60.2			1258925	
40	7/16/2013	7:46:30	00d 00:10.0	61	71	62	60.2	·	61.5	61.3	60.2	59.1	58.9			1000000	
41	7/16/2013	7:46:40	00d 00:10.0	60 E9.4	70	61.8 59.2	58.8		59	58.9	58.5	58.2	58.1			691831	1
42	7/16/2013	7:46:50	00d 00:10.0	58.4	68.4		58	X	61.1	61.1	59.8	58.1	58			1023293	
43	7/16/2013	7:47:00	00d 00:10.0	60.1	70.1	61.2	57.9		61.2	61.2	59	57.6	57.5			831763.8	
44	7/16/2013	7:47:10	00d 00:10.0	59.2	69.2	61.4	57.4					57	56.9	· · · · · · · · · · · · · · · · · · ·		537031.8	
45	7/16/2013	7:47:20	00d 00:10.0	57,3	67.3	57.8	56.7	· · · · · ·	57,7	57.6	57.2 59.5	58.4	58.1			977237.2	ļ
46	7/16/2013	7:47:30	00d 00:10.0	59.9	69.9	60.5	57.8		60.5 61.4	60.4 61.2	59.9	58.9	58,8			977237.2	1
47	7/16/2013	7:47:40	00d 00:10.0	59.9	69.9	61.5	58.6					57.1	50,0			562341.3	1
48	7/16/2013	7:47:50	00d 00:10.0	57.5	67.5	58.6	56.9		58.4 59	58.1	57.7 58	57.7	57.7			660693.4	l l
49	7/16/2013	7:48:00	00d 00:10.0	58.2	68.2	59.1	57.5		59	58.9 57.8		57	56.9			549540.9	
50	7/16/2013	7:48:10	000 00:10.0	57.4	67.4	57.9	56.8			• • • • • • • • • • • • • • • •	57.6	56.7	56.7			537031.8	
51	7/16/2013	7:48:20	00d 00:10.0		67.3	58.2	56.6		58.1	58	57 58.4					741310.2	
52	7/16/2013	7:48:30	00d 00:10.0		68.7	60.3	57.9		60.1	59.9	58.5	58	58			741310.2	
53	7/16/2013	7 48 40	00d 00:10.0	+	68.7	60.5	57.1		60.3	60	~}·····	58.4	57.2			851138	
54	7/16/2013	7:48:50	00d 00:10.0	4	69.3	60.7	58.3	·	60,6	60.3	59	58.4	58.4			691831	1
55	7/16/2013	7:49:00	00d 00:10.0		68.4	59.9	57.5		59.5	59.3	58.4	57.6	57.6			1071519	
56	7/16/2013	7:49:10	00d 00:10.0	*****************	70.3	51.6	58.7		61.3	61.2	59.9	58.8	58.8			1202264	
57	7/16/2013	7:49:20	00d 00:10.0	+	70.8	62.4	58.6		62.2	62.1	61.2	59.3	59		•••		
58	7/16/2013	7:49:30	00d 00:10.0		67	58.6	56.4		58.3	57.9	57.2	56.5	56.4			501187.2	
59	7/16/2013	7:49:40	00d 00:10.0		66.5	57	55.9		56.9	56.9	56.3	S6.1	56			446683.6	
60	7/16/2013	7:49:50	00d 00:10.0	58	68	58.4	56.9	1	58.4	58.3	57.9	57	57			630957.3	ł

E	Address	Start Time	Measurement Time	Leq	LE	LMAX	LMIN	Ly	LN1	LN2	LN3	EN4	LNS	Over	Under	Inverse Log	Ovei Le
/	R23							,						T	1		65
	1 1	7/16/2013	10:10:00 00d 00:10	0 67.8	77.8	69.7	64.8		69.6	69.4	68	65.8	65.7			6025596	
	2	7/16/2013	10:10:10 00d 00:10	0 62.2	72.2	65.1	59		64.9	64.6	61.4	59.4	59.3			1659587	
	3	7/16/2013	10:10:20 00d 00:10	0 66.7	76.7	70.5	62.1		70.3	69.8	64.3	62.3	62.2	*		4677351	
	4	7/16/2013	10:10:30 00d 00:10	0 68.1	78.1	70.4	66.2		70.2	70.2	68	66.6	66.5			6456542	
	5	7/16/2013	10:10:40 00d 00:10		76.9	68.8	65.1	······	68.6	68.4	66.5	65.4	65.2			4897788	
	6	7/16/2013	10:10:50 00d 00:10		79.5	70.5	67.5		70.4	70.4	69.6	68	67.8			8912509 5128614	
	7	7/16/2013	10:11:00 00d 00:10		77.1	69.7	64.9	·····	69.4	69.2	66.6	65	65			2818383	
		7/16/2013	10:11:10 00d 00:10		74.5	67.6	61		67.5	67.1	64.9	61,4	61.1 59.9			2010303	
	9	7/16/2013	10:11:20 00d 00:10		73.3	66.5	59.7	·	66.4	66.2	62.4	60 58	57.9			954992.6	
	10	7/16/2013	10:11:30 00d 00:10		69.8	62.3	57.8	·····	61.7	60.8	59.3 64.8	62.7	62.6			2951209	
	11	7/16/2013	10:11:40 00d 00:10		74.7	66.1	62.2	<u> </u>	66.1	66	61.8	60	59.7			1479108	
	12	7/16/2013	10:11:50 00d 00:10		71.7	64.1	59.5		63.8 66.3	63.6 66	63.8	63.3	63.2		*****	2691535	
	13	7/16/2013	10:12:00 00d 00:10		74.3	66.4	62.9 63.6	<u></u>	68,9	68.7	65.4	63.9	63.8			4365158	1
	14	7/16/2013	10:12:10 00d 00:10 10:12:20 00d 00:10		76.4 74.9	67.7	62.5		67.6	67.4	63.9	62.8	62.6			3090295	
	15	7/16/2013	10:12:30 00d 00:10		74,5	71.1	63.6		71	70.8	67.1	63.8	63.7			6456542	1
	16	7/16/2013			73.6		61.5	·····	66.1	66	63.6	62	61.8			2290868	
	17	7/16/2013	10:12:40 00d 00:10 10:12:50 00d 00:10		78.4	66.5 73	60.7		72.8	72.1	65.2	61	61			6918310	
	18	7/16/2013	10:13:00 00d 00:10		70.1	68.5	58.6		67	65.5	60.1	59.1	58.8	·		1023293	
	19 20	7/16/2013	10:13:10 00d 00:10		69.9	62.3	58.1		61.9	61.2	59	58.3	58.2			977237.2	1
		7/16/2013	10:13:20 00d 00:10		77.4	70.7	62.2	••	70.5	70.3	66.3	63.2	62.9			5495409	1
	21	7/16/2013	10:13:30 00d 00:10		74.8	66.9	62.2	~	66.8	66.8	63.7	62.4	62.3			3019952	1
		7/16/2013	10:13:40 00d 00:10		76.7	68.2	64.9		68.1	67.9	66.9	65.6	65.2			4677351	
	23	7/16/2013	10:13:50 00d 00:10		72.1	64.9	61		64.5	64.2	62.2	61.2	61.1			1621810	
	25	7/16/2013	10:14:00 00d 00:10		71.4	62.1	60.5		62	62	61.6	60.7	60.6			1380384	
	26	7/16/2013	10:14:10 00d 00:10		74.1	67.5	61.1	<u>.</u>	67.4	67.2	63	61.2	61.1			2570396	
	27	7/16/2013	10:14:20 00d 00:10		76.9	68.7	61.9		68.6	68,4	67.7	62	62			4897788	
	2.8	7/16/2013	10:14:30 00d 00:10		78.9	71.8	63.6		71.6	71.3	68.8	65.4	54.5			7762471	
	29	7/16/2013	10:14:40 00d 00:10		75.9	68.1	63.2		68	67.9	64.4	63.4	63.3	ļ		3890451	
	30	7/16/2013	10:14:50 00d 00:10	.0 64.3	74.3	66.7	61.7	-,-	66.6	66.5	64.5	62	61.9			2691535	
	31	7/16/2013	10:15:00 00d 00:10	.0 65.6	75.6	68	62.8	-,-	67.9	67.7	64.6	63.2	63.1			3630781	ļ
	32	7/16/2013	10:15:10 00d 00:10	.0 63.1	73.1	66.5	60.2		66.4	66.1	62.4	60.6	60.4			2041738	
	33	7/16/2013	10:15:20 00d 00:10	.0 61.3	71.3	62.6	59.9		62.5	62.3	61	60	60			1348963	
	34	7/16/2013	10:15:30 00d 00:10	.0 61.2	71.2	62.4	60.5		62,2	61.8	60.9	60.6	60.6			1318257	-
	35	7/16/2013	10:15:40 00d 00:10	.0 67.5	77.5	69.9	62.4		69.6	69.4	66.7	63.5	63.1		·	5623413	
	36	7/16/2013	10:15:50 00d 00:10	.0 62.5	72.5	68.9	60.3		67.9	66.9	62.2	60.7	60.5			1778279	
	37	7/16/2013	10:16:00 00d 00:10	.0 63.7	73.7	67.2	59.2		67.1	66.8	62.9	59.6	59.3			2344229	1
	38	7/16/2013	10:16:10 00d 00:10	.0 61	71	63.3	57.4		62.9	62.3	60.6	57.8	57.6			1258925	2
	39	7/16/2013	10:16:20 00d 00:10	.0 62.8	72.8	63.8	61.8		63.7	63.6	62.9	62	61.9			1905461	
	40	7/16/2013	10:16:30 00d 00:10		76.2	69.1	62.6		68.9	68.6	65.2	63.4	63		·	4168694	*
	41	7/16/2013	10:16:40 00d 00:10		78	69.2	65.4		69.2	69.1	67.7	66.9	66.6			6309573 1949845	2
	42	7/16/2013	10:16:50 00d 00:10		72.9	66.6	60.5		66.1	65.7	63.1	60.6	60.5			2187762	-
	43	7/16/2013	10:17:00 00d 00:10		73.4	65.8	60.8		65.7	65.5	62.3	61.1	60.9			3890451	-
	44	7/16/2013	10:17:10 00d 00:10		75.9	67.6	62.3		67.5	67.3	66	64	63.2 60.9			1737801	-1
	45	7/16/2013	10:17:20 00d 00:10		72.4	64.1	60.8		64	63.9	62.3 58.9	61 58.6	58.5			776247.1	1
	46	7/16/2013	10:17:30 00d 00:10		68.9	61.1	58.4		60.7 65.8	60.3 65.7	60.8	59.6	59.3			1905461	i
	47	7/16/2013	10:17:40 00d 00:10		72.8	65.9	58.9		65.8	65.7	63.4	60.8	60.8			2290868	-
	48	7/16/2013	10:17:50 00d 00:10		73.6	65.7	60.5 62.3		68.4	68.3	66.3	63.6	62.9			4265795	-1
	49	7/16/2013	10:18:00 00d 00:10		76.3	68.5	60.1		68.4	64.8	61.3	60.2	60.2			1737801	-
	50	7/16/2013			72.4	65 67.4	60.8		66.9	65.7	62.5	60.9	60.8			2344229	-
	51	7/16/2013					60.8		68.4	68.2	66.9	64.7	64.7			4466836	5
	52	7/16/2013			76.5	68.5 66.1	62.6		66	65.8	63.9	62.7	62.7			2691539	5
	53	7/16/2013			74.5	66.1	61.4		65.8	65.7	64.7	61.8	61.5			2511886	-
	54	7/16/2013				61.9	59.2		61.7	61.7	61.2	59.4	59.3			1202264	
	55	7/16/2013			70.8	64.4	59.2		64.3	64	61.5	60.1	59.7			1659587	
	56	7/16/2013			72.7	65.3	60.5		65.2	65	61.6	60.7	60.6			186208	-
	57	7/16/2013			73.5	65.2	61.4		65.1	64.9	63,3	61.7	61.6			2238723	
	58	7/16/2013		*****	75	68.1	59.9		67.9	67.6	63.8	60	60			3162278	
	59 60	7/16/2013			77	71.6	60.8		71.5	71.2	65.1	61.3	61			5011872	2

Address	Start Time	Measuren	nent Time	Leq	LE	LMAX	LMIN	Ly	LN1	LN2	LN3	LN4	LN5	Over	Under	Log
R24													3		,	
1	7/16/2013	10:10:00	00d 00:10.0	63	73	65.4	55.4		65	64.7	62.5	55.6	55.5			1995262
2	7/16/2013	10:10:10	00d 00:10.0	68.1	78.1	69.4	65.4		69.4	69.2	68	66.1	65.6			6456542
3	7/16/2013	10:10:20	00d 00:10.0	68.4	78.4	71	63	-,-	70.8	70.7	68.3	64.5	63.7			6918310
4	7/16/2013	10:10:30	00d 00:10.0	61.3	71.3	63.1	60.3		63	62.8	61.2	60.6	60.5			1348963
5	7/16/2013	10:10:40	00d 00:10.0	67.3	77.3	70.7	60,4		70.6	70.3	63.9	60.5	60.5			5370318
6	7/16/2013	10:10:50	00d 00:10.0	68.4	78.4	70.7	66.1		70.6	70.5	69.2	66.3	66.2			6918310
7	7/16/2013	10:11:00	00d 00:10.0	68.5	78.5	69.6	66.3	÷,*	69.5	69.4	68.1	66.9	66.6			7079458
8	7/16/2013	10:11:10	00d 00:10.0	70.9	80.9	72.1	68.3		71.9	71.9	71	69.4	68.9			12302688
9	7/16/2013	10:11:20	00d 00:10.0	67.9	77.9	69.8	65.3	·····	69.5	69.3	67.6	66	65.5			6165950
10	7/16/2013	10:11:30	00d 00:10.0	64.3	74.3	68	60.9		66.9	66.7	65.6	61.1	61			2691535
11	7/16/2013	10:11:40	00d 00:10.0	63.2	73.2	66	57.9		65.9	65.7	62.8	59.1	58.4			2089296
12	7/16/2013	10:11:50	00d 00:10.0	59.8	6 9.8	62.7	57.4	-7	62	61.1	58.6	57.5	57.4			954992.6
13	7/16/2013	10:12:00	00d 00:10.0	64.9	74.9	66,2	62.7	~	66.1	65.9	64.7	63.6	63.1			3090295
14	7/16/2013	10:12:10	00d 00:10.0	61.5	71.5	64.2	58.9		63.4	63.2	61.3	59.3	59.1			1412538
15	7/16/2013	10:12:20	00d 00:10.0	65.2	75.2	66.4	64		66.3	66.2	65.1	64.2	64.1			3311311
16	7/16/2013	10:12:30	00d 00:10.0	67.1	77.1	69	64.9		68.9	68.8	66.3	65.5	65.1			5128614
17	7/16/2013	10:12:40	aod 00:10.0	64.9	74.9	67.2	62		67.1	67	64.7	62.3	62,1			3090295
18	7/16/2013	10:12:50	00d 00:10.0	68.6	78.6	71.9	62.1		71.7	71.4	67.9	62.5	62.2			7244360
19	7/16/2013	10:13:00	00d 00:10.0	62.8	72.8	65	61.7	·.·	64.8	64.5	63	62	61.9			1905461
20	7/16/2013	10:13:10	00d 00:10.0	68.4	78.4	71.8	61.2		71.4	70.7	68.2	61.3	61.3		<u> </u>	6918310
21	7/16/2013	10:13:20	00d 00:10.0	59.9	69.9	66.7	57.3	···	65.5	65.1	59	57.5	57.4			977237.2
22	7/16/2013	10:13:30	00d 00:10.0	61.5	71.5	62.8	58	<u></u>	62.7	62.7	61.3	58.4	58.4			1412538
23	7/16/2013	10:13:40	00d 00:10.0	68.2	78.2	71.5	62.7		71.1	71.1	67.6	62.9	62.9		ļ	6606934
24	7/16/2013	10:13:50	00d 00:10.0	65.3	75.3	67.1	62.9		67.1	66.9	64.5	63.1	63			3388442
25	7/16/2013	10:14:00	00d 00:10.0	67.1	77.1	68.7	64.5	·····	68.5	68.4	67.3	65.4	64,9			5128614
26	7/16/2013		00d 00:10.0	61.4	71.4	64.5	61.1		63.7	63.1	61.5	61.2	61.2			1380384
27	7/16/2013		00d 00:10.0	61.1	71.1	62.6	59.7	·····	62.5	62.4	60.7	S9.9	59.8			1288250
28	7/16/2013		00d 00:10.0	64.8	74.8	68	62	·····	67.8	67.4	63.9	62.4	62.3			3019952
29	7/16/2013		00d 00:10.0	68.8	78.8	71.1	62.4	·····	71	70.9	68.7	62.8	62.5			7585776
30	7/16/2013		00d 00:10.0	69.3	79.3	72	62.4	·····	71.9	71.8	69.8	63.7	63			8511380
31	7/16/2013		00d 00:10.0	66.4	76.4	68.2	62.3		68.1	68	65.8	62.8	62.5			4365158
32	7/16/2013		00d 00:10.0	64.4	74.4	66.8	61.9	····· ···	66.5	66.2	64.5	62.2	62			2754229 3630781
33	7/16/2013		00d 00:10.0	65.6	75.6	68.9	62.9		68.6	68.2	64.6	63.1	63			
34	7/16/2013		00d 00:10.0	62.2	72.2	65.1	60.1	·····	65	64.8	61.5	60.2	60.1 60.4			1659587 1412538
35	7/16/2013		00d 00:10.0	61.5	71.5	62.4	60.4		62.4	62.3	61.8 60	60.4 59.6	59.6		ł	1202264
36	7/16/2013		00d 00:10.0	60.8	70.8 77.8	63.1 69.7	59.5		62.4 69.6	61.9 69.4	67.9	64.1	63.4			6025596
37	7/16/2013		00d 00:10.0	67,8	*********		63		67		62.2	60.5	60.5			1778279
38	7/16/2013		00d 00:10.0 00d 00:10.0	62.5 63.1	72.5 73.1	67.5 65.7	60.3 58.3		65.6	66.3 65.5	63.3	59.5	58.8			2041738
40	7/16/2013		00d 00:10.0	59.8	69.8	62.3	57.1		62.3	61.9	59	57.4	57.2			954992.6
40	7/16/2013	************	00d 00:10.0	61.8	71.8	63.1	60.5		62.9	62.7	61.5	60.7	60.6			1513561
41	7/16/2013	{	00d 00:10.0	65.8	75.8	67.5	63.1		67.4	67.3	65.3	63.8	63.5	+		3801894
42	7/16/2013		00d 00:10.0	67.5	77.5	68.5	65.2		68,4	68.3	67.7	66.4	65.9			5623413
45	7/16/2013		00d 00:10.0	61.7	71.7	65.2	60.1		64.5	63.9	61.8	60.8	60.5			1479108
44	7/16/2013		00d 00:10.0	63.4	73.4	65.5	59.6	-,-	65.5	65.3	62.4	59.7	59.7	• • • • • • • • • • • • • • • • • • • •		2187762
46	7/16/2013		00d 00:10.0	65.5	75.5	67.1	61.3		67	66.9	65.7	63	62.2			3548134
47	7/16/2013	***************	00d 00:10.0	58.6	68.6	61.3	57.8		60.4	59.8	58.9	58.1	57.9			724436
48	7/16/2013		00d 00:10.0	57.9	67.9	58.7	57.4		58.4	58.3	58	57.5	57.5			616595
49	7/16/2013		00d 00:10.0	62.2	72.2	64.7	57.8	-,-	64.5	64.4	60.7	58.4	58.1			1659587
50	7/16/2013	{	00d 00:10.0	62.5	72.5	64.5	60,6		64.3	64.1	62.3	60.7	60.7			1778279
51	7/16/2013	{	00d 00:10.0	67.2	77.2	69.6	63.1	-,-	69.4	69.4	67.1	64.6	63.9			5248075
52	7/16/2013	*******	00d 00:10.0	*	71.9	64.7	58.7	-,-	64.6	64.5	60.8	59	58.8			1548817
53	7/16/2013		00d 00:10.0		74.3	67.4	62.2		67.1	66.4	63.2	62.3	62.3]	2691535
54	7/16/2013	**********	00d 00:10.0		76.8	68.6	65.5		68.5	68.4	67	65.6	65.5			4786301
55	7/16/2013		00d 00:10.0		73.4	65.8	61.4		65.6	65,4	62.6	61.5	61.5			2187762
56	7/16/2013		00d 00:10.0	*	74.Z	66	61		65.9	65.8	65,1	61.5	61.4			2630268
57	7/16/2013		00d 00:10.0	**********	69.8	61	58.5		60.9	60.9	59.8	58.7	58.6			954992.6
58	7/16/2013	10:19:30	00d 00:10.0	61.5	71.5	62.9	59.7		62.8	62.7	61.3	59.9	59.8			1412538
59	7/16/2013		00d 00:10.0	************	71.6	63	60.1	-,-	62.9	62.7	61.4	60.2	60.1			1445440
60	7/16/2013		00d 00:10.0	*	73.9	65.6	60.3	-,-	65.1	65	63.2	60.6	60.6			2454709

<u>مشما</u>	dress	Start Time	Measurement Time	Leg	LE	LMAX	LMIN	Ly	LN1	LN2	LN3	LN4	LN5	Over	Under	Log	୍ଦ୍
F	125								,			,	·····		.		6
	1	7/16/2013	10:10:00 00d 00:10	.0 67.8	77.8	70.2	64.2		70	69.7	67.8	65.5	64.8			6025596	~
1	2	7/16/2013	10:10:10 00d 00:10	.0 60.6	70.6	64.2	58.5	-7	63.5	62.7	60.9	58.8	58.6			1148154	
	3	7/16/2013	10:10:20 00d 00:10	.0 64.9	74.9	68.6	60		68.5	68.4	60.6	60.2	60.2			3090295	
	4	7/16/2013	10:10:30 00d 00:10	.0 66.2	76.2	68.7	64.1	-,-	68.5	68.5	66.2	64.2	64.2			4168694	
	5	7/16/2013	10:10:40 00d 00:10		76,6	67.6	64.5		67.4	67.4	66.5	65.6	64.9	*		4570882	
·····	6	7/16/2013	10:10:50 00d 00:10		79.4	71	66	<u></u>	70.8	70.6	69.2	67.4	66.8			8709636	
1	7	7/16/2013	10:11:00 00d 00:10		76.4	68.1	65.6		67.8	67.4	66.5	65.9	65.8	****		4365158	
	8	7/16/2013	10:11:10 00d 00:10		74	65.9	61.8		65.7	65.5	64.6	62	61.9			2511886	
		7/16/2013	10:11:20 00d 00:10		73.1	65.2	60.7		65.2	65.1	62.5	61.1	60.9			2041738	
	9 10	7/16/2013	10:11:30 00d 00:10		69.7	61.1	59	·····	60.9	60.6	59.5	59.1	59			933254.3	
· · · · · ·	11	7/16/2013	10:11:40 00d 00:10		73	+	60.6	·····	63.9	63.8	63	61.3	61.2			1995262	
÷		7/16/2013	10:11:50 00d 00:10		71.8	64 63	60.9	<u></u>	62.7	62.6	61.5	61.2	61.2			1513561	
	12		10:12:00 00d 00:10			+	61.4	<u></u>	64.6	64.4	63.5	61.5	61.5			2137962	
	13	7/16/2013			73.3	64.6 67.4		·	*************	67.1	65.1	61.6	61.3			3388442	
	14	7/16/2013			75.3	+	61.2		67.2			59.7				2238721	
	15	7/16/2013	10:12:20 00d 00:10		73.5	66.1	59.3		66,1	66	63.9	************	59.4			5011872	
	16	7/16/2013	10:12:30 00d 00:10		77	70.4	59.1		70.2	70	64.6	59.2	59.2			*************	
	17	7/16/2013	10:12:40 00d 00:10		73.6	67.9	62.2	·····	66.8	56	63.9	63.1	62.6			2290868	
	18	7/16/2013	10:12:50 00d 00:10		76	69.8	61.5		69.3	68.1	64.5	61.8	61.7			3981072	
******	19	7/16/2013	10:13:00 00d 00:10		71.3	67.2	60.1		65.8	65.3	61	60.5	60.3			1348963	
+	20	7/16/2013	10:13:10 00d 00:10		70.3	61.4	59.2		61.3	61.2	60.7	59.4	59.3			1071519	
	21	7/16/2013	10:13:20 00d 00:10		76.2	68.8	59.6	·	68.7	68.5	66.2	59,7	59.7			4168694	
	22	7/16/2013	10:13:30 00d 00:10	.0 64.5	74.5	66.7	63.2	··	66.2	65.8	64.7	63.4	63.3			2818383	
	23	7/16/2013	10:13:40 00d 00:10	.0 66.6	76.6	68.9	64.4		68.8	68.7	66	64.8	64.6		*****	4570882	
l	24	7/16/2013	10:13:50 00d 00:10	61.5	71.5	64.4	60.7	·	64	63.4	61.5	60.9	60.8			1412538	
l	25	7/16/2013	10:14:00 00d 00:10	60.2	70.2	60.9	59.7		60.8	60,7	60.2	59.8	59.8			1047129	
ł	26	7/16/2013	10:14:10 00d 00:10	0.0 62.9	72.9	65.8	57.8		65.7	65.4	62.4	58.1	57.9		ļ	1949845	
	27	7/16/2013	10:14:20 00d 00:10	0.0 67.5	77.5	71	60.6		70.7	70.5	65.3	60.8	60.7			5623413	
	28	7/16/2013	10:14:30 00d 00:10	.0 67.8	77.8	70.4	63.3	-,-	70.3	70.1	68.4	64	63.6			6025596	
	29	7/16/2013	10:14:40 00d 00:10	.0 65.2	75.2	67.5	62		67.4	67.3	64.3	62.4	62.2			3311311	
	30	7/16/2013	10:14:50 00d 00:10	.0 53	73	65.6	60.7		65.3	65.3	63	60.9	60.8			1995262	
l	31	7/16/2013	10:15:00 00d 00:10	0.0 64.1	74.1	67	60.1		66.7	66.6	63.6	60.4	60.2			2570396	
L	32	7/16/2013	10:15:10 00d 00:10	0.0 61.9	71.9	64.1	60.5		64.1	64	61.3	60.7	60.6			1548817	
	33	7/16/2013	10:15:20 00d 00:10	0.0 59	69	61.4	57.4		61.1	60.9	59	58.4	57.9			794328.2	
	34	7/16/2013	10:15:30 00d 00:10	0.0 57.4	67.4	58,9	56.4	<u>.</u>	58.7	58,2	57	56.5	56.5			549540.9	
	35	7/16/2013	10:15:40 00d 00:10	0.0 65	75	67.1	58.9		66.9	66.7	64.5	59.8	59.5			3162278	
	36	7/16/2013	10:15:50 00d 00:10	62.4	72.4	66.6	59.6	·	66.3	65.9	62.6	59.9	59.8			1737801	
	37	7/16/2013	10:16:00 00d 00:10	62.5	72.5	64.7	59		64.6	64.5	62.3	59.7	59.4		****	1778279	
	38	7/16/2013	10:16:10 00d 00:10	0.0 59	69	59.6	58.4		59.5	59.4	58.9	58.6	58.5			794328.2	
	39	7/16/2013	10:16:20 00d 00:10	0.0 59.4	69.4	62.1	56.9	·.·	61.7	61.5	58.2	57.1	57			870963.6	
	40	7/16/2013	10:16:30 00d 00:1	0.0 65.1	75.1	67.3	62.1	-,-	67.1	66.8	64.5	62.8	62.3		*****	3235937	
	41	7/16/2013	10:16:40 00d 00:1	.0 66.5	76.5	67.7	64.9	-,-	67.5	67.3	66.4	65.2	65.1			4466836	
	42	7/16/2013	10:16:50 00d 00:1	0.0 61.4	71.4	66.6	58,5		66.1	65.3	61.5	59	58.8			1380384	
	43	7/16/2013	10:17:00 00d 00:1	0.0 61.4	71.4	65	57.8		63.8	63	59,9	58.1	58			1380384	
	44	7/16/2013	10:17:10 00d 00:1		74.9	66.7	62.2		66.6	66.5	64.8	63.6	62.9			3090295	
h	45	7/16/2013	10:17:20 00d 00:1		69	62.2	58		61.5	60.9	59	58.4	58.3			794328.2	ł
	46	7/16/2013	10:17:30 00d 00:1		67.2	58	56.2		57.8	57.7	57.2	56.4	56.3			524807.5	
	47	7/16/2013	10:17:40 00d 00:1		71	64.8	57.5		64.5	63.4	58.8	58	57.8	~~~	<u> </u>	1258925	
	48	7/16/2013	10:17:50 00d 00:1		72	64.5	59.9		64.2	64	61.1	60.2	60			1584893	
h	49	7/16/2013	10:18:00 00d 00:1	*****************	76.1	68.7	63.6		68.5	68.1	65.7	63.9	63.8			4073803	
	50	7/16/2013	10:18:10 00d 00:1		72.1	64.5	60.4	-,-	64.2	63.8	61.4	60.5	60.5		1	1621810	
	51	7/16/2013	10:18:20 00d 00:1		72.7	65.6	60	-,-	65.2	64.5	61.8	60.1	60			1862087	
ł	52	7/16/2013	10:18:30 00d 00:1		76.1	68.8	63.2	-,-	68.4	68.2	65.8	63.7	63.5			4073803	
	********	7/16/2013	10:18:40 00d 00:1		72.6	64.6	60.7		64.3	64.2	62.2	61	60.8			1819701	
	53 54	7/16/2013	10:18:50 00d 00:1		73.5	64.9	61.3		64.8	64.6	64.1	61.7	61.4			2238721	
			10:19:00 00d 00:1		69.2	61.4	57.4		61.1	61	59.5	57.6	57.5			831763.8	1
	55	7/16/2013				63.6	57.9		63.4	63.2	61	59,5	59			1412538	1
	56 57	7/16/2013			71.5				62.6	62.6	60.9	59.3	59.3		- {	1258925	
		7/16/2013			71	62.7	59.1		65	64.9	62	58.6	58.6			2041738	
	58	7/16/2013	10:19:30 00d 00:1		73.1	65.3	58.5		65.7	65.6	63.6	59.9	59.8			2344229	
	59	7/16/2013	10:19:40 00d 00:1	0.0 63.7	73.7	66.1	59.6		1 00./		1 03.0	12.3	33,0			2377223	i

	Address	Start Time	Measure	ament Time	Leq	LE	LMAX	LMIN	Ly	LN1	LN2	LN3	LN4	LN5	Over	Under	Log	
-	R26																	
Т	1	7/16/2013	10:10:00	00d 00:10.0	61.2	71.2	64.5	59.4	·.·	64.5	64.3	60.9	\$9.5	59.5			1318257	
	2	7/16/2013	10:10:10	00d 00:10.0	62.2	72.2	66.7	58.9		65.6	64.4	59.3	59	59	****		1659587	
ŀ		7/16/2013	10:10:20	00d 00:10.0	66.7	76.7	68.6	62.9	·····	68.5	68.3	67.6	63,2	63			4677351	
ŀ	3	7/16/2013	10:10:30	00d 00:10.0	67.2	77.2	68.9	62.8	<u>``</u>	58.6	68.5	67.1	63.5	63.1			5248075	
ł	4 5	7/16/2013	10:10:40	00d 00:10.0	68.5	78.5	69.7	66.3	·····	69.7	69.6	68.2	66.7	66.6			7079458	
ł		7/16/2013	10:10:50	00d 00:10.0	66.3	76.3	69.2	64.5		69	68.6	66.2	64.7	64.6	·		4265795	
ł	6 7	7/16/2013	10:11:00	00d 00:10.0	65.7	75.7	69	61.8	·····	58.9	68.8	65.2	63.5	62.6			3715352	
ŀ	8	7/16/2013	10:11:10	00d 00:10.0	63.4	73,4	65.4	61.4		65.4	65.3	62.4	61.6	61.5			2187762	
ł	9	7/16/2013	10:11:20	00d 00:10.0	61	71	62.6	59.3		62.5	62.4	61	59.6	59.4			1258925	
ł	10	7/16/2013	10:11:30	00d 00:10,0	64	74	65.1	61	·	65	64.9	64	61.4	61.3			2511886	l
ł	11	7/16/2013	10:11:40	00d 00:10.0	63.1	73.1	64.4	61.4		64.3	64.3	63.4	62.1	61.7			2041738	í.
ł	12	7/16/2013	10:11:50	00d 00:10.0	63.5	73.5	65.9	61.2	 	65.7	65.5	62.9	61.8	61.4		[2238721	i i
ł	13	7/16/2013	10.12.00	00d 00:10.0	64.9	74.9	67.4	61.1		67.3	67.2	64.3	61.4	61.3			3090295	ĺ.
ŀ	14	7/16/2013	10:12:10	00d 00:10.0	62.6	72.6	64.9	58.6		64.7	64.6	63.3	59	58.7			1819701	1
ł	15	7/16/2013	10:12:20	00d 00:10.0	64.9	74.9	68,9	59		68.6	67.8	61.3	59.6	59.3			3090295	
l	16	7/16/2013	10:12:30	00d 00:10.0	64.7	74.7	69.5	61.1	-,-	69.3	69	63	61.6	61.5			2951209	l l
ŧ	17	7/16/2013	10:12:40	00d 00:10.0	64.2	74.2	66.5	60		66	δ5.8	63.7	60.7	60.2			2630268	l I
ľ	18	7/16/2013	10:12:50	00d 00:10.0	63.1	73.1	67.6	60.3		67.2	66.6	62.2	60.5	60.4			2041738	l I
I	19	7/16/2013	10:13:00	00d 00:10.0	60.4	70.4	62	58.5	•,•	61.9	61.6	61	59.1	58.6			1095478	
ľ	20	7/16/2013	10:13:10	00d 00:10.0	65.3	75.3	68.6	58.5	-,-	68.4	67.9	62.8	59	58.7			3388442	
ſ	21	7/16/2013	10:13:20	00d 00:10.0	64.4	74.4	68.6	63.2		68.3	67.4	64.3	63.3	63.3			2754229	
1	22	7/16/2013	10:13:30	00d 00:10.0	66.5	76.5	67.7	64.4		67.6	67.5	66.2	65.5	65		•	4466836	ł
Í	23	7/16/2013	10:13:40	00d 00:10.0	63.4	73,4	65.6	61.7	- 22	65.4	65.1	63.8	62.1	62			2187762	Ĺ
1	24	7/16/2013	10:13:50	00d 00:10.0	60	70	61.8	58,9	·····	61.4	61.3	60.4	59	59			1000000	Ĺ
- [25	7/16/2013	10:14:00	00d 00:10.0	62.4	72.4	65.8	58.2		65.6	65.4	59.8	58.7	58.4			1737801	1
- [26	7/16/2013	10:14:10	00d 00:10.0	64.1	74.1	67.2	60.4	·····	67	66.6	62.9	60.6	60.5	· · · · · · · · · · · · · · · · · · ·		2570395	Í.
l	27	7/16/2013	10:14:20	00d 00:10.0	68.2	78.2	69.5	64.6		69.3	69.3	68.6	66.6	65.4		*****	6606934	í I
	28	7/16/2013	10:14:30	00d 00:10.0	64.5	74.5	66.9	62.7	···	66.3	65.9	<u> 63.8</u>	63.2	63			2818383	í I
ļ	29	7/16/2013	10:14:40	00d 00:10.0	65.3	75.3	67.7	62		67.4	67.4	65.9	62.3	62.1			3388442	í I
1	30	7/16/2013	10:14:50	00d 00:10.0	66.6	76.6	69.3	62.1		69	68.7	66.1	62.6	62.4			4570882	í I
ł	31	7/16/2013	10:15:00	00d 00:10.0	64.4	74.4	67.3	60.4		67	66.8	64.7	60.8	60.6			2754229	1
ŀ	32	7/16/2013	10:15:10	00d 00:10.0	59.5	69.5	62.8	55.2		62.7	62.5	60	55.5	55.3			891250.9	1
ł	33	7/16/2013	10:15:20	00d 00:10.0	58.2	68.2	58.8	55.7		58.7	58.7	58.1	57	56.5		ļ	660693.4	1
ŀ	34	7/16/2013	10:15:30	00d 00:10.0	63.9	73.9	66.6	57.9		66	65.7	62.9	58.6	58.2			2454709	Ĺ
ŀ		7/16/2013	10:15:40	00d 00:10.0	64,1	74.1	67.4	60.9		67.2	67.1	62.9	61.5	61.2			2570396	ĺ
ŀ	36	7/16/2013	10:15:50		62.4	72.4	65.1	59.3		65.1	64.9	61.7	59.6	59.5		+	1737801	Í
ŀ	37	7/16/2013	10:16:00	00d 00:10.0	56.3	66.3	59.3	54.6		58.9	58.8	55.8	54.7	54.6			426579.5	i i
ŀ	38	7/16/2013	10:16:10	00d 00:10.0	59	69	60.6	57		60	59.5	58.6	57.7	57.6			794328.2	i i
ŀ	39	7/15/2013	10:16:20	00d 00:10.0	65.3	75.3	67	60.6		66.9	66.7	65.5	61.1	61			3388442 3630781	
	40	7/16/2013	10:15:30	00d 00:10.0	65.6	75.6	67.4	63.6		67.2	67.2	65.2 63.9	63.8 60.9	63.7 60.8	+		2454709	1
ŀ	41	7/16/2013	10:16:40	00d 00:10.0	+	73.9	67	60.7	<u></u>	66.8	66.5		+	58.4	-+		1023293	
ł	42	7/16/2013	10:16:50	00d 00:10.0 00d 00:10.0	60.1	70.1	62.2 66.2	58.4 60.5		62 66	61.5 65.7	60.1 64.2	58.5 61.8	60.9		+	2884032	ł
ł	43	7/16/2013	10:17:00		64.6	71.5	+	59		66	65.7	61.1	59.1	59.1			1412538	
ł	44	7/16/2013	10:17:10 10:17:20		61.5 58.8	68.8	66.2 59.9	57.4		59.8	59.7	58.5	57.6	57.5	+		758577.6	1
	45 46	7/16/2013 7/16/2013	10:17:20		59.2	69.2	59.5	58.8		59.8	59.8	59.2	58.9	58.9			831763.8	í
ł	40	7/16/2013	10:17:50		53.2 52.7	72.7	65.3	58.9		65	64.8	62.3	59.1	59			1862087	1
ł	47	7/16/2013	10:17:50		65.6	75.6	68.5	55,5		68.3	67.9	64	60.1	59.7		·	3630781	1
ł	49	7/16/2013	10:18:00		61.8	71.8	66.5	59,1		66.1	65.4	61.3	59.2	59.1			1513561	1
	50	7/16/2013	10:18:10		+	73.2	64.4	60.2		64.3	64.1	62.8	61.5	60.9			2089296	1
ł	51	7/16/2013		00d 00:10.0	+	75.7	66.8	63.1		66.7	66.6	66.2	63.6	63.3			3715352	1
	52	7/16/2013	**************	00d 00:10.0	********	72.8	64	61.5		63.9	63.8	62.9	61.6	61.5			1905461	1
ł	53	7/16/2013	10:18:40		******	74.1	65.3	62.6		65.2	64.9	63.9	63.3	62.8			2570396	
ł	55	7/16/2013	10:18:50		**********	74	67.9	61.5	 	67.5	66.8	63.3	61.7	61.6			2511886	
ł	55	7/16/2013	10:19:00		4	72.1	63.8	60.8		63.6	63.6	61.8	60.9	60.9			1621810	
	56	7/16/2013	10:19:10			71.7	63.4	60.2		63.3	63.2	61.2	60.3	60.3			1479108	
ł	57	7/16/2013	10:19:20			72.2	64,9	60.2		64.2	63.7	61.1	60.4	60.3			1659587	
ł	58	7/16/2013	10:19:30			74.1	66.3	60.1		66.2	66.2	65.1	60.3	60.2			2570396	1
ŀ	59	7/16/2013	10:19:40			76.6	69.7	61.5	-,-	69.6	69.4	66.1	61.8	61.8			4570882	
- F	60	7/15/2013	10:19:50			70.8	62	59.7		61.8	61.7	60.9	60.5	60.2			1202264	1

Address	Time	Measuren	nent	Time	Leq	LE	LMAX	LMIN	Ly	LN1	LN2	LN3	LN4	LN5	Over	Under		
R1-A1									E						1	1	176047 1107	ŋ 6
1 2	7/23/2014 7/23/2014			00:10.0	58.9 56.3	68.9 66.3	61 59.2	57 53.1	·····	60.8 59	60,6 58.9	58 55.8	57.2 53.6	57.1 53.3			776247.1166 426579.5188	l
3	7/23/2014	****************		00:10.0	56.5 64.9	74.9	68.6	58		68.5	68.1	62.6	60.1	59.8			3090295.433	i i
4	7/23/2014			00:10.0	60.2	70.2	64.5	58.5		64.4	64	59.3	58.7	58.6			1047128.548	
	7/23/2014			00:10.0	61.5	71.5	64.1	56.5	·····	64	63.8	61.5	57.7	57.2			1412537.545	
6	7/23/2014			00:10.0	55.8 59.8	65.8 69.8	56.8 62.2	54.7 54.6		56.7 62.1	56.5 61.9	56.1 59.6	54.8 55.7	54.7 54.9			380189.3963 954992.586	-
7 8	7/23/2014 7/23/2014			00:10.0	60.7	70.7	63.4	58.1	 	63.2	63.1	60	58.4	58.3			1174897.555	
9	7/23/2014			00:10.0	61.1	71.1	63.4	56.8		63.3	63.1	60.7	57.1	56.9			1288249.552	
10	7/23/2014	***************		00:10.0	64.5	74.5	69.2	59.2		69	68.3	62.7	59.8	59.4			2818382.931	
11	7/23/2014			00:10.0	60.5 57	70.5	62.5 59.4	58.3 55		62.4 59.3	62.3 59.2	60 56.8	58.4 55.2	58.3 55.1			1122018.454 501187.2336	·
12 13	7/23/2014			00:10.0		67 71.6	64	57.5		63.6	63.3	60.5	57.6	57.5			1445439.771	
14	7/23/2014	8:27:10		00:10.0	60.7	70.7	65.4	54.3	. :	65.2	65	60.1	55.1	54.6			1174897.555	
15	7/23/2014			00:10.0	65.3	75.3	70	54.2	·:	69.7	69.1	59.9	54.4	54.3			3388441.561 26302679.92	-
16 17	7/23/2014			00:10.0	74.2 60.2	84.2 70.2	78 63.1	63.1 59.3		77.9 62.2	77.5 61.4	74 60.6	65.2 59.6	64 59.5			1047128.548	-
18	7/23/2014	**************		00:10.0	************	70.4	61.7	58.9		61.6	61.5	60.4	59	59	4544		1096478.196	1
19	7/23/2014			00:10.0		73.8	66.6	59, 6	·	65.6	66.2	63.1	60	59.8			2398832.919	
20	7/23/2014			00:10.0	62.6	72.6	65.7	57.9		65.6 63.7	65.6 63.6	62.2 61.3	58.2 58.6	58 58.6			1819700.859 1479108.388	-
21 22	7/23/2014 7/23/2014			00:10.0	61.7 53.9	71.7 63.9	63.9 59.7	58.5 52		58.7	57.8	53.8	52.3	52.1			245470.8916	1
23	7/23/2014			00:10.0	*************	76	71.1	54.6		71	70.5	59.2	55	54.7			3981071.706	
24	7/23/2014	8:28:50		00:10.0		72.5	70.9	56.8	~	70,4	69.6	60.9	56.9	56.8		*****	1778279.41	
25	7/23/2014	8:29:00		00:10.0	*	67.8 79.8	60.4 72.8	56.6 60.4		59.5 72.7	58.2 72.5	57.1 69,7	56.7 63.8	56.6 62.1			602559.5861 9549925.86	-
26 27	7/23/2014 7/23/2014	8:29:10 8:29:20		00:10.0		67.7	65.9	55.6		64.8	63.7	57.2	55.7	55.7		†	588843.6554	
28	7/23/2014	8:29:30	00d	00:10.0	63.4	73.4	65.7	58		65.7	65.5	63.1	59,5	58.8			2187761.624	
29	7/23/2014			00:10.0	4	67.9	61.4	56.5		60.9	60.5	57.7	56.7	56.6			616595.0019	
30	7/23/2014	8:29:50 8:30:00		00:10.0		65.4 69	57.6 61.9	52.8 54.8		57 61.8	57 61.5	55 58.6	53 55.9	52.9 55.3			346736.8505	·
31 32	7/23/2014 7/23/2014	8:30:00		00:10.0		68.9	61.9	54.8	•••	61.8	61.5	55.7	54.3	54.3			776247.1166]
33	7/23/2014	8:30:20		00:10.0	63.7	73.7	66	61.7		65	64.1	63.2	61.9	61.8			2344228.815	_
34	7/23/2014	8:30:30	******	00:10.0	64.7	74.7	66.6	61.4		66.5	66.4	65.2	62.6	62 59.2			2951209.227 6456542.29	-
35 36	7/23/2014 7/23/2014	8:30:40 8:30:50		00:10.0 00:10.0		78.1 68.4	73.8	59.1 56.6		73.6 65.2	72.9 64.2	61.8 57.7	59,4 56.8	55.2			691830.9709	-
37	7/23/2014	8:31:00		00:10.0	55.4	65.4	57.8	52.8		57.6	57.3	56.5	53	52.9			346736.8505	1
38	7/23/2014	8:31:10		00:10.0	58.1	68.1	59.1	53	·	58.9	58.9	58.4	53.8	53.3		ļ	645654.229	
39	7/23/2014	8:31:20		00:10.0		72.9	65.1	58.9	····· 7:5	65	64.8	61.9 62.2	60.3 58.7	59.6 58	 	+	1949844.6 1412537.545	-
40 41	7/23/2014 7/23/2014	8:31:30 8:31:40		00:10.0	61.5 61.4	71.5 71.4	63.4 66.4	57.2 56.3		63.3 65.3	63.1 64.1	57.2	56.6	56.4			1380384.265	-
42	7/23/2014			00:10.0		74,4	69	58.2		68.9	68.7	62.6	58.8	58.7			2754228.703	-
43	7/23/2014	8:32:00		00:10.0		63.4	58.2	49.7	ļ	57.9	57.8	52.9	49.9	49.9	Ļ		218776.1624	
44	7/23/2014	8:32:10		00:10.0	+	62.1 70.9	54.4 63.1	50.1 54.4		53.3 62.9	52.4 62.7	51.3 60.9	50.7 56.9	50.6 56.1	+		162181.0097 1230268.771	~
45 46	7/23/2014 7/23/2014	8:32:20 8:32:30		00:10.0	**********	69.5	60.4	58.9		60.3	60.1	59.4	59	59			891250.9381	
47	7/23/2014	8:32:40		00:10.0		70	61.4	57.6		61.3	61.3	60.7	58	57.8			1000000	-
48	7/23/2014	8:32:50	*****	00:10.0	******	71.7	63.9	57.3		63.8	63.7	61.6	57,4	57.4			1479108.388 537031.7964	
49 50	7/23/2014 7/23/2014	8:33:00 8:33:10	******	00:10.0 00:10.0		67.3 73.4	60.8 64.7	54.1 60.7	·····	60.1 64.6	59.5 64.4	56.6 63.7	54.4 61.1	54.2 60.8			2187761.624	
51	7/23/2014	8:33:20		00:10.0	************	77.2	69.6	60.7		69.5	69.3	67.3	61.4	61.1			5248074.602	
52	7/23/2014	8:33:30		00:10.0		75.2	69.2	61.3	<u></u>	68.8	68.2	65.6	61.6	61.4			3311311.215	
53	7/23/2014			00:10.0		74.7	69.2 60.1	60 54.4		69.1 59.9	68.5 59.8	63.8 57.8	60.5 55.1	60.3 54.6		*****	2951209.227 537031.7964	
54 55	7/23/2014 7/23/2014	8:33:50 8:34:00		00:10.0		67.3 69	62.5	54.1	<u></u>	61.7	61.2	57.2	54.2	54.2			794328.2347	-
56	7/23/2014	8:34:10		00:10.0		69.2	62.4	57.9		62	61.5	59,1	58.1	58			831763.7711	
57	7/23/2014	8:34:20		00:10.0		72.1	64.4	59.5	·	64.3	63.9	61.9	59,9	59.7			1621810.097 512861.384	
58	7/23/2014	8:34:30 8:34:40		00:10.0		67.1	61.6 60.6	55.3 54.8	·····	60.9 60	60.3 59	57.2 55.3	55.5 55	55.4 54.9			512861.384	
59 60	7/23/2014	8:34:40	******	00:10.0		75.8	68.6	60.5		68.2	67.7	65.9	61.9	60.9			3801893.963	
61	7/23/2014	8:35:00	00d	00:10.0	56	66	61.8	55.1		61	60.1	55.6	55.3	55.2			398107.1706	
62	7/23/2014	8:35:10		00:10.0		75.6	71.1	55.3		70.9	69.4	61.2	55.8 57.5	55.4 57.3			3630780.548 1584893.192	
63 64	7/23/2014 7/23/2014	8:35:20 8:35:30	*****	00:10.0		72 73.1	71 65.1	57.2 58.6		70 64.8	68.8 64.4	61.6 63.5	58.8	58.7		44.000	2041737.945	
65	7/23/2014	8:35:40		00:10.0		71.7	63.6	59.8		63.5	63.3	61.6	59,9	59.9			1479108.388	
66	7/23/2014	8:35:50	00d	00:10.0	63.3	73.3	67.1	58.9		66,8	66.5	62.8	59.6	59.1			2137962.09	
67	7/23/2014	8:36:00	******	00:10.0		68.1	59.3	57.3 57.1		59.2 60.6	59.1 59.5	58 57.7	57.5 57.4	57.4 57.2			645654.229 741310.2413	
	7/23/2014 7/23/2014	8:36:10 8:36:20		00:10.0		68.7 71.8	61.6 64.2	57.1		64.1	63.2	61.2	58.6	58.5			1513561.248	
70	7/23/2014	8:36:30		00:10.0		72.6	65.3	59.4		65.1	64.9	62.8	60.2	59.8			1819700.859	
71	7/23/2014	8:36:40		00:10.0		67.7	59.4	55.6		59.2	59	57.9	57.4	56.5			588843.6554	
72	7/23/2014			00:10.0		64.7 64.2	56.7 56.7	52.1 51.3	·······	56.5 56.4	56 56.3	54.7 54.3	52.4 52.3	52.3 51.8			295120.9227 263026.7992	
73	7/23/2014	8:37:00		00:10.0	************	64.6	58.3	49.1		58.2	58.1	52	49.2	49.2			288403.1503	
75	7/23/2014	8:37:20	00d	00:10.0	59.2	69.2	60.8	57.2	T.T	60.7	60.4	59.3	57.3	57.2			831763.7711	***
76	7/23/2014	8:37:30	******	00:10.0		63.7	59.1	50.6		58.6	58.2	53.1	50.7	50.6 53.7			234422.8815	
77	7/23/2014 7/23/2014			00:10.0		68.6 73.8	61.6 65.8	53.6 61.5		61.2 65.6	60.5 65.5	56.8 63	53.8 62.2	62			2398832.919	
78 79	7/23/2014			00:10.0		67.5	64.8	54.1		63.9	63	57,4	54.2	54.2			562341.3252	Ē.
80	7/23/2014	8:38:10	00d	00:10.0	56.2	66.2	57.7	54.1		57.6	57.5	55.7	54.3	54.2			416869.3835	
81	7/23/2014			00:10.0		65.8	56.7	55.3		56.6	56.5	55.7	55.4	55.4			380189.3963	
82	7/23/2014	8:38:30 8:38:40		00:10.0	************	75.8 73.5	70.7	55.5 59.3		70.5	70.2 68.9	58.3 62.5	56 59.5	55.8 59,4	.+		2238721.139	
83 84	7/23/2014			00:10.		81.1	74.4	59.6		74.2	74.2	70.5	61.8	60.7			12882495.52	**
85	7/23/2014	8:39:00	00d	00:10,0	63.1	73.1	67.6	57.2	~	67.2	67	59.9	57.4	57.3			2041737.945	
86	7/23/2014			00:10.	***********	72.5	66.8	57.5		66.6	66.4	60.4	57.6 58.5	57.6			1778279.41 1122018.454	
87 38	7/23/2014			00:10.0		70.5	65 65	58.3 61.1		63.9 64.9	63.3 64.7	60.1 61.9	58.5 61.2	58.4 61.2			1659586.907	(m. m)
4 40	1 1/23/2014	1 0.53.50	1000	100.204							63	61.7	*************	60.2	**********			ĩ

E 2 1	Address	Start Time	Measure	ment Time	Leq	LE	LMAX	LMIN	Ly	LN1	LN2	LN3	LN4	LN5	Over	Under		Ove
	R1-C2	7/23/2014	9:10:00	00d 00:10.0	61.6	71.6	62.8	58.6	-,-	62.7	62.7	61.4	59	58.9			1445439.771	6
*******	2	7/23/2014	9:10:10	00d 00:10.0	68.8	78.8	71.6	62.7		71.5	71.4	68,5	63.1	62.8			7585775.75]
	3	7/23/2014	9:10:20	00d 00:10.0	61	71	67.2	58.9		66.1	65.3	60.2	59	59			1258925.412	ļ
	4	7/23/2014	9:10:30	00d 00:10.0	61.7	71.7	63.7	58.4	<u>.</u>	63.6	63.5	59.8	58.8	58,6			1479108.388	ł
	5	7/23/2014 7/23/2014	9:10:40 9:10:50	00d 00:10.0 00d 00:10.0	61.5 60.4	71.6 70.4	63.5 64.1	59.8 57.6		63.4 62.3	63.4 60.8	61.7 59.8	60 57.9	59.9 57.7			1445439.771 1096478.196	
	6	7/23/2014	9:11:00	00d 00:10.0	65.9	75.9	72,3	56.7		72.1	71.3	62.3	57.2	56.9			3890451.45	1
	8	7/23/2014	9:11:10	00d 00:10.0	58.8	68.8	60.4	56.7	-,-	60.3	59.9	58.2	57.1	57			758577.575	
	9	7/23/2014	9:11:20	00d 00:10.0	61.3	71.3	62.5	59.6		62.4	62.2	61.4	59.9	59.8			1348962.883	
	10	7/23/2014	9:11:30	00d 00:10.0	64.9	74.9	68.3	60.2		68.2 59.3	67.9 58.8	64 56.7	61.4 55.3	61.3 55.3			3090295.433 436515.8322	
	11 12	7/23/2014	9:11:40 9:11:50	00d 00:10.0 00d 00:10.0	56.4 65.4	66.4 75.4	60.2 70.2	55.2 55.3		70	69.6	63.5	56.2	55.6			3467368.505	
	13	7/23/2014	9:12:00	00d 00:10.0	61.2	71,2	62.5	60.4		62.4	62.3	61.1	60.6	60.6			1318256.739	1
	14	7/23/2014	9:12:10	00d 00:10.0	56.4	66.4	60.4	55.3	ļ .	59.8	59.3	56.2	55.5	55.5			436515.8322	
	15	7/23/2014	9:12:20	0Dd 00:10.0	53.7	63.7	57.1	50.7		56.9	56.7	53.9	51.4	51.3			234422.8815	
	16	7/23/2014	9:12:30 9:12:40	00d 00:10.0 00d 00:10.0	53.5 58.2	63.5 68.2	56 59.8	49.2 55.8	<u> </u>	55.9 59.6	55.9 59.6	51.8 57.8	49.5 56.2	49.4 56			660693.448	-
	17 18	7/23/2014 7/23/2014	9:12:50	00d 00:10.0	63.5	73.5	65.5	58.2		65.4	65.1	63.5	59	58.5			2238721.139	1
	19	7/23/2014	9:13:00	00d 00:10.0	64.3	74.3	56.8	61	<u></u>	66.7	66.5	63.9	62.7	62			2691534.804	
	20	7/23/2014	9:13:10	00d 00:10.0	59.9	69.9	62	57.8		61.8	61.6	60	58.3	58.1			977237.221	
	21	7/23/2014	9:13:20	00d 00:10.0	60.5	70.5	61.4	58.2		61.3	60.8	60.4 58.1	58.4	58.3			1122018.454	
	22	7/23/2014	9:13:30 9:13:40	00d 00:10.0	58.6 60.6	68,6 70.6	61.5 61.1	56.5 58.1		61.4 61	61.3 61	60.4	56.6 60.1	56.6 59.1	t		1148153.621	
	23 24	7/23/2014	9:13:50	00d 00:10.0	60.4	70.0	64.3	57.3		63.8	60.9	59.4	57.5	57.4			1096478.196	4
	25	7/23/2014	9:14:00	00d 00:10.0	58.8	68.8	63.8	56.1	<u>.</u>	62.7	62.4	57.9	56.2	56.2	+-		758577.575	-
	26	7/23/2014	9:14:10	0Dd 00:10.0	62	72	66	57.1	<u> </u>	65.9	65.7	61.2 57 g	57.4	57.2			1584893.192	1
	27	7/23/2014	9:14:20	00d 00:10.0 00d 00:10.0	*****	68.1 69.3	59.4 60.5	56.7 57.6		59.2 60.4	59 60.3	57.8 59.3	56.9 57.6	56.8 57.6			645654.229 851138.0382	-
	28 29	7/23/2014 7/23/2014	9:14:30 9:14:40	00d 00:10.0		68.6	60.5	57.6		60.6	60.4	59	56.2	56	+		724435.9601	ļ
	30	7/23/2014	9:14:50	00d 00:10.0	*****	69.6	60.9	57. 9		60.8	60.7	59.5	58.2	58			912010.8394	1
	31	7/23/2014	9:15:00	00d 00:10.0	57.7	67.7	60	54.6	· · · · · · · · · · · · · · · · · · ·	59.9	59.8	57	54.9	54.7			588843.6554	-
	32	7/23/2014	9:15:10	00d 00:10.0	64	74	68.4	59.6		68.3 68.7	66.5 68.4	61.3 64.4	60.6 60.9	60.5 60.8			2511886.432	- 1
	33	7/23/2014	9:15:20 9:15:30	00d 00:10.0 00d 00:10.0		74.1	68.8 63.8	60.4 54.8		63.7	63.7	61	\$5.1	54.9			1096478.196	
	35	7/23/2014	9:15:40	00d 00:10.0	+	69.1	60.4	56.2	<u>~</u>	60.3	60.1	58.6	57.6	57			812830.5162	1
	36	7/23/2014	9:15:50	00d 00:10.0	**************	69.1	61.5	56		61.4	61.3	58.9	56.4	56.1			812830.516	-
	37	7/23/2014	9:16:00	00d 00:10.0	+	69.3	60.7	57.3		60.3	60.3	59.3	57.6	57.5	+		851138.0382	- H
	38	7/23/2014	9:16:10	00d 00:10.0	55.2	65.2	59.7	50.2		59.6 66.2	59.5 65.5	53.2 57.5	50.5 53.6	50.4 52.8			331131.1215	
	39 40	7/23/2014	9:16:20 9:16:30	00d 00:10.0 00d 00:10.0	61.8 68.1	71.8 78.1	66.4 73.8	52 60.1		73.6	72.9	66.6	60.4	60.3			6456542.29	
	41	7/23/2014	9:16:40	00d 00:10.0		68.3	60.3	55.9		60	5 9 .9	58.2	56.1	56			676082.9754	
	42	7/23/2014	9:16:50	00d 00:10.0	59.6	69.6	60.3	58.5		60.2	60.2	59.7	58.6	58.5			912010.839	-
	43	7/23/2014	9:17:00	00d 00:10.0		68.9	60.8	56.9		60,4	59.9	58.7	57.2 58	57			776247.116	
	44	7/23/2014	9:17:10 9:17:20	00d 00:10.0 00d 00:10.0	+	71.5 68.4	64.2 63.6	57.7 55.9		64.1 62.8	63.9 62.1	58.4	57.2	57.8 56.5			691830.970	
	45	7/23/2014	9:17:30	000 00:10.0		71.3	65.5	54.2		65.3	64.8	60.6	54.3	54.3			1348962.88	9
	47	7/23/2014	9:17:40	00d 00:10.0		72.2	64.2	59.2		64.1	64	62.2	59,4	59.3			1659586.90	
	48	7/23/2014	9:17:50	00d 00:10.0		66.3	61.9	54.4		61	59.8	56.2	54.7	54.6			426579.518	
	49	7/23/2014	9:18:00	00d 00:10.0		71	62.3 61.9	58.3 57		62.2 61.5	62.1 60.6	60.6 58,4	59.1 57.3	59 57.3			1258925.41	
	50	7/23/2014	9:18:10 9:18:20	00d 00:10.0 00d 00:10.0		68.3 69.8	60.5	58.2		6D.4	60.4	59.7	58.4	58.3			954992.58	
	52	7/23/2014	9:18:30	00d 00:10.0		66	60	53.2		59.8	59.6	55.6	54	53.5			398107.170	- 4
	53	7/23/2014	9:18:40	000 00:10.0	54.7	64.7	56	52.8		56	55.8	54.5	53.1	53			295120.922	-
	54	7/23/2014	9:18:50	00d 00:10.0		71.3	63	55		62.9	62.7	61.6	56.1 61.4	55.2 61.4	······		1348962.88 5888436.55	
	55 56	7/23/2014	9:19:00 9:19:10	00d 00:10.0 00d 00:10.0		77.7	70.3 68.7	61.2 58.1	~	70.2 67.5	70.1 66.8	66.6 64.4	59.4	58.6		*****	2137962.0	
	57	7/23/2014	9:19:20	00d 00:10.0		65.7	58.1	53.3		57.9	57.6	56	54	53.6			371535.229	1
	58	7/23/2014	9:19:30	00d 00:10.0	53.2	63.2	55.6	51.1		55.6	55,3	52.7	51.2	51.2			208929.613	
	59	7/23/2014	9:19:40	00d 00:10.0		66.5	58.2	54.6		58.1	58.1	56	54.8	54.7			445683.592 1122018.454	:
	60	7/23/2014	9:19:50 9:20:00	00d 00:10.0 00d 00:10.0		70.5 66.1	61.7 60.4	56.6 54.2		59.9	61.5 59.3	60.5 55.5	57.7 54.6	57 54.4			407380.2778	1
	61 62	7/23/2014	9:20:00	004 00:10.0		68.2	60.4	55.5		60.4	60.2	57.9	55.9	55.8			650693.448	1
	63	7/23/2014	9:20:20	00d 00:10.0		61.2	55.5	50.2		54.7	53.9	51.3	50.3	50.3			131825.6739	
	64	7/23/2014	9:20:30	00d 00:10.0		59.9	52.5	47,9	-,-	52.1	51.7	48.8	48	48			97723.7221	-
	65	7/23/2014	9:20:40	00d 00:10.0		64.6	55,7	52.5		55.4	55.2 73,8	54	53.8 56.7	53.6 56.3			288403.1503 7762471.166	-1
	66	7/23/2014		00d 00:10.0		78.9 72.5	75.2 66.4	55.7 60.9		74.8 66.3	65.6	66.3	61.1	56.5 61			1778279.41	1
	67	7/23/2014	4	008 00:10.0		75.9	70.6	61		70.4	69.9	64.5	62.1	61.6			3890451.45]
	69	7/23/2014	9:21:20	00d 00:10.0		72	64.9	59		64.6	64.4	61.7	59.4	59.1			1584893.192	
	70	7/23/2014	9:21:30	00d 00:10.0		74.5	69.3	56.6		69	68.4	59.1	56.9	56.6			2818382.931 2398832.919	-
	71	7/23/2014		00d 00:10.0	**************	73.8	69.2	61.4 61.1		68.9 63	68.3 62.9	63.6 62,1	61.5 61.4	61.5 61.2	·+		1659586.907	-1
	72	7/23/2014	9:21:50 9:22:00	00d 00:10.0		72.2	63.1 63.5	59.8		63.4	63.4	63	60.5	60.1			1778279.41	1
	73	7/23/2014				67.9	59,8	57		59.3	59.1	57.8	57.3	57.2			616595.0019	
	75	7/23/2014		00d 00:10.0	53.7	63.7	57.5	52.6		57.2	56.6	53.4	53	52.8			234422,8815	
	76	7/23/2014		00d 00:10.		65.8	59.7	51.4		59.4	58.6	53.8	51.6	51.5			380189.3963 524807.4602	-
		7/23/2014		00d 00:10.		67.2	58.9	55.7 56.3		58.9 73.2	58.8 72.6	56.6 65.3	55.8 58.9	55.7 57.8	+		6309573.445	-1
	78	7/23/2014		00d 00:10.		78 69.5	73.7 61.9	55.2		61.7	61.5	60.9	56	55.5			891250.9381	
	79 80	7/23/2014		00d 00:10.		69.6	62.6	55.2		62.4	62.1	58.9	55.3	55.2			912010.8394	
	81	7/23/2014		00d 00:10.	0 61.2	71.2	62.7	59.1		62.7	62.6	61.7	59.4	59.2			1318256.739	
	82	7/23/2014	9:23:30	00d 00:10.	D 66.1	76.1	69.7	59.3		69.5	69.4	64.9	59.7	59.5			4073802.778 5011872.336	
	83	7/23/2014		00d 00:10.		77	72.1	61.6 60.3		71.9 65.5	71.2 64.4	65.5 61.3	61.8 60.7	61.7 60.4			1548816.619	-1
	84	7/23/2014		00d 00:10.		71.9	65.8 73.1	60.3		72.9	72.7	67.2	61.5	60.4		v+ v-+	7585775.75	1
	85 86	7/23/2014		00d 00:10.		65.7	60,2	51.2		60.1	59.9	54.7	51.8	51.5			371535.2291	
	87	7/23/2014	**************			64.8	58.4	51.2		57.4	56.9	52.2	51.8	51.7			301995.172	
	88	7/23/2014	9:24:30	00d 00:10		71.3	62.3	58.4			62.2	61,4	59.2	58.9			1348962.883	
	89	7/23/2014	9:24:40	00d 00:10.		73.4	66.3 70.6	59.2 61.3		65.5 70.4	64.5 70	62.9 67.4	59.5 64.1	59.3 62.8			2187761.624 5623413.252	

E	Address	Start Time	Measure	ment Tir	ne	Leq	LE	LMAX	LMIN	Ly	LN1	LN2	LN3	LN4	LN5	Over	Under	Inverse	Over Lec
	R1-D2	7/23/2014	10:12:00	000 00:	10.0	46.5	56,5	47.5	44.8	-,-	47,4	47.4	46.7	45.5	45.1			44568.36	47.
******	2	7/23/2014	10:12:10	00d 00:	****	43.2	53.2	44.8	41.9		44.6	44.6	43.4	42.3	42.1			20892.96	
	3	7/23/2014	10:12:20	00 600		41.9	51.9	42.8	41.4 40.4		42.6 42.4	42.2 42	41.7 40.7	41.6 40.5	41.5 40.4			15488.17 12022.64	
	4	7/23/2014	10:12:30 10:12:40	00d 00:		40.8 42.8	50.8 52.8	42.6 44.7	40.4		44.6	44.5	42.6	40.7	40.6			19054.61	
	6	7/23/2014	10:12:50	00d 00:		40.1	50.1	42.7	39.6		42.1	41.5	40.1	39.7	39.7			10232.93	
	7	7/23/2014	10:13:00	00d 00:		40.1	50.1	40.7	39.4		40.6 43.4	40.5 43.2	40 41.9	39 .5 40.7	39.4 40.7		 	10232.93	1
	8	7/23/2014 7/23/2014	10:13:10 10:13:20	00 b00		42.2 46.1	52.2 56.1	43.5 47.9	40.6 43.5		47.8	47.6	45	43.7	43.6			40738.03	
	10	7/23/2014	10:13:30	00 b00		51.8	61.8	56.9	47.2	·····	55.9	54.6	50.2	47.8	47.3			151356.1	
	11	7/23/2014	10:13:40	00d 00		48.6	58.6	53	46.6 44.1		51.9 48.1	50.6 47.2	47.9 45	46.9 44.3	46.8 44.2			72443.6 30199.52	
	12 13	7/23/2014 7/23/2014	10:13:50	00d 00:		44.8	54.8 54.1	49.3 45.9	44.1		45.5	45	43.9	43.2	43.1			25703.96	1
	14	7/23/2014	10:14:10	00d 00		48.3	58.3	49.2	44.4		49.1	49.1	48.1	47	46.3		<u> </u>	67608.3	
	15	7/23/2014	10:14:20	00d 00	*******	46.6	56.6	47.6	46.1		47.3 48	47.1 47.9	46.7 46.8	46.2 45.3	46.1 45.1			45708.82	
	16 17	7/23/2014	10:14:30 10:14:40	00 b00		46.7 44.5	56.7 54.6	48.1 45.4	44.8 44		45.1	44.9	44.6	44.2	44.1			28840.32	
	18	7/23/2014	10:14:50	00 b00		46.4	56.4	48.9	44.4		48.6	48.3	45.8	44.5	44.4			43651.58	
	19	7/23/2014	10:15:00	00 b00	********	47	57	52	45.2		50.9 53.2	49.5 52.7	46.1 50.5	45.5 47.6	45.4 47.3			50118.72 117489.8	
	20	7/23/2014	10:15:10	00d 00		50.7 48.4	60,7 58,4	53.5 50.8	46.3 46.1		50.7	50.5	48.8	46.6	46.3			69183.1	
	21 22	7/23/2014	10:15:30	00d 00		43.2	53.2	46.4	41.8		45.8	45.2	43.4	42.1	42			20892.96	•
	23	7/23/2014	10:15:40	00d 00		42.6	52.6	44.8	39.5		44.3	44	41.9 43.9	40.1 40.5	39.9 40.4			18197.01	4
	24 25	7/23/2014 7/23/2014	10:15:50	00d 00 00d 00		43.5 46	53.5 56	46.4 47.1	40.3 43.8		45.6 46.9	45.1 46.8	45.6	40.5 44.1	40.4			39810.72	
	25	7/23/2014	10:16:10	00d 00		47	57	48.1	45		48	48	47.2	45.9	45.4			50118.72	2
	27	7/23/2014	10:16:20	000 00	*********	42.9	52.9	45	42.1		44,8	44.7 44.7	42.8 42.5	42.2 41.8	42.2 41.6			21877.62	
	28 29	7/23/2014	10:16:30 10:16:40	00 b00 00 b00		43.4 47	53.4 57	45.9 50.4	41.6 44.2		45.5 50	44.7 48.5	42.5	41.0	41.8			50118.72	
	30	7/23/2014	10:16:50	000 00		45.3	55.3	49.8	43.5		49.4	48,3	45.4	44.1	43.8			33884.42	2
	31	7/23/2014	10:17:00	00 b00		44,8	54.8	46.4	43.1		46.3	46.2	44.1	43.4	43.2 45.4			30199.52	1
	32	7/23/2014 7/23/2014	10:17:10		0:10.0 0:10.0	51.8 44.2	61.8 54.2	54.5 48.4	45.2 42	-,- -,-	54.4 47.4	54.3 46.5	51.7 43.2	45.6 42.3	45.4			26302.68	
	33 34	7/23/2014	10:17:30	000 000	********	44.3	54.3	48.1	42.7		47.5	46.9	44.3	43	42.9			26915.39	-1
	35	7/23/2014	10:17:40	00d 00		50.4	60.4	54.8	44,6		54.3	53.6	46.9	44.9	44.7			109647.8	3
	36	7/23/2014 7/23/2014	10:17:50	00 b00 00 b00		50.6 47.6	60.6 57.6	56.3 51.1	43.4 43.7		55.9 49.4	55.7 48.3	47,4 48.3	43.6 44	43.5 43.8			57543.99	
	37 38	7/23/2014	10:18:10	000 000		50.6	60.6	53.9	47		\$3,5	53.2	49.4	47.4	47.1			114815.4	
	39	7/23/2014	10:18:20	00d 00		45.6	55.6	49.2	41.9		49.1	49.1	44.9	42.2	42.1			27542.29	
	40	7/23/2014	10:18:30	00 b00 00 b00		44.4	54.4 54	48 46.4	42.3 42.1		47.2	46.2 46	43.6 43.8	42.5 42.2	42.5 42.1			25118.86	-
	41 42	7/23/2014 7/23/2014	10:18:40	00d 00		45.5	\$5.5	48.3	42.6		47	46.7	45.1	42.8	42.8			35481.34	~
	43	7/23/2014	10:19:00	00d 00	********	47.8	57.8	50.7	44.2		50.4	50.1	47.8	45.9	45.1	ļ		60255.90 30199.5	
	44	7/23/2014	10:19:10			44.8 47.6	54.8 57.6	47.5 49.1	42 45.9	······	46.5 48.7	46.1 48.4	44.4 47.6	42.3 47	42.2 46.6			57543.9	
	45	7/23/2014 7/23/2014	10:19:20		********	44.1	54.1	47.3	42.2		46.7	46.2	44.1	43.1	42.5			25703.90	
	47	7/23/2014	10:19:40	~~~~~~~~		44.9	\$4.9	47.5	42.2		46.B	46.4	44.5	42.8	42.4			30902.9 25118.8	
	48	7/23/2014	10:19:50	** *******	0:10.0	44	54	46.8 47.5	41.8 44.3		45.7 46.8	45.4 46.5	43.3 45.6	41.9 44.5	41.8 44.4			33884.4	**
	49 50	7/23/2014	10:20:00		******	45.3 45.8	55.3 55.8	46.5	44.4		46.4	46.3	45.6	45.1	44.7			38018.9	4
	51	7/23/2014	10:20:20			44.7	54.7	46.3	43.3		46.2	46.1	44.7	43.5	43.4	ļ		29512.0	
	52	7/23/2014	10:20:30			48.3	58.3	51.5 48.8	42.6 40.4		51.4 47.6	51.1 46.8	46.6 43.8	42.7 40.5	42.6 40.5			67608. 23988.3	
	53 54	7/23/2014	10:20:40			43.8 50.8	53.8 60.8	54.4	41.9		54.2	54.1	45.7	42.3	42.1			120226.	4
	55	7/23/2014	10:21:00			46.7	56.7	\$4,3	42.3		53.9	53	45.3	43	42.5			46773.5	* W.
	56	7/23/2014				51.5	61.5 62.1	55 56.1	42.8 46.3		54.3 55.5	54.2 55.4	48,3 51,1	43.1 48.2	43			141253. 16218	
	57	7/23/2014				52.1 44.4	54.4	47.9	41.1		47	46.1	43.6	41.4	41.2			27542.2	
	59	7/23/2014	10:21:40	00d 00		50.3	60.3	53,4	41.2		53.3	53.3	50.2	43.2	42.1			107151. 17782.7	
	60	7/23/2014				42.5	52.5	46.8 6 49.	39.4 5 39,-		46.3	45.9 48.7	41.3 44	39.8 41.3	39.6 40.	6		39810.7	
	61	1 7/23/2014 2 7/23/2014		0 000 0 0 000 0		46 45.5	+				49.1		*************					35481.3	4
	6	3 7/23/201	4 10:22:2	20 00d 0	0:10.0	46.4	56,	4 49.	в 44.		48.9	48.3	45.8					43651.5 64565.4	
	64			30 00d 0 40 00d 0	*******	48.1 45.6	58. 55.		~ *		51.3 49.6					*************		36307.8	
	6			50 00d 0		45.6	***********				42.9			1 40.4	40.	9		14454.	4
	6	7/23/201	4 10:23:0	00 00d 0	0:10.0	40,5					42.3					7		11220.1 16595.8	
	68				0:10.0 0:10.0						43.5							60255.9	
	69			20 00d 0 30 00d 0						2	45,4		3 43.9	9 43.	3 43,	3		23442.2	9
	7	1 7/23/201	4 10:23:4	40 00d 0	00:10.0	44.5	54.	5 44.	9 43.		44.9					**********		28183.8 26302.6	
		2 7/23/201			0:10.0	44.2 49.2	**************				44.6				****************	/ 6		83176.3	
	7	3 7/23/201 4 7/23/201		***********	0:10.0	************					52.7			1 46.:	1 45.	9		95499.2	6
	7	5 7/23/201	4 10:24:	20 00d 0	00:10.0	49.7	59.	7 53.	2 44.	3	52.6	52.		**************				93325.4 79432.8	
	7	6 7/23/201	4 10:24:	30 00d 0	******	49 50.5					52.					8 1		112201	
	7	7 7/23/201 8 7/23/201	4 10:24: 4 10:24:	40 00d 0 50 00d 0		50.5	************				53.4		3 50.	9 49.	1 48.	4		151356	.1
		9 7/23/201	4 10:25:	00 00d C	00:10.0	49.8	59.	8 53.	8 45.	.6	53.	1 52.	5 49.	• • • • • • • • • • • • • • • • • • •		8		95499.2	
	8	0 7/23/201	4 10:25:	10 00d 0		+	*********				53. 51.					5 6		114815 72443	
		1 7/23/201 2 7/23/201		20 00d 0 30 00d 0			+				51.			************	*****	5		83176.	38
		2 7/23/201 3 7/23/201	4 10:25:	40 00d 0	00:10.0	48.1		1 52	2 4	IS -,-	51.	7 51.	2 47.	5 45.	4 45.	3		64565.4	
	8	4 7/23/201	4 10:25:	50 00d 0							52. 52.				*************	4 6		10000 95499.2	
		5 7/23/201 6 7/23/201		00 00d 0 10 00d 0	*********						48.		***********	**********		7		34673.6	69
		7 7/23/201		20 00d (50.9	60	.9 54	3 45	8	54.	1 53.	9 49.		1 4	6		123026	
	8	8 7/23/201	4 10:26:	30 00d 0	**********		6	50 52			52.			**************		.6		10000 43651.5	
		9 7/23/201	ai 10.26:	40 00d (00:10.0	46.4	1 56	.4 52	.9 42		52.	4 49.			************			56234.1	

ASTE IERE	Address	Start Time	Measure	men	t Time	Leq	LE	LMAX	LMIN	Ly	LN1	LN2	LN3	LN4	LN5	Over	Under		Overal Leq
<u> </u>	R2-D2	7/23/2014	10:12:00	004	00:10.0	42.2	52.2	43.9	40.5	÷	43.5	43.4	41.8	40.7	40.7			16595.8691	46.6
	2	7/23/2014	10:12:10		00:10.0	40.4	50.4	41.1	39.9		40.8	40.7	40.4	40.1	40			10964.782	
	3	7/23/2014	10:12:20		00:10.0	42.9	52.9	44.9	40.2		44.7 44.8	44.4 44.7	43	40.7 41.1	40.4 41			19498.446 19054.6072	
	4	7/23/2014 7/23/2014	10:12:30 10:12:40		00:10.0	42.8 41.5	52.8 51.5	44.8 43.1	40.8 39.7	-v. -v.	44.8	43	41.2	39.9	39.8			14125.3754	
	6	7/23/2014	10:12:50	00d	00:10.0	39.7	49.7	40.8	39.1		40.6	40.5	39.5	39.2	39.1			9332.54301 19054.6072	
	7	7/23/2014	10:13:00 10:13:10		00:10.0	42.8 44.5	52.8 54.5	45 47.3	39.5 41.3		44.9 47.3	44,8 47.1	41.3 42.7	39.7 41.6	39.6 41.4			28183,8293	
	8 9	7/23/2014	10:13:20		00:10.0	46.6	56.6	50.5	43.5		49.5	48.4	45.1	43.9	43.7			45708.819	1
	10	7/23/2014	10:13:30		00:10.0	48.6	58.6	51.6	45.5 41.8		51.5 45.3	51.1 45.2	49.2 44	46.1 41.9	46 41.8			72443.596	
	11 12	7/23/2014 7/23/2014	10:13:40 10:13:50		00:10.0	43.7	53.7 52	45.6 43.8	41.8		43.5	43.4	42.6	40.6	40.5			15848.9319	
	13	7/23/2014	10:14:00		00:10.0	41.4	51.4	45.1	39.8		42.3	41.4	40.4	40	40			13803.8426	
	14 15	7/23/2014	10:14:10 10:14:20		00:10.0	47.5 45	57.5 55	49.9 45.3	44.7 44.5		49.8 45.2	49.7 45.2	47 44.9	44.9 44.6	44.8 44.6			56234.1325 31622.7766	
	16	7/23/2014	10:14:30	******	00:10.0	49.9	59.9	51	45.2		50.9	50,8	50.3	46.2	45.5			97723.7221	
	17 18	7/23/2014	10:14:40		00:10.0	45.2	56.2	49.5	45		48,8 52.1	48.5	46.3 50.1	45.2 45.5	45.1 45.4			41686.9383	-
	18 19	7/23/2014 7/23/2014	10:14:50 10:15:00		00:10.0	50 43.1	60 53.1	52.2 47.3	45.2 42.6		45	52 45.1	43.2	42.9	42.8			20417.3794	
	20	7/23/2014	10:15:10		00:10.0	48.8	58.8	51.1	43.7		50.5	50.3	47.6	44.4	44.2			75857.7575 426579.519	-
	21	7/23/2014 7/23/2014	10:15:20 10:15:30		00:10.0	56.3 42.4	66.3 52.4	59.3 46.2	46.2 41.1		59.2 45.2	58.9 44.7	56.2 42.7	48.6 42	47.3 41.5			17378.0083	
	22 23	7/23/2014	10:15:40		00:10.0	40.8	50.8	41.6	40.2	~	41.3	41.2	40.7	40.4	40.3			12022.6443	
	24	7/23/2014	10:15:50		00:10.0	52.5	62.5	55.3	41.6		55.2 52.7	55 51.9	53.1 49.1	42.1 44.1	41.9 43.6			177827.941 72443.596	-
	25 26	7/23/2014 7/23/2014	10:16:00 10:16:10		00:10.0	48.6 46.3	58.6 56.3	53.2 47.3	43.5 43.5		52.7 47.2	47.1	49.1	43.9	43.8			42657.9519	1
	27	7/23/2014	10:16:20	000	00:10.0	42.9	52.9	46.3	42.3		45.6	45	42.6	42.3	42.3 43.2			19498.446 91201.0839	·
	28 29	7/23/2014 7/23/2014	10:16:30 10:16:40		00:10.0	49.6 40.4	59.6 50.4	52.9 46.4	43.2 39.7		52.9 45	52.7 43,8	48.6 40.5	43.3 39.9	43.2 39.8			10964.782	1
	30	7/23/2014	10:16:50	000	I 00:10.0	44.6	54.6	49.2	40.2		48.1	46.9	41.8	40.4	40.3			28840.315	
	31	7/23/2014	10:17:00		1 00:10.0 1 00:10.0	51.8 40.2	61.8 50.2	55.2 41.1	41.1 39.4		55.1 40.9	55 40.8	51.7 39.9	42.5 39.5	41.8 39.5			151356.125 10471.2855	
	32 33	7/23/2014 7/23/2014	10:17:10 10:17:20		00:10.0	40.2	56.5	41.1 49.5	39.4 41.1	-,- -,-	40.9	40.8	45.6	42.2	41.6			44668.3592	1
	34	7/23/2014	10:17:30	000	00:10.0	48	58	51.4	41.9		51.3	51.2	44.3	42.3	42.1			63095.7344 31622.7766	-1
	35 36	7/23/2014 7/23/2014	10:17:40 10:17:50		00:10.0 00:10.0	45 41.7	55 51.7	50.9 45.2	42.1 40.9		49.9 44.4	48.9 43.7	45.2 41.6	42.6	42.3			14791.0839	-
	37	7/23/2014	10:18:00		00:10.0	49.4	59.4	52.1	41.9		52.1	51. 9	48.3	42.4	42.1			87096.359	
	38	7/23/2014	10:18:10	*****	00:10.0	44.7	54.7	50.8 51.4	42.9 41.1		50 51.4	48.7 51	43.8	43 41.7	43 41.4			29512.0923	-
	39 40	7/23/2014 7/23/2014	10:18:20 10:18:30		d 00:10.0	47.1 49.1	57.1 59.1	52.5	41.6		52.5	52.2	48.4	41.9	41.7			81283.0516	~1
	41	7/23/2014	10:18:40		00:10.0	42.6	52.6	47.8	41.5		46.3	44.8	43	41.6	41.5			18197.0086	
	42 43	7/23/2014 7/23/2014	10:18:50 10:19:00		d 00:10.0 d 00:10.0	42.6	52.6 58	44.7 51.5	41 44.5		43.7 51.1	43.7	42.1 45.7	41.3 44.7	41.2 44.6			63095.7344	1
	44	7/23/2014	10:19:10		d 00:10.0	46.5	56.5	51.5	43.3		51.2	50.4	46.9	43.6	43.5			44668.3592	
	45	7/23/2014	10:19:20		00:10.0	45.3	55.3	47.8	42.9		47.8 48.5	47.1	44.2	43.3 42.7	43.1 42.5		······	33884.4156	
	46	7/23/2014 7/23/2014	10:19:30	00	d 00:10.0 d 00:10.0	46.1	56.1 54	48.6 45	42.3 42.3		44.9	44.8	43.5	42.7	42.5			25118.8645	
	48	7/23/2014	10:19:50	00	d 00 :10.0		56.8	48.5	44.9		48.1	47.7	46.7	45.2	45			47863.0092	2
	49 50	7/23/2014 7/23/2014	10:20:00 10:20:10		d 00:10.0 d 00:10.0	**************	55.6 53.6	47.6	44 41.3		47.2	47	45.7	44.6 41.7	44.3 41.5			22908.6765	5
	51	7/23/2014	10:20:20		d 00:10.0	+	51	43.1	39.4		42.8	42.1	40.5	39.7	39.6			12589.2541	
	52	7/23/2014	10:20:30		d 00:10.0		54.7	47.2 47	42.3 39.6		46.9 46.5	46.5 45.9	43.7	42.5 40.1	42.4 39.9			29512.092	
	53 54	7/23/2014 7/23/2014	10:20:40 10:20:50		d 00:10.0 d 00:10.0		53.1 52.7	46.3	41.2		45.6	45.1	42.5	41.6	41.4			18620.8714	4
	55	7/23/2014	10:21:00		d 00:10.0	*************	56.5	49.4	42.3		49.2	48.9	44,4	42.7	42.5 41.6			44668.3592 20892.9613	~~
	56 57	7/23/2014	10:21:10 10:21:20		d 00:10.0 d 00:10.0		53.2 53.9	47.2	41.6 40.2		46.7 46.9	46.1	43	41.7 41.1	40.6			24547.0892	E
	58	7/23/2014	10:21:30		d 00:10.0		52.6	48	38.3		46.9	43.3	40.9	38.9	38.5			18197.008	**
	59	7/23/2014	10:21:40		d 00:10.0		55.5 52.3	49.4 46.1	42.2		48.4 45.3	48.1 44.8	45.4	42.7 40.7	42.4			35481.3389	
	60 61	7/23/2014 7/23/2014	10:21:50 10:22:00		d 00:10.0		52.3 52.5	46.1	39.8		45.5	44.9	42.2	40.2	40		*****	17782.794	1
	62	7/23/2014	10:22:10	00	d 00:10.0	44.6	54.6	47.8	39.8		47.4	47.1 48.9	41.9 46.5	40.8 45.4	40.8			28840.315 50118.723	
	63 64	7/23/2014	10:22:20		d 00:10.0		57 55	49.2 48.2	45 41.7	-,-	49.1 47.7	48.9	45.6	45.4	43.2			31622.776	6
	65	7/23/2014	10:22:40	00	d 00:10.0	44,4	54.4	45.6	41.7		45.3	44.9	44.4	42.6	42.5			27542.287	
	66	7/23/2014	10:22:50 10:23:00		d 00:10.0		56 52.9	49.2 45.4	42.1 40.7		49 45,1	48.8	45.3 42.8	43.6 4 <u>1</u>	42.8			19498.446	
	67 68	7/23/2014 7/23/2014			id 00:10.0		52.5	44.2	40.6		43.8	43.7	42,1	41.3	41			17378.008	
	69	7/23/2014	10:23:20	00	d 00:10.0		51.5	42.9	39.3		42.9 43.1	42.8 42.8	41.2	39,9 40.6	39.6 40.5			14125.375	
	70 71	7/23/2014	10:23:30		d 00:10.0		51.4 51.6	43.2 43.8	40.5 39.5		43.1	42.8	41.2	40.6 39.8	39.6			14454.397	7
	72	7/23/2014	10:23:50	00	d 00:10.	42.9	52.9	44.3	41.7		44	43.9	42.6	41.8	41.8			19498.446 50118.723	~
	73	7/23/2014		***	d 00:10.		57 53.9	48.5 46.8	44.3 40.4		48.3	48.2 45.9	47	45.1 41.2	44.9 40.9			24547.089	
	74 75	7/23/2014 7/23/2014			d 00:10.		54,4	46.9	41.5		46.5	46.2	44,4	41.8	41.6			27542.287	
	76	7/23/2014	10:24:30	0	od 00:10.	50.1	60.1	52	44,3		51.9	51.8	50.1 53.5	44.6 46.4	44.6 45.9			102329.29 275422.87	
	77 78	7/23/2014			d 00:10.		64.4 56.2	59 47.7	45.5 43.9		58.7 47.5	58.3 47.2	45.7	46.4	45.9			41686,938	
	78	7/23/2014	10:25:00	00	od 00:10.	48.1	58.1	50.9	40.2		50.8	50.7	48.7	41.5	40.8			64565.422	
	80	7/23/2014			d 00:10.		S3.7	47.6	39.5		46.9 53.9	45,5 53.7	42.5	40 46.1	39.7 46			23442.288	
	81 82	7/23/2014	10:25:20		d 00:10. d 00:10.		60.9 60.3	54 53.9	46		53.9	53.7	48.8 50.7	46.1	46.4			107151.93	1
	83	7/23/2014	10:25:40	00	od 00:10.	0 43.8	53.8	47.2	41.9		46.8	46.3	43,4	42.2	42.1			23988.329	
	84	7/23/2014			od 00:10.		55.5 53.1	49.3 45,3	41.3		48.9	48.5 45	44.9 42.2	42.9	42.1			35481.338 20417.379	
	85 86	7/23/2014	*****************		od 00:10.		53.1	45,5	42		45	45	43.4	42.2	42.1			22387.211	4
	87	7/23/2014	10:26:20	0	0d 00:10,	0 42.4	52.4	46.2	39.8		45.5	45	42	40.1 40.4	40 40.3			17378.008 27542.28	
	88	7/23/2014			od 00:10.		54.4 50.3	46.9 44.5	40.1 38.4	-,-	46.6	45.4 44	43.9 39.1	40.4 38.5	40.3 38.4		*****	10715.193	
	89	7/23/2014			od 00:10.		49.3	40.7	38.4		40.5	40.3	38.9	38.5	38.4			8511.3803	8

Appendix D Traffic Data Summary

	From East to West			AM F	Peak		
	Link	E	xisting (201	3)	Futur	e No-Build	(20 25)
Location	Description	cars	МТ	HT	cars	МТ	HT
1	I80 EB West of Rt. 611 Ramp	1096	228	188	1390	289	238
2	I80 WB West of Rt. 611 Ramp	887	171	160	1125		203
3	I80 EB btw Rt. 611 Ramp and Rt. 209 Ramp	977	203	168	1239		
4	I80 WB btw Rt. 611 Ramp and Rt. 209 Ramp	820	158	148	1040	201	187
5	I80 EB btw Rt. 209 and W. Main St.	1580	329	271	2004	417	344
6	I80 WB btw Rt. 209 and W. Main St.	1215	235	219	1541	298	278
7	I80 EB btw W. Main St. and Broad St.	1637	341	281	2076	432	356
8	I80 WB btw W. Main St. and Broad St.	1250	242	225	1585	306	286
9	I80 EB East of Broad St.	1445	301	248	1833	382	314
10	I80 WB East of Broad St.	1206	233	217	1530	296	276
11	Park Ave. (Rt. 611) NB	362	10	10	460	12	12
12	Park Ave. (Rt. 611) SB	192	5	5	244	6	6
13	Broad St. (Rt. 191) NB	589	12	12	745	16	16
14	Broad St. (Rt. 191) SB	387	8	8	491	10	10
15	I80 EB to Rt. 611	154	8	3	195	10	4
16	Rt. 611 to I80 WB	85	4	3	108		4
17	Rt. 209 NB to I80 EB	768	27	39	974		-
18	I80 WB to Rt. 209 SB	480	25	38	609	-	
19	W. Main St. to I80 EB	165	7	0	209	-	0
20	W. Main St. to I80 WB	161	11	2	204		-
21	I80 EB to W. Main St	193	14	2	245	-	-
22	I80 WB to W. Main St	147	2	2	186	-	-
23	Dreher Ave. to I80 EB	110	5	1	140	-	
24	I80 EB to Rt. 611 (Park Ave.)	364	13	4	462	-	5
25	Rt. 611 (Park Ave.) to I80 EB	104	9	3	132		4
26	I80 WB to Broad St.	186	5	0	236		-
27	Broad St. to I80 WB	235	14	5	298	18	6

Ramps

	From East to West	PM Peak						
	Link	Ex	isting (201	3)	Futur	e No-Build (2025)	
Location	Description	cars	MT	HT	cars	MT	HT	
1	I80 EB West of Rt. 611 Ramp	1390	289	238	1762	367	302	
2	I80 WB West of Rt. 611 Ramp	1848	357	333	2344	453	422	
3	I80 EB btw Rt. 611 Ramp and Rt. 209 Ramp	1232	256	211	1562	325	268	
4	I80 WB btw Rt. 611 Ramp and Rt. 209 Ramp	1724	333	311	2186	422	394	
5	I80 EB btw Rt. 209 and W. Main St.	1787	372	306	2266	472	389	
6	I80 WB btw Rt. 209 and W. Main St.	2496	482	450	3165	612	570	
7	I80 EB btw W. Main St. and Broad St.	1820	379	312	2308	480	396	
8	I80 WB btw W. Main St. and Broad St.	2604	503	469	3303	638	595	
9	I80 EB East of Broad St.	1672	348	287	2121	441	364	
10	I80 WB East of Broad St.	2515	486	453	3190	617	575	
11	Park Ave. (Rt. 611) NB	295	8	8	374	10	10	<u>.0</u>
12	Park Ave. (Rt. 611) SB	409	11	11	519	14	14	Used for Analysis
13	Broad St. (Rt. 191) NB	598	12	12	757	16	16	Ana
14	Broad St. (Rt. 191) SB	485	10	10	614	13	13	or /
15	I80 EB to Rt. 611	215	2	1	273	3	1	d fo
16	Rt. 611 to I80 WB	169	2	0	214	3	0	Se
17	Rt. 209 NB to I80 EB	735	15	17	932	19	22	
18	I80 WB to Rt. 209 SB	1020	23	19	1294	29	24	
19	W. Main St. to I80 EB	193	3	0	245	4	0	
20	W. Main St. to I80 WB	309	9	2	392	11	3	
21	I80 EB to W. Main St	237	11	2	301	14	3	
22	I80 WB to W. Main St	302	4	2	383	5	3	
23	Dreher Ave. to I80 EB	99	1	0	126	1	0	
24	I80 EB to Rt. 611 (Park Ave.)	330	12	2	419	15	3	
25	Rt. 611 (Park Ave.) to I80 EB	136	3	1	172	4	1	
26	I80 WB to Broad St.	294	3	0	373	4	0	
27	Broad St. to I80 WB	403	14	2	511	18	3	

MT = Medium Truck (2 axles with 6 wheels) HT = Heavy Truck (3 or more axles)

Ramps

	From East to West		AM P	eak	
	Link		Alternat	ive 2A	
Location	Description	cars	MT	HT	Total AM
1	I80 EB West of Ramp A	1985	413	341	2746
2	I80 WB West of Ramp B	1596	308	288	2195
3	I80 EB btw Ramp A and Ramp C	1879	391	322	2599
4	I80 WB btw Ramp B and Ramp F	1547	299	279	2128
5	I80 EB btw Ramp C and Ramp G	3015	628	517	4170
6	I80 WB btw Ramp F and Ramp D	2128	411	383	2927
7	I80 EB btw Ramp G and Ramp E	2692	560	462	3724
8	I80 WB btw Ramp F and Ramp R	2355	455	424	3240
9	I80 EB btw Ramp E and Ramp Q	3085	642	529	4267
10	I80 WB btw Ramp R and Ramp S	2011	389	362	2766
11	I80 EB btw Ramp Q and Ramp T	2566	534	440	3549
12	I80 EB East of Ramp T	2724	567	467	3767
13	I80 WB East of Ramp S	2273	439	410	3126
14	Park Ave. (Rt. 611) NB (North of EB ramp)	593	16	16	625
15	Park Ave. (Rt. 611) SB (South of EB Ramp)	256	7	7	270
16	Broad St. (Rt. 191) NB (North of WB Ramps)	648	13	13	674
17	Broad St. (Rt. 191) SB (South of WB Ramps)	183	4	4	191
18	Main St. EB (East of Ramp F)	574	12	12	598
19	Main St. WB (East of Ramp F)	515	11	11	537
20	Dreher St. NB North of CD Road	201	4	4	209
21	Dreher St. SB North of CD Road	188	4	4	196
22	Dreher St. NB South of CD Road	257	5	5	267
23	Dreher St. SB South of CD Road	143	3	3	149
24	CD Road NB North of Ramps E and G	329	7	7	343
25	CD Road SB North of Ramps E and G	320	7	7	334
26	CD Road NB South of Ramps E and G	219	5	5	229
27	CD Road SB South of Ramps E and G	120	2	2	124
28	Ramp A West of 611 Connector (I-80 EB to SR 611)	244	51	42	337
29 30	Ramp A East of 611 Connector (SR 611 to I-80 EB)	137	29 24	24 23	190 172
30	Ramp B West of 611 Connector (SR 611 to I-80 WB)Ramp B East of 611 Connector (I-80 WB to SR 611)	125	15	23	172
31	Ramp B East of 611 Connector (1-80 wB to SK 611) Ramp C (US 209 NB to I-80 EB)	1137	237	14	1572
32	Ramp D (I-80 WB to US209 SB)	648	125	193	891
33	Ramp E (Dreher Connector Rd to I-80 EB)	393	82	67	543
35	Ramp E (Dener Connector Ru to 1-80 EB) Ramp F (I-80 WB to Bus209)	228	44	41	313
36	Ramp F (Bus209 to I-80 WB)	197	38	36	271
37	Ramp G (I-80 EB to Dreher Connector Rd)	323	67	55	447
38	Ramp Q (I-80 EB to Park Ave SR611)	519	108	89	718
39	Ramp R (SR191 to I-80 WB)	344	66	62	473
40	Ramp S (I-80 WB to SR191)	262	51	47	360
41	Ramp T (SR191 to I-80 EB)	158	33	27	219
	Rt. 209 NB South of West Main St.	1462	55	55	1572
	Rt. 209 SB South of West Main St.	801	45	45	891

Alternative 2A Traffic (AM)

	From East to West		PM P	eak		
	Link		Alternat	ive 2 A		
Location	Description	cars	MT	HT	Total	
1	I80 EB West of Ramp A	2499	486	429	3456	
2	I80 WB West of Ramp B	3314	641	597	4559	
3	I80 EB btw Ramp A and Ramp C	2368	460	406	3275	
4	I80 WB btw Ramp B and Ramp F	3228	624	582	4440	
5	I80 EB btw Ramp C and Ramp G	3413	663	585	4721	
6	I80 WB btw Ramp F and Ramp D	4413	853	795	6070	
7	I80 EB btw Ramp G and Ramp E	3026	630	519	4186	
8	I80 WB btw Ramp F and Ramp R	4907	948	884	6750	
9	I80 EB btw Ramp E and Ramp Q	3429	714	588	4743	
10	I80 WB btw Ramp R and Ramp S	4334	838	781	5961	
11	I80 EB btw Ramp Q and Ramp T	2961	616	508	4095	
12	I80 EB East of Ramp T	3152	656	541	4359	
13	I80 WB East of Ramp S	4741	916	854	6521	
14	Park Ave. (Rt. 611) NB (North of EB ramp)	602	16	16	634	
15	Park Ave. (Rt. 611) SB (South of EB Ramp)	445	12	12	469	
16	Broad St. (Rt. 191) NB (North of WB Ramps)	738	15	15	768	
17	Broad St. (Rt. 191) SB (South of WB Ramps)	392	8	8	408	
18	Main St. EB (East of Ramp F)	711	15	15	741	Jsed for analysis
19	Main St. WB (East of Ramp F)	959	20	20	999	<u>الج</u>
20	Dreher St. NB North of CD Road	186	4	4	194	na
21 22	Dreher St. SB North of CD Road	400	8	8	416 196	L C
22	Dreher St. NB South of CD Road Dreher St. SB South of CD Road	333	4	4	347	fo
23	CD Road NB North of Ramps E and G	409	9	9	427	eq
24	CD Road SB North of Ramps E and G	362	8	9	378	∩
26	CD Road NB South of Ramps E and G	191	4	4	199	
27	CD Road SB South of Ramps E and G	122	3	3	133	
28	Ramp A West of 611 Connector (I-80 EB to SR 611)	325	68	56	449	
29	Ramp A East of 611 Connector (SR 611 to I-80 EB)	195	40	33	268	
30	Ramp B West of 611 Connector (SR 611 to I-80 WB)	234	45	42	322	
31	Ramp B East of 611 Connector (I-80 WB to SR 611)	148	29	27	204	
32	Ramp C (US 209 NB to I-80 EB)	1045	217	179	1445	
33	Ramp D (I-80 WB to US209 SB)	1278	247	230	1758	
34	Ramp E (Dreher Connector Rd to I-80 EB)	403	84	69	558	
35	Ramp F (I-80 WB to Bus209)	494	96	89	680	
36	Ramp F (Bus209 to I-80 WB)	367	71	66	505	
37	Ramp G (I-80 EB to Dreher Connector Rd)	387	81	66	535	
38	Ramp Q (I-80 EB to Park Ave SR611)	469	98	80	648	
39	Ramp R (SR191 to I-80 WB)	574	111	103	790	
40	Ramp S (I-80 WB to SR191)	407	79	73	560	
41	Ramp T (SR191 to I-80 EB)	191	40	33	264	
	Rt. 209 NB South of West Main St.	1343	51	51	1445	
	Rt. 209 SB South of West Main St.	1582	88	88	1758	

Alternative 2A Traffic (PM)

	From East to West		AM Peak							
	Link		Alternati	ve 2B						
Location	Description	cars	MT	HT	Total					
1	I80 EB West of Ramp A	1944	405	333	2689					
2	I80 WB West of Ramp B	1679	324	302	2309					
3	I80 EB btw Ramp A and Ramp C	1664	346	285	2302					
4	I80 WB btw Ramp B and Ramp F	1450	280	261	1994					
5	I80 EB btw Ramp C and Ramp G	3039	633	521	4204					
6	I80 WB btw Ramp F and Ramp D	2128	411	383	2927					
7	I80 EB btw Ramp G and Ramp E	3039	633	521	4204					
8	I80 WB btw Ramp F and Ramp R	2331	450	420	3206					
9	I80 EB btw Ramp E and Ramp Q	3039	633	521	4204					
10	Iso WB btw Ramp R and Ramp S	1986	384	358	2732					
-										
11	I80 EB btw Ramp Q and Ramp T	2520	525	432	3486					
12	I80 EB East of Ramp T	2724	567	467	3767					
13	I80 WB East of Ramp S	2273	439	410	3126					
14	Park Ave. (Rt. 611) NB (North of EB ramp)	593	16	16	625					
15	Park Ave. (Rt. 611) SB (South of EB Ramp)	384	10	10	404					
16	Broad St. (Rt. 191) NB (North of WB Ramps)	679	14	14	707					
17	Broad St. (Rt. 191) SB (South of WB Ramps)	116	2	2	120					
18	Main St. EB (East of Ramp F)	612	13	13	638					
19	Main St. WB (East of Ramp F)	424	9	9	442					
20	Dreher St. NB North of CD Road	194	4	4	202					
21	Dreher St. SB North of CD Road	238	5	5	248					
22	Dreher St. NB South of CD Road	337	7	7	351					
23	Dreher St. SB South of CD Road	291	6	6	303					
24	CD Road NB North of Ramps E and G	168	3	3	174					
25	CD Road SB North of Ramps E and G	76	2	2	80					
26	CD Road NB South of Ramps E and G	168	3	3	174					
27	CD Road SB South of Ramps E and G	76	2	2	80					
28	Ramp A West of 611 Connector (I-80 EB to SR 611)	176	37	30	243					
29	Ramp A East of 611 Connector (SR 611 to I-80 EB)	123	26	21	170					
30	Ramp B West of 611 Connector (I-80 EB to US209SB/Bus209)	227	47	39	314					
31	Ramp C East of 611 Connector (US209NB to I-80WB)	228	48	39	316					
32	Ramp D West of 611 Connector (SR 611 to I-80 WB)	126	24	23	173					
33	Ramp E East of 611 Connector (I-80 WB to SR 611)	126	24	23	174					
34	Ramp F (I-80 EB to Bus209)	192	40	33	265					
35	Ramp G (I-80 WB to US209 SB)	744	144	134	1023					
36	Ramp H (Bus209 to I-80 WB)	142	28	26	196					
37 38	Ramp J (US 209 NB to I-80 EB)	1061	221	182	1468					
	Ramp K (Bus209 to I-80 EB)	314	65	54	434					
39	Ramp L (US209NB to Bus 209)	125 95	26 20	21	173					
40	Ramp M (Bus 209 to US209SB)			16	132					
41	Ramp N (I-80 WB to Bus209)	203	39	37	279					
42	Ramp Q (I-80 EB to Park Ave SR611)	519	108	89	718					
43	Ramp R (SR191 to I-80 WB)	344	66	62	473					
44	Ramp S (I-80 WB to SR191)	286	55	52	394					
45	Ramp T (Park Ave SR611 to I-80 EB)	204	42	35	282					
	Rt. 209 NB South of West Main St.	1721	65	65	1851					

Alternative 2B Traffic (AM)

	From East to West		PM P	eak		
	Link		Alternat	ive 2B		
Location	Description	cars	MT	HT	Total	
1	I80 EB West of Ramp A	2451	510	420	3390	
2	I80 WB West of Ramp B	3443	665	620	4736	
3	I80 EB btw Ramp A and Ramp C	2095	436	359	2898	
4	I80 WB btw Ramp B and Ramp F	3072	594	553	4225	
5	I80 EB btw Ramp C and Ramp G	3388	705	581	4686	
6	I80 WB btw Ramp F and Ramp D	4413	853	795	6070	
7	I80 EB btw Ramp G and Ramp E	3388	705	581	4686	
8	I80 WB btw Ramp F and Ramp R	4851	937	874	6672	
9	I80 EB btw Ramp E and Ramp Q	3388	705	581	4686	
10	I80 WB btw Ramp R and Ramp S	4277	827	771	5883	
11	I80 EB btw Ramp Q and Ramp T	2919	608	501	4038	
12	I80 EB East of Ramp T	3152	656	541	4359	
13	I80 WB East of Ramp S	4741	916	854	6521	
14	Park Ave. (Rt. 611) NB (North of EB ramp)	507	13	13	533	
15	Park Ave. (Rt. 611) SB (South of EB Ramp)	667	18	18	703	
16	Broad St. (Rt. 191) NB (North of WB Ramps)	811	17	17	845	
17	Broad St. (Rt. 191) SB (South of WB Ramps)	323	7	7	337	
18	Main St. EB (East of Ramp F)	775	16	16	807	
19	Main St. WB (East of Ramp F)	771	16	16	803	
20	Dreher St. NB North of CD Road	150	3	3	156	<u>.</u>
21	Dreher St. SB North of CD Road	494	10	10	514	ys
22	Dreher St. NB South of CD Road	279	6	6	291	ାସ
23	Dreher St. SB South of CD Road	603	13	13	629	Used for analysis
24	CD Road NB North of Ramps E and G	152	3	3	158	or
25	CD Road SB North of Ramps E and G	132	3	3	138	d.
26	CD Road NB South of Ramps E and G	152	3	3	158	Se
27	CD Road SB South of Ramps E and G	132	3	3	138	
28	Ramp A West of 611 Connector (I-80 EB to SR 611)	234	49	40	324	
29	Ramp A East of 611 Connector (SR 611 to I-80 EB)	173	36	30	239	
30	Ramp B West of 611 Connector (I-80 EB to US209SB/Bus209)	294	61	50	407	
31	Ramp C East of 611 Connector (US209NB to I-80WB)	330	69	57	457	
32	Ramp D West of 611 Connector (SR 611 to I-80 WB)	234	45	42	322	
33	Ramp E East of 611 Connector (I-80 WB to SR 611)	196	38	35	269	
34	Ramp F (I-80 EB to Bus209)	225	47	39	311	
35	Ramp G (I-80 WB to US209 SB)	1455	281	262	2001	
36	Ramp H (Bus209 to I-80 WB)	262	51	47	360	
37	Ramp J (US 209 NB to I-80 EB)	964	201	165	1334	
38	Ramp K (Bus209 to I-80 EB)	328	68	56	454	
39	Ramp L (US209NB to Bus 209)	128	27	22	177	
40	Ramp M (Bus 209 to US209SB)	176	37	30	243	
41	Ramp N (I-80 WB to Bus209)	438	85	79	602	
42	Ramp Q (I-80 EB to Park Ave SR611)	469	98	80	648	
43	Ramp R (SR191 to I-80 WB)	574	111	103	790	
44	Ramp S (I-80 WB to SR191)	464	90	84	638	
45	Ramp T (Park Ave SR611 to I-80 EB)	232	48	40	321	
	Rt. 209 NB South of West Main St.	1580	59	59	1698	
	Rt. 209 SB South of West Main St.	2106	117	117	2340	

Alternative 2B Traffic (PM)

Alternative 2D Traffic (AM)

	From East to West		AM F	Peak	
	Link		Alterna	tive 2D	
Location	Description	cars	MT	HT	Total
1	I80 EB West of Ramp A	1944	405	333	2689
2	I80 WB West of Ramp B	1679	324	302	2309
3	I80 EB btw Ramp A and Ramp C	1664	346	285	2302
4	I80 WB btw Ramp B and Ramp F	1527	295	275	2100
5	I80 EB btw Ramp C and Ramp G	3039	633	521	4204
6	I80 WB btw Ramp F and Ramp D	2128	411	383	2927
7	I80 EB btw Ramp G and Ramp E	3039	633	521	4204
8	I80 WB btw Ramp F and Ramp R	2331	450	420	3206
9	I80 EB btw Ramp E and Ramp Q	3039	633	521	4204
10	I80 WB btw Ramp R and Ramp S	1986	384	358	2732
11	I80 EB btw Ramp Q and Ramp T	2520	525	432	3486
12	I80 EB East of Ramp T	2724	567	467	3767
13	I80 WB East of Ramp S	2273	439	410	3126
14	Park Ave. (Rt. 611) NB (North of EB ramp)	593	16	16	625
			10	-	
15	Park Ave. (Rt. 611) SB (South of EB Ramp)	384	-	10	404
16	Broad St. (Rt. 191) NB (North of WB Ramps)	679	14	14	707
17	Broad St. (Rt. 191) SB (South of WB Ramps)	116	2	2	120
18	Main St. EB (East of Ramp F)	612	13	13	638
19	Main St. WB (East of Ramp F)	424	9	9	442
20	Dreher St. NB North of CD Road	194	4	4	202
21 22	Dreher St. SB North of CD Road	238	5	5	248
22	Dreher St. NB South of CD Road Dreher St. SB South of CD Road	337 291	7	6	351 303
23	CD Road NB North of Ramps E and G	168	3	3	174
25	CD Road SB North of Ramps E and G	76	2	2	80
26	CD Road NB South of Ramps E and G	168	3	3	174
27	CD Road SB South of Ramps E and G	76	2	2	80
28	Ramp A West of 611 Connector (I-80 EB to SR 611)	176	37	30	243
29	Ramp B East of 611 Connector (SR 611 to I-80 EB)	123	26	21	170
30	Ramp C East of 611 Connector (I-80 WB to SR 611)	126	24	23	174
31	Ramp D West of 611 Connector (SR 611 to I-80 WB)	126	24	23	173
32	Ramp E East of 611 Connector (US209NB to I-80WB)	152	32	26	210
33	Ramp F West of 611 Connector (I-80 EB to US209SB)	35	7	6	49
34	Ramp G (I-80 EB to Bus209)	192	40	33	265
35	Ramp H (Bus209 to I-80 WB)	142	28	26	196
36	Ramp I (I-80 WB to US209 SB)	744	144	134	1023
37	Ramp J (US 209 NB to I-80 EB)	1061	221	182	1468
38	Ramp K (Bus209 to I-80 EB)	314	65	54	434
39	Ramp L (US209NB to Bus 209)	125	26	21	173
40 41	Ramp M (Bus 209 to US209SB) Ramp N (I-80 WB to Bus209)	95 203	20 39	16 37	132 279
41	Ramp Q (I-80 EB to Park Ave SR611)	519	39 108	37 89	718
42	Ramp Q (1-80 EB to Park Ave Skorr) Ramp R (SR191 to I-80 WB)	344	66	62	473
44	Ramp S (I-80 WB to SR191)	286	55	52	394
45	Ramp T (Park Ave SR611 to I-80 EB)	204	42	32	282
46	Rt. 209 NB South of West Main St.	1721	65	65	1851
47	Rt. 209 SB South of West Main St.	1084	60	60	1204

Alternative 2D Traffic (PM)

	From East to West		PM P	eak		
	Link		Alternat	ive 2D		
ocation	Description	cars	MT	HT	Total	
1	I80 EB West of Ramp A	2451	510	420	3390	
2	I80 WB West of Ramp B	3443	665	620	4736	
3	ISO EB btw Ramp A and Ramp C	2095	436	359	2898	
4	I80 WB btw Ramp B and Ramp F	3220	622	580	4429	
5	I80 EB btw Ramp C and Ramp G	3388	705	581	4686	
6	I80 WB btw Ramp F and Ramp D	4413	853	795	6070	
7	I80 EB btw Ramp G and Ramp E	3388	705	581	4686	
8	I80 WB btw Ramp F and Ramp R	4851	937	874	6672	
9	I80 EB btw Ramp E and Ramp Q	3388	705	581	4686	
10	I80 WB btw Ramp R and Ramp S	4277	827	771	5883	
11	I80 EB btw Ramp Q and Ramp T	2919	608	501	4038	
12	I80 EB East of Ramp T	3152	656	541	4359	
13	I80 WB East of Ramp S	4741	916	854	6521	
14	Park Ave. (Rt. 611) NB (North of EB ramp)	507	13	13	533	
15	Park Ave. (Rt. 611) SB (South of EB Ramp)	667	18	18	703	
16	Broad St. (Rt. 191) NB (North of WB Ramps)	811	17	17	845	
17	Broad St. (Rt. 191) SB (South of WB Ramps)	323	7	7	337	
18	Main St. EB (East of Ramp F)	775	16	16	807	
19	Main St. WB (East of Ramp F)	771	16	16	803	
20	Dreher St. NB North of CD Road	150	3	3	156	S
21	Dreher St. SB North of CD Road	494	10	10	514	/si
22	Dreher St. NB South of CD Road	279	6	6	291	a
23	Dreher St. SB South of CD Road	603	13	13	629	Jsed for analysis
24	CD Road NB North of Ramps E and G	152	3	3	158	<u>с</u>
25	CD Road SB North of Ramps E and G	132	3	3	138	d
26	CD Road NB South of Ramps E and G	152	3	3	158	Se
27	CD Road SB South of Ramps E and G	132	3	3	138	Ď
28	Ramp A West of 611 Connector (I-80 EB to SR 611)	234	49	40	324	
29	Ramp B East of 611 Connector (SR 611 to I-80 EB)	173	36	30	239	
30	Ramp C East of 611 Connector (I-80 WB to SR 611)	196	38	35	269	
31	Ramp D West of 611 Connector (SR 611 to I-80 WB)	234	45	42	322	
32	Ramp E East of 611 Connector (US209NB to I-80WB)	183	38	31	253	
33	Ramp F West of 611 Connector (I-80 EB to US209SB)	69	14	12	96	
34	Ramp G (I-80 EB to Bus209)	225	47	39	311	
35	Ramp H (Bus209 to I-80 WB)	262	51	47	360	
36	Ramp I (I-80 WB to US209 SB)	1455	281	262	2001	
37	Ramp J (US 209 NB to I-80 EB)	964	201	165	1334	
38	Ramp K (Bus209 to I-80 EB)	328	68	56	454	
39	Ramp L (US209NB to Bus 209)	128	27	22	177	
40	Ramp M (Bus 209 to US209SB)	176	37	30	243	
41	Ramp N (I-80 WB to Bus209)	438	85	79	602	
42	Ramp Q (I-80 EB to Park Ave SR611)	469	98	80	648	
43	Ramp R (SR191 to I-80 WB)	574	111	103	790	
44	Ramp S (I-80 WB to SR191)	464	90	84	638	
45	Ramp T (Park Ave SR611 to I-80 EB)	232	48	40	321	
46	Rt. 209 NB South of West Main St.	1580	59	59	1698	
47	Rt. 209 SB South of West Main St.	2106	117	117	2340	

APPENDIX E TNM NOISE MODELING INPUT AND OUTPUT FILES (CD)

APPENDIX F

FEASIBILITY AND REASONABLENESS WORKSHEETS (NOT APPLICABLE AT THIS TIME)

APPENDIX G References

References

- Pennsylvania Department of Transportation Publication #24, "Project Level Highway Traffic Noise Handbook," December 2013.
- Federal Highway Administration Federal Aid Policy Guide 23 CFR 772, U.S. Government Printing Office, updated July 13, 2010.
- U.S. Department of Transportation, Federal Highway Administration "Highway Traffic Noise: Analysis and Abatement Guidance," December 2011.
- U.S. Department of Transportation, Federal Highway Administration "Measurement of Highway-Related Noise," FHWA Report No. FHWA-PD-96-046, May 1996.
- U.S. Department of Transportation, Federal Highway Administration "FHWA Traffic Noise Model User's Guide," FHWA Report No. FHWA-PD-96-009, January 1998.

APPENDIX H LIST OF PREPARERS AND REVIEWERS

List of Preparers / Reviewers

McCormick Taylor, Inc.

Jeffery C. Lasko Acoustical Scientist Education: *B.A., Geography and Environmental Planning* Professional Experience: 9 Years Role: Noise Monitoring, Noise Modeling, Project Coordination

Josh J. Wilson

Sr. Transportation Noise Specialist Education: B.S., Geo-Environmental Studies M.S., Geo-Environmental Studies Professional Experience: 14 Years Role: Report Preparation

Jack A. Cramer

Sr. Transportation Noise Specialist Education: *B.S., Geo-Environmental Studies* Professional Experience: 15 Years Role: Noise Monitoring, QA/QC

Adam Diltz

Acoustical Scientist Education: *B.A., Geography and Environmental Planning* Professional Experience: 1 Year Role: Report Preparation